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**Welding Practice  
for the Sandvik Duplex Stainless Steels  
SAF 2304, SAF 2205 and SAF 2507**

**Presented by**

**Frank Babish**



# Key Points

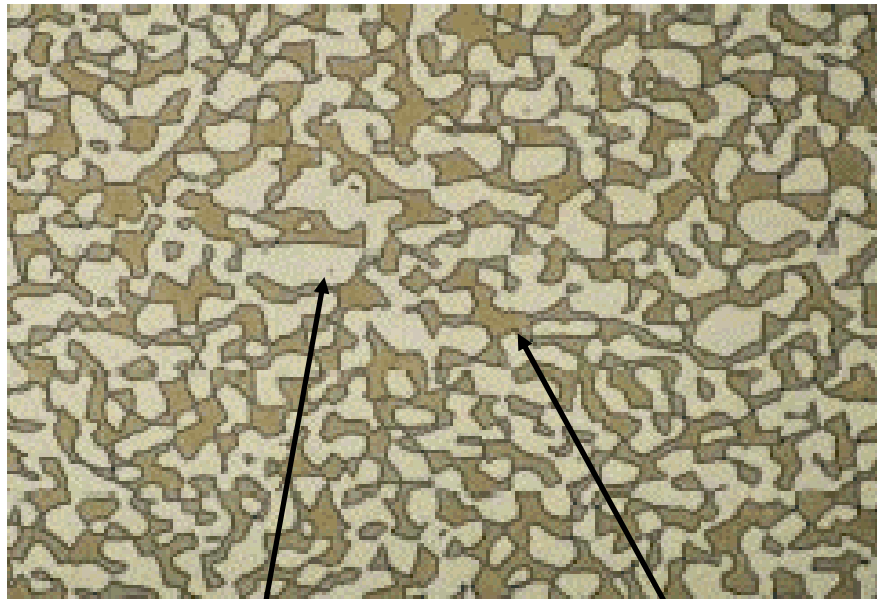
- **Metallurgical Considerations**
- **Welding Processes**
- **Composition differences Base Metal and Filler Metal**
- **Good Mechanical and Corrosion Properties of Welds**
- **Importance of Heat Input and Interpass Temperature**
- **Role of Nitrogen**
- **Post Weld Cleaning**
- **Dissimilar Joining**
- **Joint Design**

# Characteristics of Duplex stainless steels

- **Excellent resistance to stress corrosion cracking**
- **Very high mechanical strength**
- **Excellent resistance to pitting and crevice corrosion**
- **High resistance to general corrosion in a variety of environments**
- **Low thermal expansion**
- **High resistance to erosion corrosion and corrosion fatigue**
- **Good weldability**
- **Lower life cycle cost**



