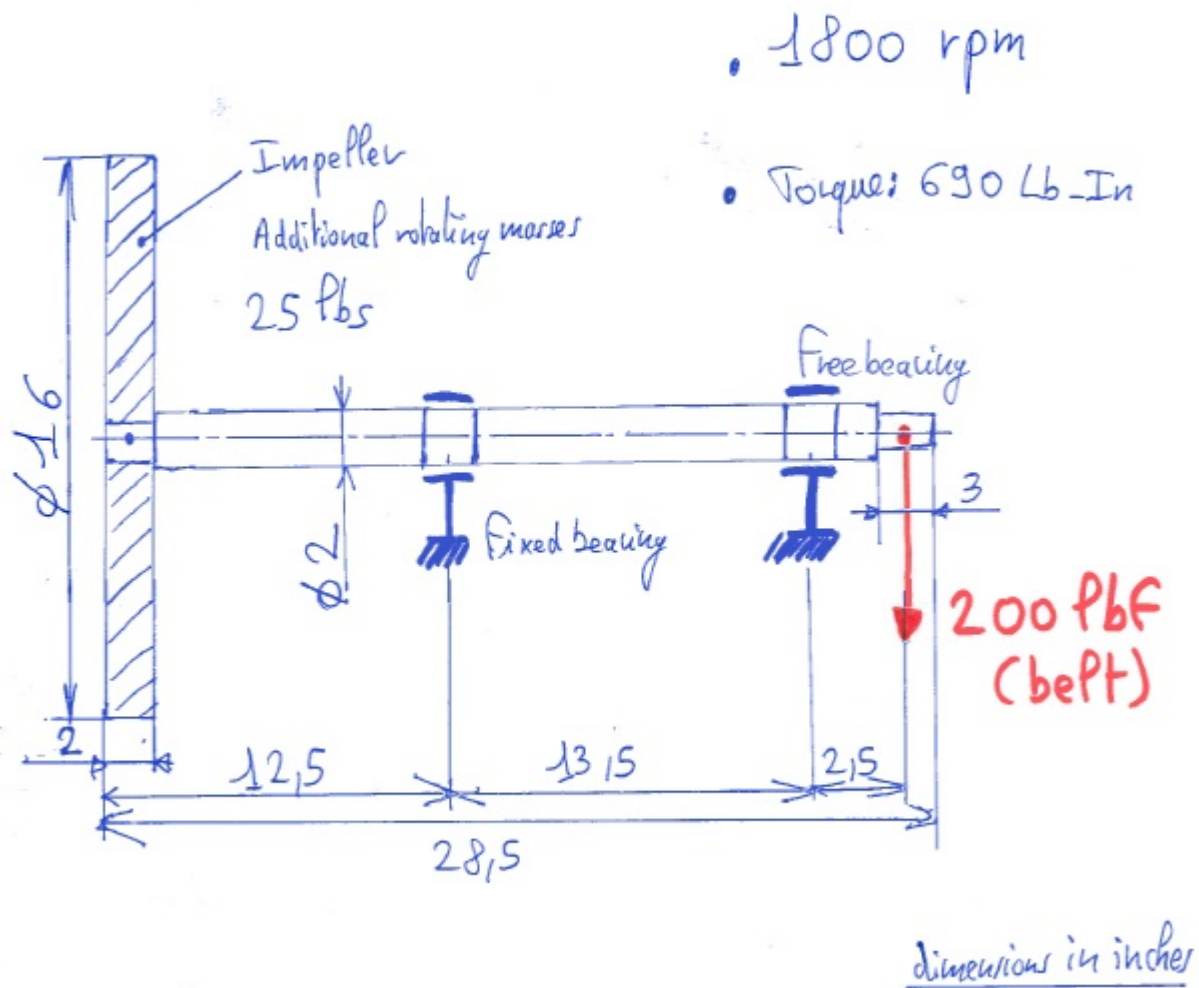
