

At the support:  $z := 0 \text{ ft}$

For Case 3, from Appendix C for  $0 < z < \alpha L$ :

$$\begin{aligned}\theta(z) &:= \frac{T \cdot L}{G_s \cdot J} \cdot \left[ (1 - \alpha) \cdot \frac{z}{L} + \frac{a}{L} \cdot \left( \sinh\left(\frac{\alpha \cdot L}{a}\right) + \tanh\left(\frac{L}{a}\right) - \cosh\left(\frac{\alpha \cdot L}{a}\right) \right) \cdot \sinh\left(\frac{z}{a}\right) \right] \\ \theta'(z) &:= \frac{T \cdot L}{(G_s \cdot J)} \cdot \left[ \frac{(1 - \alpha)}{L} + \frac{1}{L} \cdot \left( \sinh\left(\frac{\alpha \cdot L}{a}\right) + \tanh\left(\frac{L}{a}\right) - \cosh\left(\frac{\alpha \cdot L}{a}\right) \right) \cdot \cosh\left(\frac{z}{a}\right) \right] \\ \theta''(z) &:= \frac{T}{(G_s \cdot J)} \cdot \left( \sinh\left(\frac{\alpha \cdot L}{a}\right) + \tanh\left(\frac{L}{a}\right) - \cosh\left(\frac{\alpha \cdot L}{a}\right) \right) \cdot \frac{1}{a} \cdot \sinh\left(\frac{z}{a}\right) \\ \theta'''(z) &:= \frac{T}{(G_s \cdot J)} \cdot \left( \sinh\left(\frac{\alpha \cdot L}{a}\right) + \tanh\left(\frac{L}{a}\right) - \cosh\left(\frac{\alpha \cdot L}{a}\right) \right) \cdot \frac{1}{a^2} \cdot \cosh\left(\frac{z}{a}\right)\end{aligned}$$

$$\frac{T \cdot L}{(G_s \cdot J)} = 0.28$$

$$\theta'(0) = 0.0119 \text{ ft}^{-1}$$

$$\frac{(1 - \alpha)}{L} = 0.0441 \text{ ft}^{-1}$$

$$\sinh\left(\frac{\alpha \cdot L}{a}\right) + \tanh\left(\frac{L}{a}\right) = 29.50$$

$$V_{\text{sup}} := R \quad V_{\text{sup}} = 0.83 \text{ kips}$$

$$\cosh\left(\frac{\alpha \cdot L}{a}\right) = 29.51$$

$$\text{Flange stress, due to beam action: } \tau_{bf} := \frac{V_{\text{sup}} \cdot Q_f}{I_x \cdot t_f} \quad \tau_{bf} = 0.14 \text{ ksi} \quad \cosh\left(\frac{z}{a}\right) = 1.00$$

$$\text{Web stress, due to beam action: } \tau_{bw} := \frac{V_{\text{sup}} \cdot Q_w}{I_x \cdot t_w} \quad \tau_{bw} = 0.26 \text{ ksi}$$

$$\text{Flange stress, due to St. Venant torsion: } \tau_{tf} := G_s \cdot t_f \cdot \theta'(z) \quad \tau_{tf} = 4.53 \text{ ksi}$$

$$\text{Web stress, due to St. Venant torsion: } \tau_{tw} := G_s \cdot t_w \cdot \theta'(z) \quad \tau_{tw} = 4.97 \text{ ksi}$$

$$\text{Flange stress, due to warping torsion: } \tau_{w1} := -\frac{E_s \cdot S_{w1} \cdot \theta'''(z)}{t_f} \quad \tau_{w1} = 0.02 \text{ ksi}$$

$$\text{Flange stress, due to warping torsion: } \tau_{w2} := -\frac{E_s \cdot S_{w2} \cdot \theta'''(z)}{t_f} \quad \tau_{w2} = 0.02 \text{ ksi}$$

$$\text{Web stress, due to warping torsion: } \tau_{w3} := -\frac{E_s \cdot S_{w3} \cdot \theta'''(z)}{t_w} \quad \tau_{w3} = 0.01 \text{ ksi}$$

Note: The stresses are not necessarily additive, but for simplicity and conservatism, I will add all the stresses.

$$\text{Flange stress: } f_{vf} := \tau_{tf} + \tau_{w1} + \tau_{bf} \quad f_{vf} = 4.7 \text{ ksi} \quad F_v(h, t_w) = 12.0 \text{ ksi}$$

$$\text{Web stress: } f_{vw} := \tau_{tw} + \tau_{bw} + \tau_{w3} \quad f_{vw} = 5.2 \text{ ksi}$$

$$\text{if}(\max(f_{vf}, f_{vw}) \leq F_v(h, t_w), \text{OK, NG}) = \text{"O.K."}$$