# Duplex microstructure

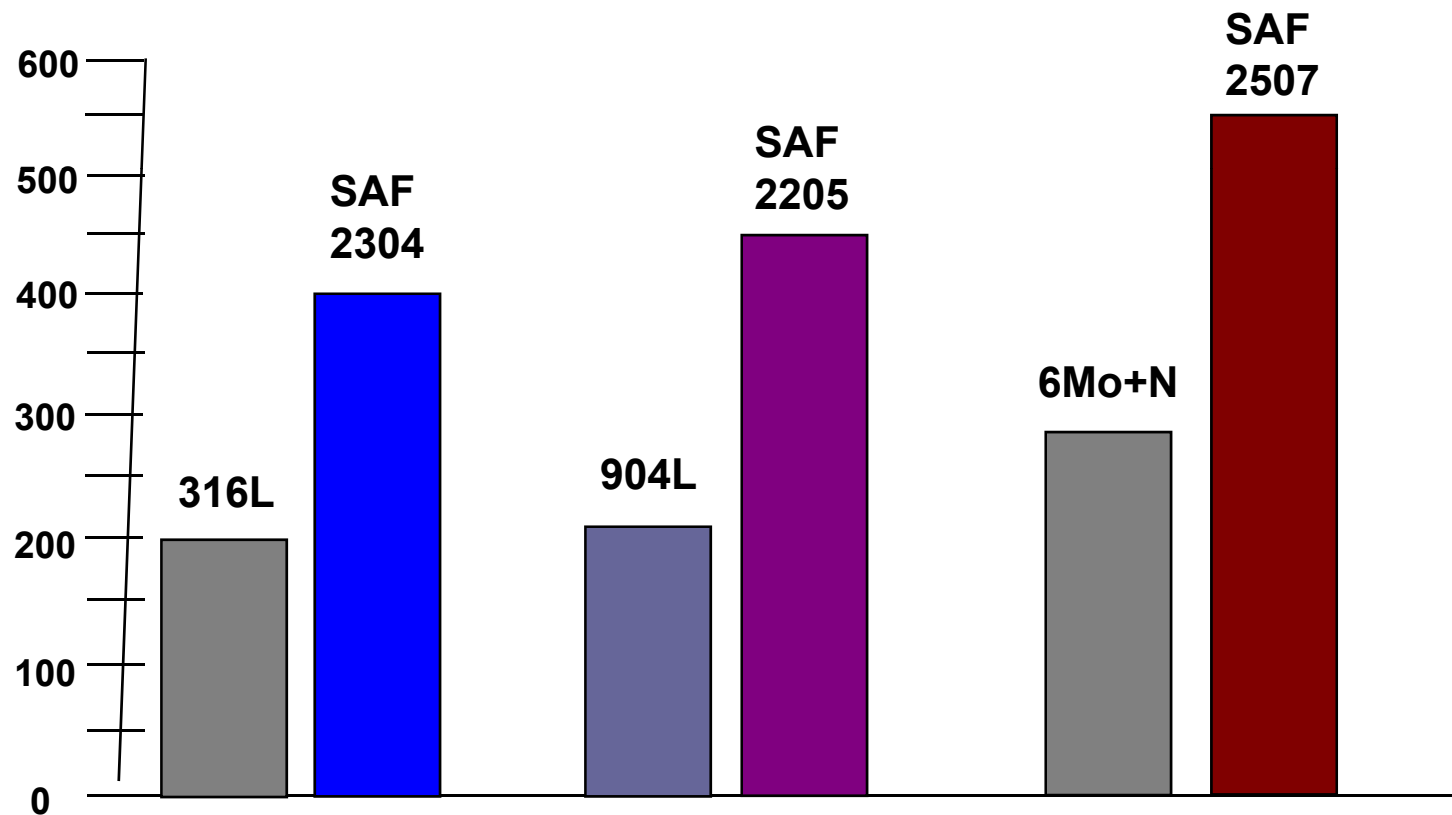


**Austenite**

**Ferrite**

- The austenite islands **(light)** are embedded in a continuous ferrite **(dark)** matrix.
- The duplex microstructure typically contains 45-65% austenite and 35-55% ferrite.

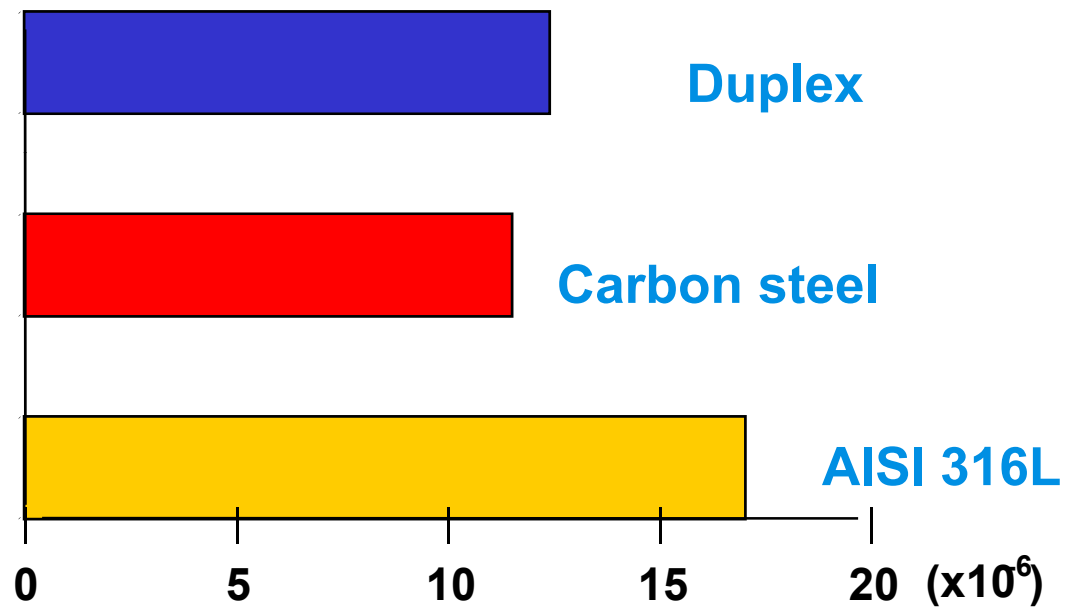
## Yield Strength 0,2% Austenitic vs Duplex Stainless Steel