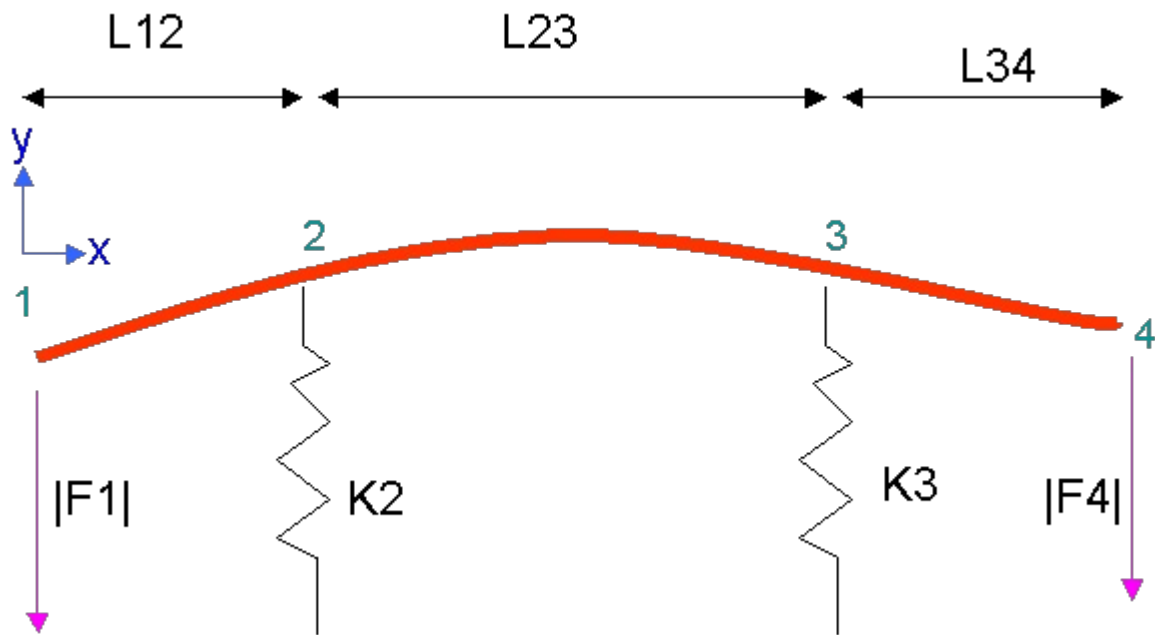


