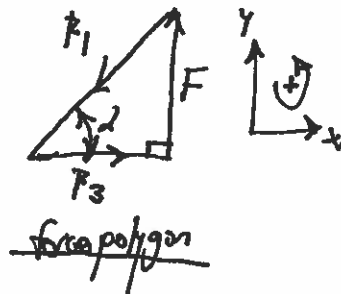
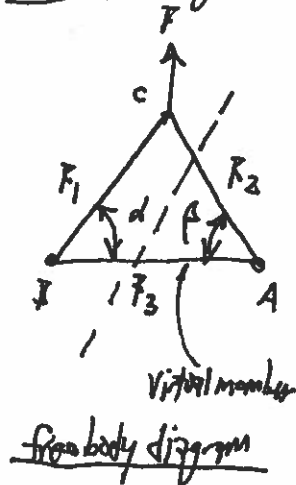
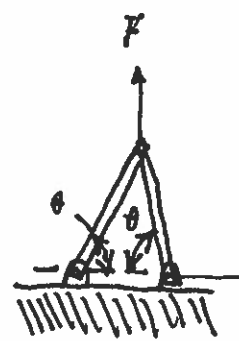


problem: compute member to symmetric truss arch.

note: the general case, 'virtual member' holding apart footings,

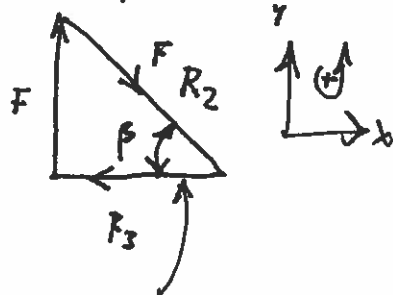


$F_x$	$F_y$
$F_1 \cos d$	$F_1 \sin d$
$F_3$	0
0	$F$
$\rightarrow \sum F_x$	$\uparrow \sum F_y$

$$\rightarrow \sum F_x = F_1 \cos d + F_3 = 0$$

$$\uparrow \sum F_y = F_1 \sin d + F = 0$$

force polygon



virtual member  
equi "p" opposite sense

$F_x$	$F_y$
$F_2 \cos(180-\beta)$	$F_2 \sin(180-\beta)$
$-F_3$	0
0	$F$
$\rightarrow \sum F_x$	$\uparrow \sum F_y$

$$\rightarrow \sum F_x = F_2 \cos(180-\beta) - F_3 = 0$$

$$= -F_2 \cos \beta - F_3 = 0$$

$$\uparrow \sum F_y = 0 = F_2 \sin(180-\beta) + F = 0$$

$$= F_2 \sin \beta + F = 0$$

$$\left. \begin{aligned} R_1 \cos \alpha + R_3 &= 0 \\ R_1 \sin \alpha + F &= 0 \\ -R_2 \cos \beta - R_3 &= 0 \\ R_2 \sin \beta + F &= 0 \end{aligned} \right\} \begin{array}{l} \text{statically indeterminate} \\ \text{4 equations in 5 unknowns } (R_1, R_2, R_3, \alpha, \beta). \\ (F \text{ is known!}) \end{array}$$

- I need another equation to solve for five unknowns; make the assumption  $m \angle \alpha \equiv m \angle \beta$  in a completely symmetric assembly OR consider material qualities.

Assumption 1:  $m \angle \alpha \equiv m \angle \beta$ ,  $F$  is known.

$$\begin{aligned} R_1 \cos \alpha + R_3 &= 0 & R_3 &= -R_1 \cos \alpha = \frac{-F}{\sin \alpha} \cdot \cos \alpha = \frac{+F}{\tan \alpha} \\ R_1 \sin \alpha + F &= 0 \Rightarrow R_1 &= \frac{-F}{\sin \alpha} \\ -R_2 \cos \alpha - R_3 &= 0 & R_3 &= -R_2 \cos \alpha = \frac{+F}{\sin \alpha} \cos \alpha = \frac{+F}{\tan \alpha} \\ R_2 \sin \alpha + F &= 0 \Rightarrow R_2 &= \frac{-F}{\sin \alpha} \end{aligned}$$

