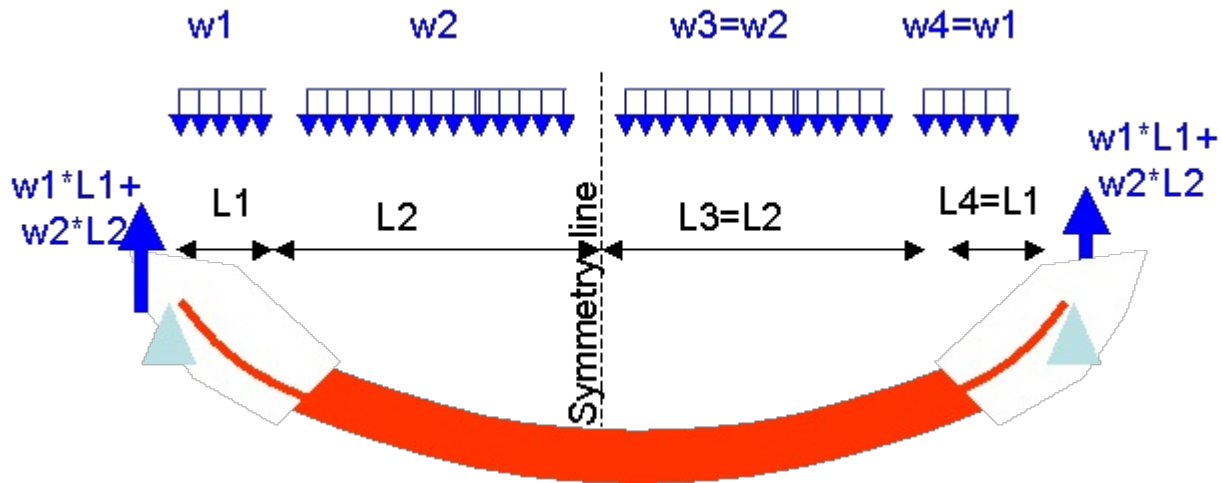


Objective: Analyse static deflection from gravity



Since the problem is symmetric about the center, we need only solve the left side.

Symbols

x = axial coordinate. $x=0$ at LHS

w_1, w_2 = weight per length in regions 1 and 2

$V_1(x), V_2(x)$ = Beam shear at position x in regions 1 and 2

$M_1(x), M_2(x)$ = Beam moment at position x in regions 1 and 2

$T_1(x), T(x)$ = Beam slope at position x in regions 1 and 2 (T stands for "Theta")

$Y_1(x), Y_2(x)$ = Beam displacement at position x in regions 1 and 2

Subscripts 1 and 2 - refer to region 1 (thin) and region 2 (thick) of beam defined by L_1 and L_2

E_s = Young's Modulus of steel

I = Diametral Moment of Inertia

CV_2 - integration constant associated with $V_2(x)$

CM_2 - integration constant associated with $M_2(x)$

CT_1, CT_2 - integration constants associated with $T_1(x), T_2(x)$

CY_1, CY_2 - integration constant associated with $Y_2(x)$

A_1, A_2 = area in sections 1 and 2

Eq1, Eq2, Eq3, Eq4, Eq5, Eq6 - 6 boundary conditions used to solve 6 unknowns constants.

All items in SI units

Initialize:

```
[ reset ()
```

Shear starts at $(w_1*L_1 + w_2*L_2)$ and decreases with slope w :

```
[ V1(x) := -w1*x + (w1*L1 + w2*L2) // value at x=0 is w1*L1 + w2*L2
```

```
[ L1 w1 + L2 w2 - w1 x
```

```
[ V2(x) := -w2*x + CV2
```

```
[ CV2 - w2 x
```

```
[ M1(x) := int(V1(x), x); // moment is 0 at LHS -> integration constant is 0
```

```
[ x (L1 w1 + L2 w2) - \frac{w1 x^2}{2}
```

```
[ M2(x) := int(V2(x), x) + CM2
```