Model system to analyse Static Deflections:
Version 15: $K_2 = K_3 =$



Simplified Model. Neglect weight of shaft



Note displacements and forces are positive in the upward direction. The applied forces shown happen to have negative values.

=====Symbols=====

x = longitudinal coordinate

y = radial coordinate

V(x) = Shear due to force F1

M(x) = Moment due to force F1

T(x) = Slope (Theta) due to force F1

Y(x) = Displacement due to force F1

VV(x) = Shear due to force F2

MM(x) = Moment due to force F2

TT(x) = Slope (Theta) due to force F2

YY(x) = Displacement due to force F2

Initialization:

```
[ reset()
[ assume(L12>0); assume(L23>0); assume(L34>0); assume(F1>0);
[ assume(K2>0); assume(K3>0);
[ use(linalg)
Warning: 'htranspose' already has a value, not exported. [use]
Warning: 'transpose' already has a value, not exported. [use]
Warning: 'det' already has a value, not exported. [use]
```

==== PART 1 - Find deflections due to force F1 =====

For the first part, we want to determine alpha11 and alpha14.

We will apply force F1 upwards at point 1 and compute the response displacements Y1 and Y4

Then alpha11 = Y1/F1 and alpha14 = Y4/F1

Note we must assume $F_4=0$ during this part! (That's a helpful simplifier)

Find R_3 based on moment balance about point 2

$$\begin{aligned} & R_3 := \text{solve}(F_1 * L_{12} = R_3 * L_{23}, R_3) [1] \\ & \frac{F_1 L_{12}}{L_{23}} \end{aligned}$$

Find R_2 based on Force balance:

$$\begin{aligned} & R_2 := \text{solve}(F_1 + R_2 + R_3 = 0, R_2) [1] \\ & -F_1 - \frac{F_1 L_{12}}{L_{23}} \end{aligned}$$

Double check the moment balance about point 3 is satisfied

$$\begin{aligned} & \text{simplify}(F_1 * (L_{12} + L_{23}) + R_2 * L_{23}) \\ & 0 \end{aligned}$$

Double check passes!

Check forces sum to zero

$$\begin{aligned} & F_1 + R_2 + R_3 \\ & 0 \end{aligned}$$

Check passes!

Write the Shear function as integration of applied forces

$$\begin{aligned} & V(x) := \text{simplify}(F_1 * \text{heaviside}(x) + R_2 * \text{heaviside}(x - L_{12}) + R_3 * \text{heaviside}(x - (L_{12} + L_{23}))) \\ & \frac{F_1 (L_{23} \text{heaviside}(x) - L_{23} + L_{12} \text{heaviside}(L_{12} - x) + L_{23} \text{heaviside}(L_{12} - x) - L_{12} \text{heaviside}(L_{12} + L_{23}))}{L_{23}} \end{aligned}$$

Write Moment as integration of shear, with unknown integ constant "M0"

$$\begin{aligned} & M(x) := \text{simplify}(\text{int}(V(x), x)) + M_0 \\ & M_0 - F_1 x - F_1 \text{heaviside}(L_{12} - x) (L_{12} - x) + F_1 x \text{heaviside}(x) - \frac{F_1 L_{12} \text{heaviside}(L_{12} - x) (L_{12} - x)}{L_{23}} + \dots \end{aligned}$$

Solve M_0 based on B.C. that moment is zero at/beyond point 3

$$\begin{aligned} & M_0 := \text{solve}((M(x) | x = L_{12} + L_{23}) = 0, M_0) [1] \\ & 0 \end{aligned}$$

As a double check, make sure the moment at left end is also zero:

$$\begin{aligned} & M(x) | x = 0 \\ & \frac{F_1 L_{12} (L_{12} + L_{23})}{L_{23}} - \frac{F_1 L_{12}^2}{L_{23}} - F_1 L_{12} \end{aligned}$$

Check passes

[

Solve slope T(x) (slope) by integrating M(x) and multiplying 1/EI, with integ const "T0"

```
T(x):=int(M(x),x)/EI+T0
T0 + 
$$\frac{\frac{F1 x^2 \text{heaviside}(x)}{2} - \frac{F1 x^2}{2} + \frac{F1 \text{heaviside}(L12-x) (L12-x)^2}{2} - \frac{F1 L12 \text{heaviside}(L12+L23-x) (L12+L23-x)^2}{2 L23} + \frac{F1 L12 \text{heaviside}(L12-x) (L12-x)^2}{2}}{EI}$$

T(x):=simplify(T(x))
T0 + 
$$\frac{\frac{F1 x^2 \text{heaviside}(x)}{2} - \frac{F1 x^2}{2} + \frac{F1 \text{heaviside}(L12-x) (L12-x)^2}{2} - \frac{F1 L12 \text{heaviside}(L12+L23-x) (L12+L23-x)^2}{2 L23} + \frac{F1 L12 \text{heaviside}(L12-x) (L12-x)^2}{2}}{EI}$$

//T(x):=simplify(1/EI/I1*int(M(x),x))+T0
```

