

3 No. STOREY
BRACED
FRAME DEFLECTION
DERIVATION

FORCES (- INDICATES TENSION)

① $\leftarrow F_3$ ② $F_3 \rightarrow$

③ $\frac{F_3 d_3}{L}$ ④ $\frac{F_3 d_3}{L}$

⑤ $\frac{F_3 h_3}{L} \uparrow$ ⑥ $\frac{F_3 h_3}{L} \downarrow$

⑦ $F_2 + F_3$ ⑧ $F_2 + F_3$

⑨ $\frac{(F_2 + F_3) d_2}{L}$ ⑩ $\frac{(F_2 + F_3) d_2}{L}$

⑪ $\frac{F_3 h_3}{L} \downarrow$ ⑫ $\frac{F_3 h_3}{L} \uparrow$

⑬ $\frac{F_3 h_3}{L} \uparrow + \frac{(F_2 + F_3) h_2}{L} \uparrow$

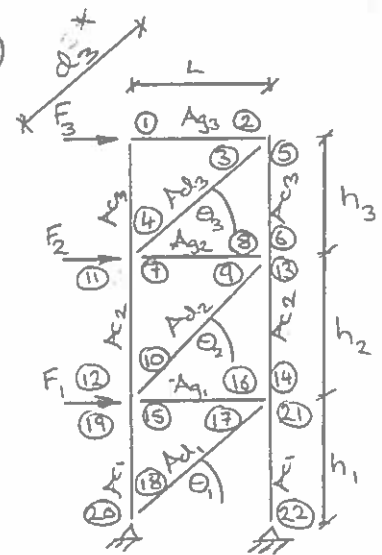
⑭ $\frac{F_3 h_3}{L} \downarrow + \frac{(F_2 + F_3) h_2}{L} \downarrow$

⑮ $F_1 + F_2 + F_3$ ⑯ $F_1 + F_2 + F_3$

⑰ $\frac{(F_1 + F_2 + F_3) d_1}{L}$ ⑱ $\frac{(F_1 + F_2 + F_3) d_1}{L}$

⑲ $\frac{F_3 h_3}{L} \uparrow + \frac{(F_2 + F_3) h_2}{L} \uparrow$ ⑳ $\frac{F_3 h_3}{L} \downarrow + \frac{(F_2 + F_3) h_2}{L} \downarrow$

㉑ $\frac{F_3 h_3}{L} + \frac{(F_2 + F_3) h_2}{L} + \frac{(F_1 + F_2 + F_3) h_1}{L} \uparrow$ ㉒ $\frac{F_3 h_3}{L} + \frac{(F_2 + F_3) h_2}{L} + \frac{(F_1 + F_2 + F_3) h_1}{L} \downarrow$



* d_2 & d_1 ON LOWER LEVELS

$\sigma = \frac{FL}{AE}$

DEFLECTION DERIVATION @ ①

$\sigma_h = \frac{F_3 L}{A_{g3} E} + \frac{(F_3 d_3 / L) d_3}{A_{d3} E} + \frac{(F_3 h_3 / L) h_3}{A_{c3} E} \quad \text{--- LVL 3}$

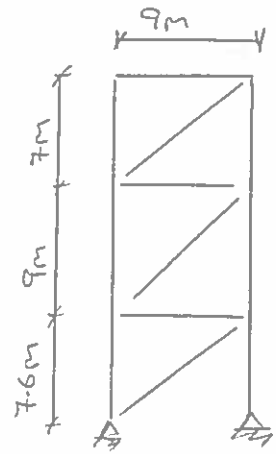
$+ \frac{(F_2 + F_3) L}{A_{g2} E} + \frac{[(F_2 + F_3) d_2 / L] d_2}{A_{d2} E} + \frac{(F_3 h_3 / L) h_3}{A_{c2} E} \quad \text{--- LVL 2}$

$+ \left(\left[\frac{F_3 h_3}{L} + \frac{(F_2 + F_3) h_2}{L} \right] h_2 \right) \quad \text{--- LVL 1}$