$\updownarrow$   
\* clearly  $R_3$  in  $\Sigma F_x$  not equal that  $\Sigma F_y$

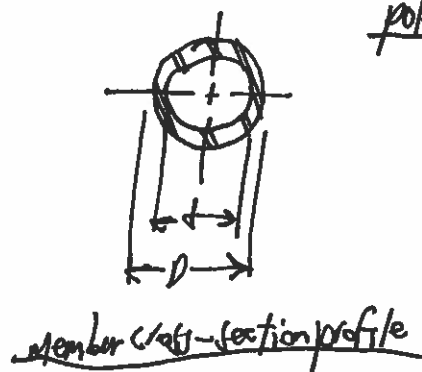
$$\therefore R_1 \equiv R_2 = \frac{-F}{\sin \alpha} \quad \wedge \quad R_3 = \frac{F}{\tan \alpha} \quad (\text{support reaction})$$

Assumption 2: material performance consideration.

- need to understand something about the member support thru either  $R_1$  or  $R_2$ ,
- typical to infer load and make a reference to factor of safety given the material properties,

i.e.  $FOS = \frac{\sigma_y}{\sigma} \quad \forall \quad \sigma_y = \text{material yield strength}, \sigma = \text{stress thru member.}$

- then I need to know geometry (cross section profile of member, say circular for simplicity,
- I suggest tubing, commercial available DOM - seamless carbon steel,



polar moment  $J = \frac{\pi}{32} (D^4 - d^4)$  since  $J = I_x + I_y$  &  $I_x = I_y$

consider pure twist / or

$$A = \frac{\pi}{4} (D^2 - d^2)$$

$$\sigma = \frac{R_1}{\frac{\pi}{4} (D^2 - d^2)}$$

$$\sigma = \frac{\sigma_y}{Fos}$$

$$\therefore \frac{\sigma_y}{Fos} = \frac{4 R_1}{\pi (D^2 - d^2)} \Rightarrow R_1 = \frac{\pi (D^2 - d^2)}{4} \cdot \frac{\sigma_y}{Fos}$$

• so my material consideration with member geometry gives me eqn independence to solve the system of equations.

• these are:

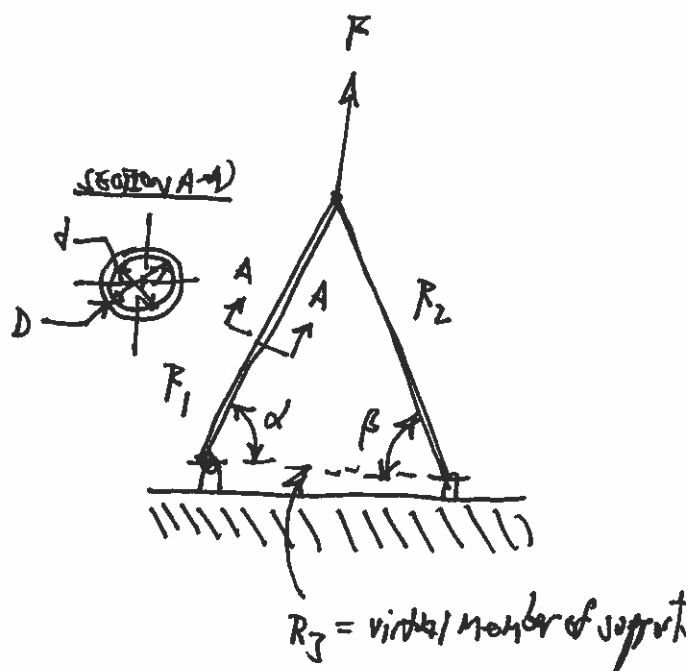
$$R_1 \cos \alpha + R_2 = 0$$

$$R_1 \sin \alpha + F = 0$$

$$-R_2 \cos \beta - R_3 = 0$$

$$R_2 \sin \beta + F = 0$$

$$R_1 = \frac{\pi (D^2 - d^2)}{4} \cdot \frac{\sigma_y}{Fos}$$



09 Jan. 2011