$$\begin{aligned}
& \left[-\frac{w_2 x^2}{2} + CV_2 x + CM_2 \right. \\
& T1(x) := (1/E_s/I_1) * \int (M1(x), x) + CT_1 \\
& \left. CT_1 - \frac{\frac{w_1 x^3}{6} - x^2 \left(\frac{L_1 w_1}{2} + \frac{L_2 w_2}{2} \right)}{E_s I_1} \right. \\
& T2(x) := (1/E_s/I_2) * \int (M2(x), x) + CT_2 \\
& \left. CT_2 + \frac{-\frac{w_2 x^3}{6} + \frac{CV_2 x^2}{2} + CM_2 x}{E_s I_2} \right. \\
& Y1(x) := \int (T1(x), x) + CY_1; \quad // CY_1 = 0 \text{ since } Y1 = 0 \text{ @ } x = 0 \\
& \left. CY_1 + CT_1 x + \frac{x(4 L_1 w_1 x^2 - w_1 x^3 + 4 L_2 w_2 x^2)}{24 E_s I_1} \right. \\
& Y2(x) := \int (T2(x), x) + CY_2; \\
& \left. CY_2 + CT_2 x + \frac{CM_2 x^2}{2 E_s I_2} + \frac{CV_2 x^3}{6 E_s I_2} - \frac{w_2 x^4}{24 E_s I_2} \right]
\end{aligned}$$

List 6 boundary conditions (Eq1, Eq2, Eq3, Eq4, Eq5, Eq6)

$$\begin{aligned}
& Eq1 := (T2(x) | x=L1+L2) = 0 \quad // 0 \text{ slope @ rhs} \\
& \left[CT_2 + \frac{CM_2 (L1 + L2) - \frac{w_2 (L1+L2)^3}{6} + \frac{CV_2 (L1+L2)^2}{2}}{E_s I_2} = 0 \right. \\
& Eq2 := (Y1(x) | x=0) = 0 \\
& \left[CY_1 = 0 \right. \\
& Eq3 := (Y1(x) | x=L1) = (Y2(x) | x=L1) \quad // \text{ continuity of displacement @ } x=L1 \\
& \left[CY_1 + CT_1 L1 + \frac{L1(3 w_1 L1^3 + 4 L2 w_2 L1^2)}{24 E_s I_1} = CY_2 + CT_2 L1 + \frac{CM_2 L1^2}{2 E_s I_2} + \frac{CV_2 L1^3}{6 E_s I_2} - \frac{L1^4 w_2}{24 E_s I_2} \right. \\
& Eq4 := (T1(x) | x=L1) = (T2(x) | x=L1) \quad // \text{ continuity of slope @ } x=L1 \\
& \left[CT_1 - \frac{\frac{L1^3 w_1}{6} - L1^2 \left(\frac{L1 w_1}{2} + \frac{L2 w_2}{2} \right)}{E_s I_1} = CT_2 + \frac{-\frac{w_2 L1^3}{6} + \frac{CV_2 L1^2}{2} + CM_2 L1}{E_s I_2} \right. \\
& Eq5 := (M1(x) | x=L1) = (M2(x) | x=L1) \quad // \text{ continuity of moment @ } x=L1 \\
& \left[L1(L1 w_1 + L2 w_2) - \frac{L1^2 w_1}{2} = -\frac{w_2 L1^2}{2} + CV_2 L1 + CM_2 \right. \\
& Eq6 := (V1(x) | x=L1) = (V2(x) | x=L1) \quad // \text{ continuity of shear @ } x=L1 \\
& \left[L2 w_2 = CV_2 - L1 w_2 \right]
\end{aligned}$$

Solve 6 above equations in 6 unknowns (CY2, CT1, CT2, CM2, CV2, CY1)

$$\text{solution} := \text{solve}(\{Eq1, Eq2, Eq3, Eq4, Eq5, Eq6\}, \{CY_2, CT_1, CT_2, CM_2, CV_2, CY_1\});$$

Display solution results for unknown integration constants:

$$\begin{aligned}
& CY2 := CY_2 | \text{solution} \\
& \left[-\frac{I_1 L1^4 w_2 - 6 I_1 L1^4 w_1 + 5 I_2 L1^4 w_1 - 8 I_1 L1^3 L2 w_2 + 8 I_2 L1^3 L2 w_2}{24 E_s I_1 I_2} \right. \\
& CT1 := CT_1 | \text{solution}
\end{aligned}$$

$$-\frac{2 I_2 L_1^3 w_1 + 2 I_1 L_2^3 w_2 + 3 I_1 L_1^2 L_2 w_1 + 6 I_1 L_1 L_2^2 w_2 + 3 I_2 L_1^2 L_2 w_2}{6 E_s I_1 I_2}$$

CT2:=CT2|solution

$$-\frac{3 L_1^3 w_1 - L_1^3 w_2 + 2 L_2^3 w_2 + 3 L_1^2 L_2 w_1 + 6 L_1 L_2^2 w_2 + 3 L_1^2 L_2 w_2}{6 E_s I_2}$$