Solve Y(x) as integral of T(x), with integration const "Y0"

```
Y(x):=int(T(x),x) + Y0
Y0 + T0 x - 
$$\frac{F1 x^3}{6 EI} + \frac{F1 x^3 \text{heaviside}(x)}{6 EI} - \frac{F1 \text{heaviside}(L12-x) (L12-x)^3}{6 EI} - \frac{F1 L12 \text{heaviside}(L12-x) (L12-x)^3}{6 EI L23} + \frac{F1 L12 \text{heaviside}(L12+L23-x) (L12+L23-x)^3}{6 EI L23}$$

Y(x):=simplify(Y(x))
Y0 + T0 x - 
$$\frac{F1 x^3}{6 EI} + \frac{F1 x^3 \text{heaviside}(x)}{6 EI} - \frac{F1 \text{heaviside}(L12-x) (L12-x)^3}{6 EI} - \frac{F1 L12 \text{heaviside}(L12-x) (L12-x)^3}{6 EI L23} + \frac{F1 L12 \text{heaviside}(L12+L23-x) (L12+L23-x)^3}{6 EI L23}$$

```

Solve Y0, T0 using force/displacement equations at points 2 and 3

```
eq1:=(Y(x)|(x=L12)) = -R2/K2
Y0 + L12 T0 + 
$$\frac{F1 L12 L23^2}{6 EI} = \frac{F1 + \frac{F1 L12}{L23}}{K2}$$

eq2:=(Y(x)|(x=L12+L23)) = - R3/K3
Y0 + T0 (L12 + L23) = 
$$-\frac{F1 L12}{K3 L23}$$

Y0T0soln:=simplify(solve({eq1,eq2},{Y0,T0}));

$$\left\{ \left[ T0 = -\frac{F1 (-K2 K3 L12 L23^3 + 6 EI K3 L23 + 6 EI K2 L12 + 6 EI K3 L12)}{6 EI K2 K3 L23^2}, Y0 = \frac{F1 (6 EI K2 L12^2 + 6 EI K3 L12^2 + 6 EI K3 L23^2 - K2 K3 L12^2 L23^3 + 12 EI K3 L12 L23 - K2 K3 L12 L23)}{6 EI K2 K3 L23^2} \right] \right\}$$

Y0:=simplify(Y0|Y0T0soln)

$$\frac{F1 (6 EI K2 L12^2 + 6 EI K3 L12^2 + 6 EI K3 L23^2 - K2 K3 L12^2 L23^3 + 12 EI K3 L12 L23 - K2 K3 L12 L23)}{6 EI K2 K3 L23^2}$$

T0:=simplify(T0|Y0T0soln)

$$-\frac{F1 (-K2 K3 L12 L23^3 + 6 EI K3 L23 + 6 EI K2 L12 + 6 EI K3 L12)}{6 EI K2 K3 L23^2}$$

```

```
[ simplify(lhs(eq1)-rhs(eq1))
0
[ simplify(lhs(eq2)-rhs(eq2))
0
```

==== Part 2 - find equations for VV, MN, TT, YY from symmetry and similar approach as part 1

```
[ // Find R2 based on moment balance about point 3
[ R2:=solve(F4*L34=R2*L23,R2)[1]:
[ // Find R2 based on Force balance
[ R3:=solve(F4+R2+R3=0,R3)[1]:
[ VV(x):=simplify(F4*heaviside(x-(L12+L23+L34))+R2*heaviside(x-L12)+R3*heaviside(x-L12-L23))
[ MM(x):=simplify(int(VV(x),x))+MM0:
[ MM0:=solve( (MM(x)|x=L12) = 0, MM0)[1]:
[ TT(x):=int(MM(x),x)/EI+TT0:
[ TT(x):=simplify(TT(x)):
[ YY(x):=int(TT(x),x) + YY0:
[ YY(x):=simplify(YY(x)):
[ eq1:=(YY(x)|(x=L12)) = -R2/K2:
[ eq2:=(YY(x)|(x=L12+L23)) = - R3/K3:
[ YY0TT0soln:=simplify(solve({eq1,eq2},{YY0,TT0})):
[ YY0:=simplify(YY0|YY0TT0soln):
[ TT0:=simplify(TT0|YY0TT0soln):
```

