

# SAFE LOAD TABLE

## 6" x 16" Flexicore<sup>®</sup> SECTION

MAXIMUM SAFE SUPERIMPOSED\* UNIFORMLY DISTRIBUTED WORKING LOADS  
IN POUNDS PER SQUARE FOOT OF AREA

(SLABS DESIGNED FOR  
45-50 PSI MAX.)

RR 1997

| STD.<br>DESIG. | SPANS IN FEET AND INCHES |       |       |       |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        |        | BOTTOM STEEL PER 16" UNIT |        |                                          |              |
|----------------|--------------------------|-------|-------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------------------------|--------|------------------------------------------|--------------|
|                | 8'-0"                    | 8'-6" | 9'-0" | 9'-6" | 10'-0" | 10'-6" | 11'-0" | 11'-6" | 12'-0" | 12'-6" | 13'-0" | 13'-6" | 14'-0" | 14'-6" | 15'-0" | 15'-6" | 16'-0" | 16'-6" | 17'-0" | 17'-6" | 18'-0" | 18'-6" | 19'-0" | 19'-6" | 20'-0" | 20'-6" | 21'-0" | 21'-6"                    | 22'-0" | CONTENT                                  | AREA—Sq. In. |
| S 99†          |                          |       | 484   | 429   | 383    | 343    | 308    | 278    | 252    | 228    | 208    | 191    | 173    | 158    | 145    | 132    | 122    | 112    | 102    | 94     | 86     | 79     | 73     | 67     | 61     | 56     | 51     | 47                        | 43     | 4- $\frac{9}{16}$ †                      | 0.994        |
| S 94           |                          | 521   | 459   | 408   | 364    | 325    | 292    | 263    | 238    | 216    | 196    | 179    | 163    | 149    | 136    | 124    | 114    | 104    | 96     | 88     | 80     | 74     | 67     | 62     | 56     | 51     | 47     | 43                        | 39     | 3- $\frac{9}{16}$ † & 1- $\frac{1}{2}$ † | 0.942        |
| S 89           | 560                      | 490   | 433   | 383   | 342    | 305    | 274    | 247    | 224    | 202    | 184    | 166    | 152    | 138    | 126    | 115    | 105    | 96     | 88     | 81     | 74     | 67     | 61     | 56     | 51     | 46     | 42     | 38                        | 34     | 2- $\frac{9}{16}$ † & 2- $\frac{1}{2}$ † | 0.890        |
| S 84           | 526                      | 460   | 406   | 360   | 320    | 286    | 257    | 230    | 208    | 188    | 170    | 155    | 141    | 128    | 117    | 106    | 97     | 88     | 81     | 74     | 67     | 61     | 55     | 50     | 46     | 41     | 37     | 33                        | 30     | 3- $\frac{1}{2}$ † & 1- $\frac{9}{16}$ † | 0.837        |
| S 79           | 491                      | 430   | 378   | 335   | 298    | 266    | 238    | 214    | 192    | 174    | 157    | 143    | 129    | 118    | 107    | 97     | 88     | 80     | 73     | 66     | 60     | 54     | 49     | 44     | 40     | 36     | 32     | 28                        | 25     | 4- $\frac{1}{2}$ †                       | 0.785        |
| S 74           | 460                      | 403   | 354   | 313   | 278    | 248    | 222    | 199    | 179    | 161    | 146    | 132    | 119    | 108    | 98     | 89     | 81     | 73     | 66     | 60     | 54     | 49     | 44     | 39     | 35     | 31     | 27     | 24                        | 21     | 3- $\frac{1}{2}$ † & 1- $\frac{7}{16}$ † | 0.739        |
| S 69           | 430                      | 376   | 330   | 292   | 259    | 230    | 206    | 184    | 166    | 149    | 134    | 121    | 109    | 99     | 89     | 81     | 73     | 66     | 59     | 54     | 48     | 43     | 38     | 34     | 30     | 27     | 23     | 20                        |        | 2- $\frac{1}{2}$ † & 2- $\frac{7}{16}$ † | 0.693        |
| S 65           | 399                      | 348   | 306   | 270   | 239    | 212    | 190    | 169    | 152    | 136    | 123    | 110    | 99     | 89     | 81     | 73     | 65     | 59     | 53     | 47     | 42     | 37     | 33     | 29     | 25     | 22     | 19     |                           |        | 3- $\frac{7}{16}$ † & 1- $\frac{1}{2}$ † | 0.647        |
| S 60           | 367                      | 320   | 280   | 247   | 218    | 194    | 172    | 154    | 138    | 123    | 110    | 99     | 89     | 80     | 71     | 64     | 57     | 51     | 46     | 40     | 36     | 31     | 27     | 23     | 20     |        |        |                           |        | 4- $\frac{7}{16}$ †                      | 0.601        |
| S 56           | 340                      | 296   | 260   | 228   | 202    | 178    | 158    | 141    | 126    | 112    | 100    | 90     | 80     | 72     | 64     | 57     | 51     | 45     | 40     | 35     | 30     | 26     | 23     | 19     |        |        |        |                           |        | 3- $\frac{7}{16}$ † & 1- $\frac{3}{8}$ † | 0.561        |
| S 52           | 315                      | 274   | 239   | 210   | 185    | 164    | 145    | 129    | 114    | 102    | 91     | 81     | 72     | 64     | 57     | 50     | 44     | 39     | 34     | 29     | 25     | 21     |        |        |        |        |        |                           |        | 2- $\frac{7}{16}$ † & 2- $\frac{3}{8}$ † | 0.522        |
| S 48           | 288                      | 249   | 218   | 190   | 168    | 147    | 130    | 115    | 102    | 91     | 80     | 71     | 63     | 56     | 49     | 43     | 37     | 32     | 28     | 24     | 20     |        |        |        |        |        |        |                           |        | 3- $\frac{3}{8}$ † & 1- $\frac{7}{16}$ † | 0.482        |
| S 44           | 260                      | 226   | 196   | 171   | 150    | 132    | 116    | 102    | 90     | 79     | 70     | 62     | 54     | 47     | 41     | 36     | 31     | 26     | 22     | 18     |        |        |        |        |        |        |        |                           |        | 4- $\frac{3}{8}$ †                       | 0.442        |

\*INCLUDES THE LIVE LOAD PLUS ANY DEAD LOAD THAT IS ADDITIONAL TO THE WEIGHT OF THE BARE GROUTED SLABS IN PLACE.

† "BALANCED SLAB", SAFE LOADS FOR GREATER STEEL CONTENT MUST NOT BE EXTRAPOLATED. BALANCED SLAB HAS 0.99 SQ. IN. OF STEEL.

### REMARKS

1. Safe superimposed  $W = \frac{6M}{L^2} - 45.8$  lb. (W in lb. per sq. ft. of area.)
2. The maximum span without stirrups =  $\frac{2080}{W_D + L}$ . With stirrups used it is  $\frac{5547}{W_D + L}$ .
3. The table is based upon dead load and grout of 61 lb. pcf.
4. Stirrups are needed for all loadings above the heavy dashed line.
5. Loadings shown in light figures indicate deflections in excess of  $\frac{1}{360}$  of the span.

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