CM2:=CM2|solution

$$\frac{L_1^2 w_1}{2} - \frac{L_1^2 w_2}{2}$$

CV2:=CV2|solution

$$L_1 w_2 + L_2 w_2$$

CY1:=CY1|solution

$$0$$

Now we have the solution for displacement. We just need to find the numerical values and plug them in. The remainder of this file does that.

rho:=7750

$$7750$$

A1:=float(PI*0.0738^2/4)

$$0.004277623973$$

w1:=rho*A1*9.8

$$324.8855408$$

A2:=float(PI*0.2423^2/4)

$$0.04611016854$$

w2:=rho*A2*9.8

$$3502.067301$$

L1:=0.1801

$$0.1801$$

L2:=0.80060045

$$0.80060045$$

Es:=2.3E11

$$2.3 \cdot 10^{11}$$

I1:=float(PI*0.0738^4/64)

$$0.000001456113894$$

I2:=float(PI*0.24230673^4/64)

$$0.0001692122521$$

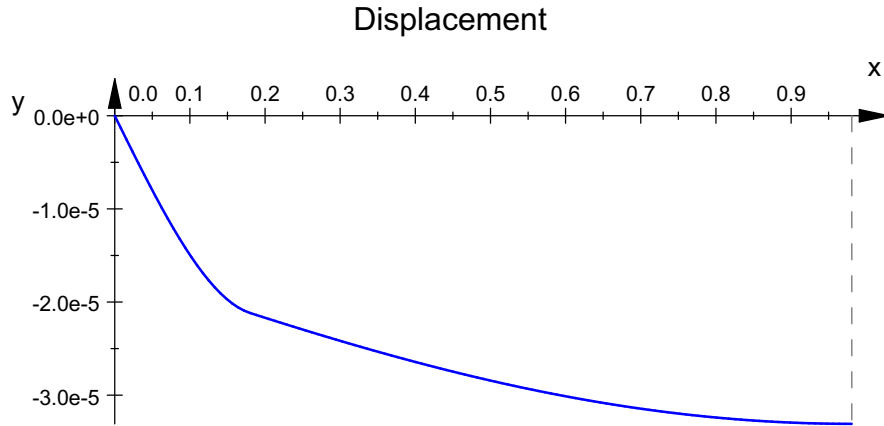
Here are the numerical values of the constants:

```
float(CY2), float(CT1), float(CT2), float(CM2), float(CV2)
-0.00001637595037, -0.0001635500671, -0.00002699286464, -51.52754967, 3434.478978
```

```
Y(x):=piecewise([x<L1,Y1(x)], [x<=L1+L2,Y2(x)])
```

$$\begin{cases} CY1 + CT1 x + \frac{x(4L1 w1 x^2 - w1 x^3 + 4L2 w2 x^2)}{24 Es I1} & \text{if } x < 0.1801 \\ CY2 + CT2 x + \frac{CM2 x^2}{2 Es I2} + \frac{CV2 x^3}{6 Es I2} - \frac{w2 x^4}{24 Es I2} & \text{if } x \leq 0.98070045 \end{cases}$$

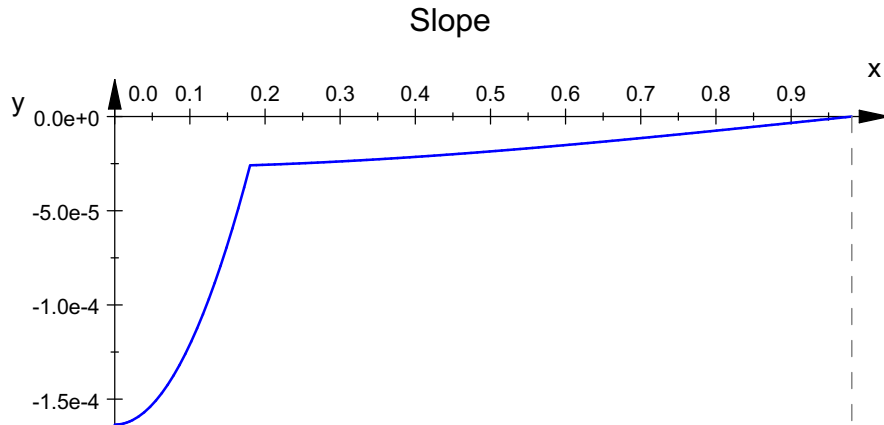
```
plot(Y(x), x=0..L1+L2, Header="Displacement")
```



```
T(x):=piecewise([x<L1,T1(x)], [x<=L1+L2,T2(x)]);
```

$$\begin{cases} CT1 - \frac{\frac{w1 x^3}{6} - x^2 \left(\frac{L1 w1}{2} + \frac{L2 w2}{2} \right)}{Es I1} & \text{if } x < 0.1801 \\ CT2 + \frac{-\frac{w2 x^3}{6} + \frac{CV2 x^2}{2} + CM2 x}{Es I2} & \text{if } x \leq 0.98070045 \end{cases}$$