Assign values in MKS system

```
[ L12:=11.5/39.37
0.2921005842
[ L23:=13.5/39.37
0.3429006858
[ L34:=2.5/39.37
0.063500127
[ Ltot:=L12+L23+L34
0.698501397
[ D1:=2/39.37 // diameter
0.0508001016
[ F1:=-25*4.44
```

```

[ -111.0
[ F4:=-200*4.44
[ -888.0
[ E1:=2.3E11
[ 2.3 1011
[ I1:=float(PI)*D1^4/64
[ 0.0000003269100125
[ EI:=E1*I1
[ 75189.30287
[ K2:=1E10
[ 10000000000.0
[ K3:=K2
[ 10000000000.0

=====Plot=====
plot(plot::Function2d(V(x),x=0..Ltot,Color=RGB::Red,Legend = "Shear from F1",
plot::Function2d(VV(x),x=0..Ltot,Color=RGB::Blue,Legend = "Shear from F4"),
plot::Function2d(V(x)+VV(x),x=0..Ltot,Color=RGB::Black,LineStyle = Dashed,1
,Header="Shear")

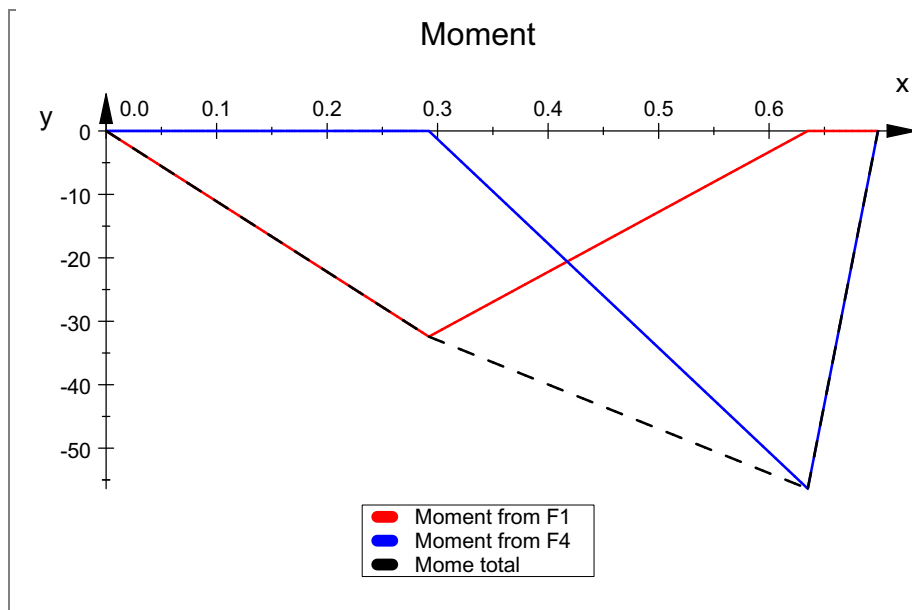
Shear

y
800
600
400
200
0
0.1 0.2 0.3 - - 0.4 - - 0.5 - - 0.6
x

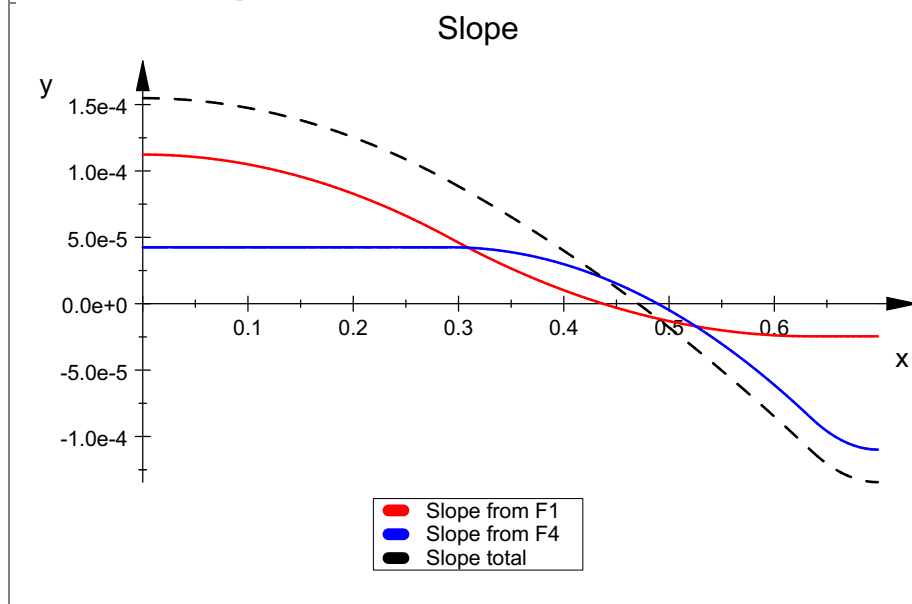
Shear from F1
Shear from F4
Shear total

plot(plot::Function2d(M(x),x=0..Ltot,Color=RGB::Red,Legend = "Moment from F1",
plot::Function2d(MM(x),x=0..Ltot,Color=RGB::Blue,Legend = "Moment from F4"),
plot::Function2d(M(x)+MM(x),x=0..Ltot,Color=RGB::Black,LineStyle = Dashed,1
,Header="Moment")