$+ \frac{[(F_1 + F_2 + F_3) L]}{A_{g1} E} + \frac{[(F_1 + F_2 + F_3) d_1 / L] d_1}{A_{d1} E} + \left(\frac{F_3 h_3 + (F_2 + F_3) h_2}{L} \right) h_1$

$+ \frac{(F_3 h_3 + (F_2 + F_3) h_2 + (F_1 + F_2 + F_3) h_1)}{A_{c1} E} \quad \text{--- LVL 1}$

APPLYING 1 kN LOAD AT EACH LEVEL:
(ALL CHS 168.3 x 8.0 mm SECTIONS)



$$\begin{aligned} \sigma_h &= \frac{1000 \text{ N} \times 9000 \text{ mm}}{31.2 \times 10^2 \text{ mm}^2 \times 210 \times 10^3 \text{ N/mm}^2} (1) \\ &+ \left(\frac{\left(\frac{1000 \text{ N} \times 11,401 \text{ mm}}{9000 \text{ mm}} \right) 11,401 \text{ mm}}{31.2 \times 10^2 \text{ mm}^2 \times 210 \times 10^3 \text{ N/mm}^2} \right) \times \frac{11,401 \text{ mm}}{9000 \text{ mm}} \\ &+ \left(\frac{\left(\frac{1000 \text{ N} \times 7000 \text{ mm}}{9000 \text{ mm}} \right) 7000 \text{ mm}}{31.2 \times 10^2 \text{ mm}^2 \times 210 \times 10^3 \text{ N/mm}^2} \right) \times \frac{7000 \text{ mm}}{9000 \text{ mm}} \\ &+ \frac{2000 \text{ N} \times 9000 \text{ mm}}{31.2 \times 10^3 \text{ mm}^2 \times 210 \times 10^3 \text{ N/mm}^2} (1) \\ &+ \left(\frac{\left(\frac{2000 \text{ N} \times 12,728 \text{ mm}}{9000 \text{ mm}} \right) 12,728 \text{ mm}}{31.2 \times 10^2 \text{ mm}^2 \times 210 \times 10^3 \text{ N/mm}^2} \right) \times \frac{12,728 \text{ mm}}{9000 \text{ mm}} \\ &+ \left(\frac{\left(\frac{1000 \text{ N} \times 7000 \text{ mm} + 2000 \text{ N} \times 9000 \text{ mm}}{9000 \text{ mm}} \right) 9000 \text{ mm}}{31.2 \times 10^2 \text{ mm}^2 \times 210 \times 10^3 \text{ N/mm}^2} \right) \times \frac{9000 \text{ mm}}{9000 \text{ mm}} + 0.00646 \text{ mm}^* \\ &+ \frac{3000 \text{ N} \times 9000 \text{ mm}}{31.2 \times 10^3 \text{ mm}^2 \times 210 \times 10^3 \text{ N/mm}^2} (1) \\ &+ \left(\frac{\left(\frac{3000 \text{ N} \times 11,780 \text{ mm}}{9000 \text{ mm}} \right) 11,780 \text{ mm}}{31.2 \times 10^2 \text{ mm}^2 \times 210 \times 10^3 \text{ N/mm}^2} \right) \times \frac{11,780 \text{ mm}}{9000 \text{ mm}} + 0.0382 \text{ mm}^* \\ &+ \left(\frac{\left(\frac{1000 \text{ N} \times 7000 \text{ mm} + 2000 \text{ N} \times 9000 \text{ mm} + 3000 \text{ N} \times 7600 \text{ mm}}{9000 \text{ mm}} \right) 7600 \text{ mm}}{31.2 \times 10^2 \text{ mm}^2 \times 210 \times 10^3 \text{ N/mm}^2} \right) \times \frac{7600 \text{ mm}}{9000 \text{ mm}} \end{aligned}$$

* BASED ON

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$$\sigma_h = 0.0137 + 0.0279 + 0.00646 + 0.0274 + 0.0778 + 0.0382 + 0.00646$$

$$+ 0.0411 + 0.0924 + 0.0382 + 0.052$$

$$\sigma_h = 0.42 \text{ mm}$$