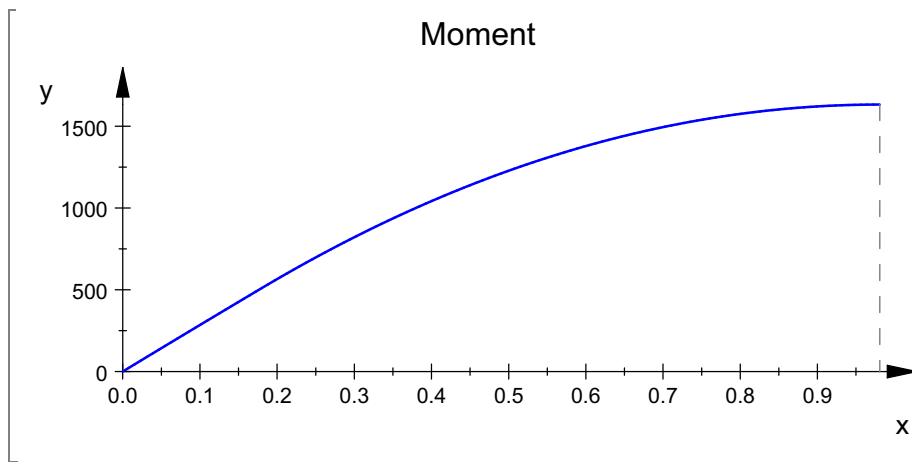
```
plot(T(x), x=0..L1+L2, Header="Slope")
```



```
M(x):=piecewise([x<L1,M1(x)], [x<=L1+L2,M2(x)]);
```

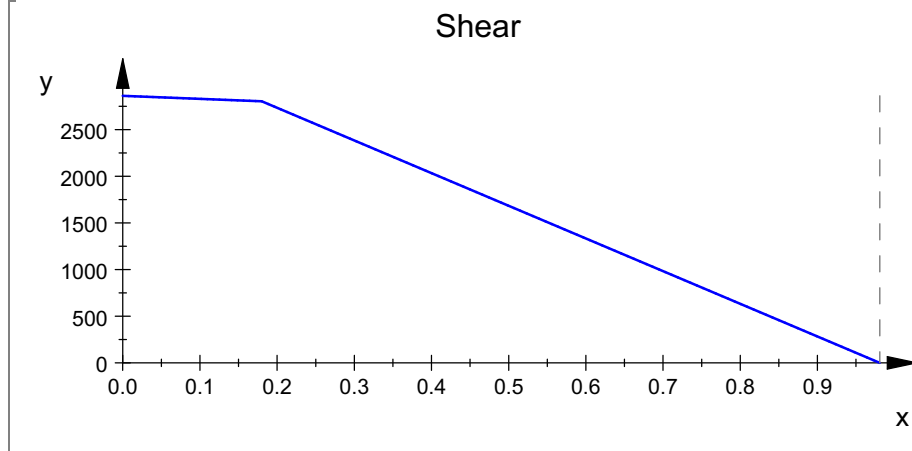
$$\begin{cases} x(L1 w1 + L2 w2) - \frac{w1 x^2}{2} & \text{if } x < 0.1801 \\ -\frac{w2 x^2}{2} + CV2 x + CM2 & \text{if } x \leq 0.98070045 \end{cases}$$

```
plot(M(x), x=0..L1+L2, Header="Moment")
```



```
V(x):=piecewise([x<L1,V1(x)],[x<=L1+L2,V2(x)]);
{ L1 w1 + L2 w2 - w1 x if x < 0.1801
  CV2 - w2 x          if x ≤ 0.98070045
```

```
plot(V(x),x=0..L1+L2,Header="Shear")
```



Do order-of-magnitude sanity check by computing natural frequency from static deflection using SDOF model

```
StaticDeflection:=Y2(x)|x=L1+L2
-0.00003308006744
Fnat:=float(sqrt(9.8/abs(StaticDeflection)))/2/PI
86.62634213
```

This is slightly less than calculated natural frequency of ~95hz. Since only the center of the beam moves 33 microns, it makes sense that the "effective" static deflection should be lower, which would give a higher natural frequency calculated from static deflection, closer to matching other natural frequency calc