```

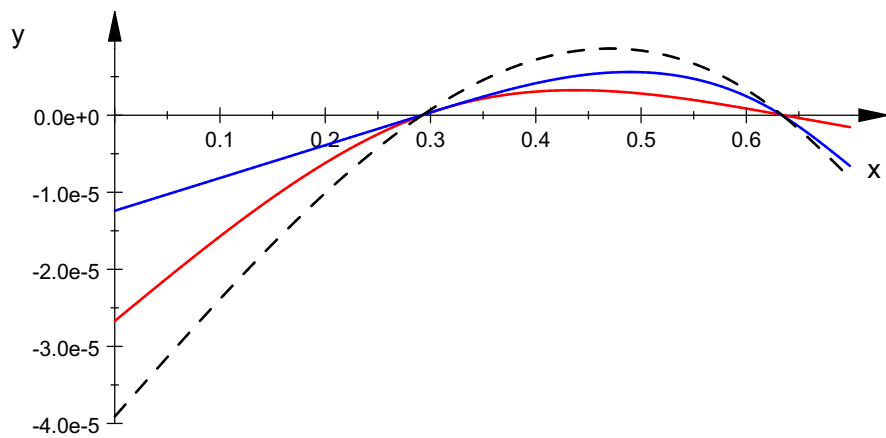


```
T(x):=simplify(T(x)|K23=K23): // needed simplification for plot to work
TT(x):=simplify(TT(x)|K23=K23): // needed simplification for plot to work
plot(plot::Function2d(T(x),x=0..Ltot,Color=RGB::Red,Legend = "Slope from F1",
plot::Function2d(TT(x),x=0..Ltot,Color=RGB::Blue,Legend = "Slope from F4"),
plot::Function2d(T(x)+TT(x),x=0..Ltot,Color=RGB::Black,LineStyle = Dashed,1
,Header="Slope")
```



```
Y(x):=simplify(Y(x))|L23=L23: // required for plot to work
YY(x):=simplify(YY(x))|L23=L23: // required for plot to work
plot(plot::Function2d(Y(x),x=0..Ltot,Color=RGB::Red,Legend = "Disp from F1",
plot::Function2d(YY(x),x=0..Ltot,Color=RGB::Blue,Legend = "Disp from F4"),
plot::Function2d(Y(x)+YY(x),x=0..Ltot,Color=RGB::Black,LineStyle = Dashed,1
,Header="Displacement, (K = ".expr2text(K2)." per brg)"))
```

Displacement, (K = 10000000000.0 per brg)



Disp from F1
Disp from F4
Disp total