## Coefficient of expansion ( $\times 10^{-6}$ )°C<sup>-1</sup>

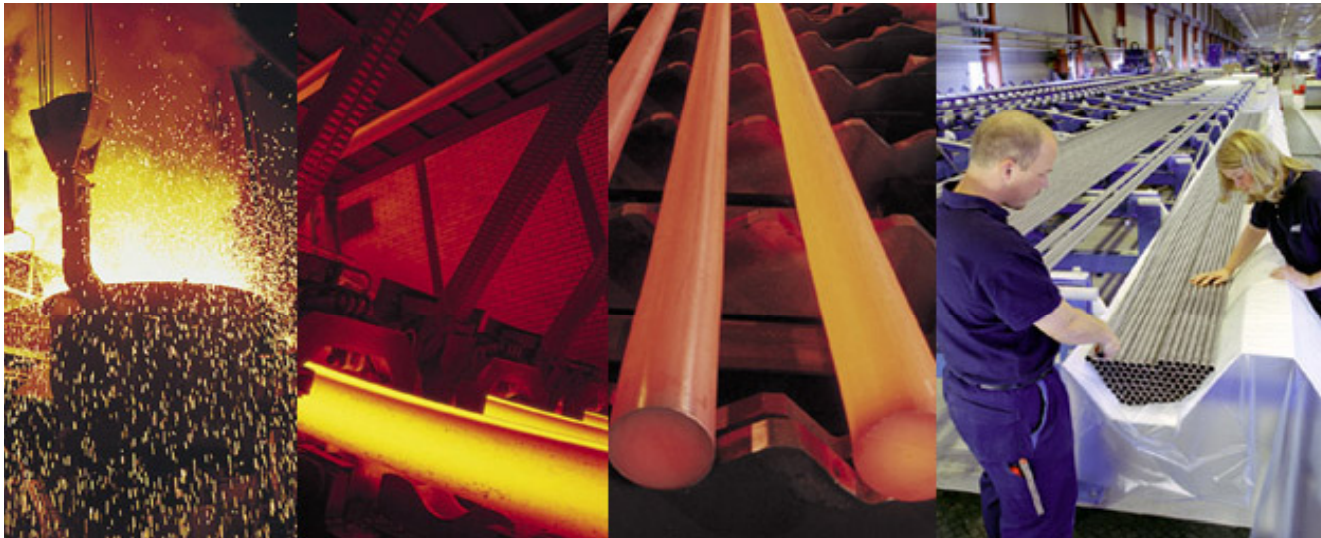
<b>Austenitic stainless steels</b>	<b>approx. 17</b>
<b>Duplex stainless steels</b>	<b>approx. 13</b>
<b>Carbon steel</b>	<b>approx. 11,5</b>

# Thermal expansion, per °C (20-100°C)



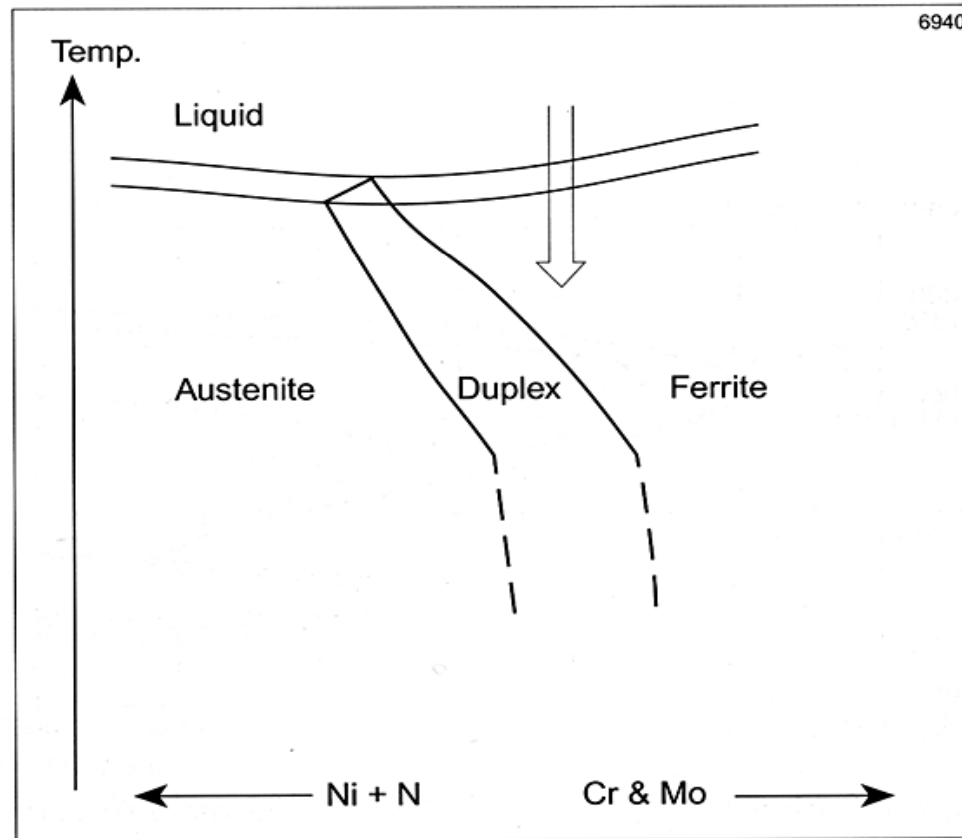


# Solidification mechanism of Duplex stainless steel

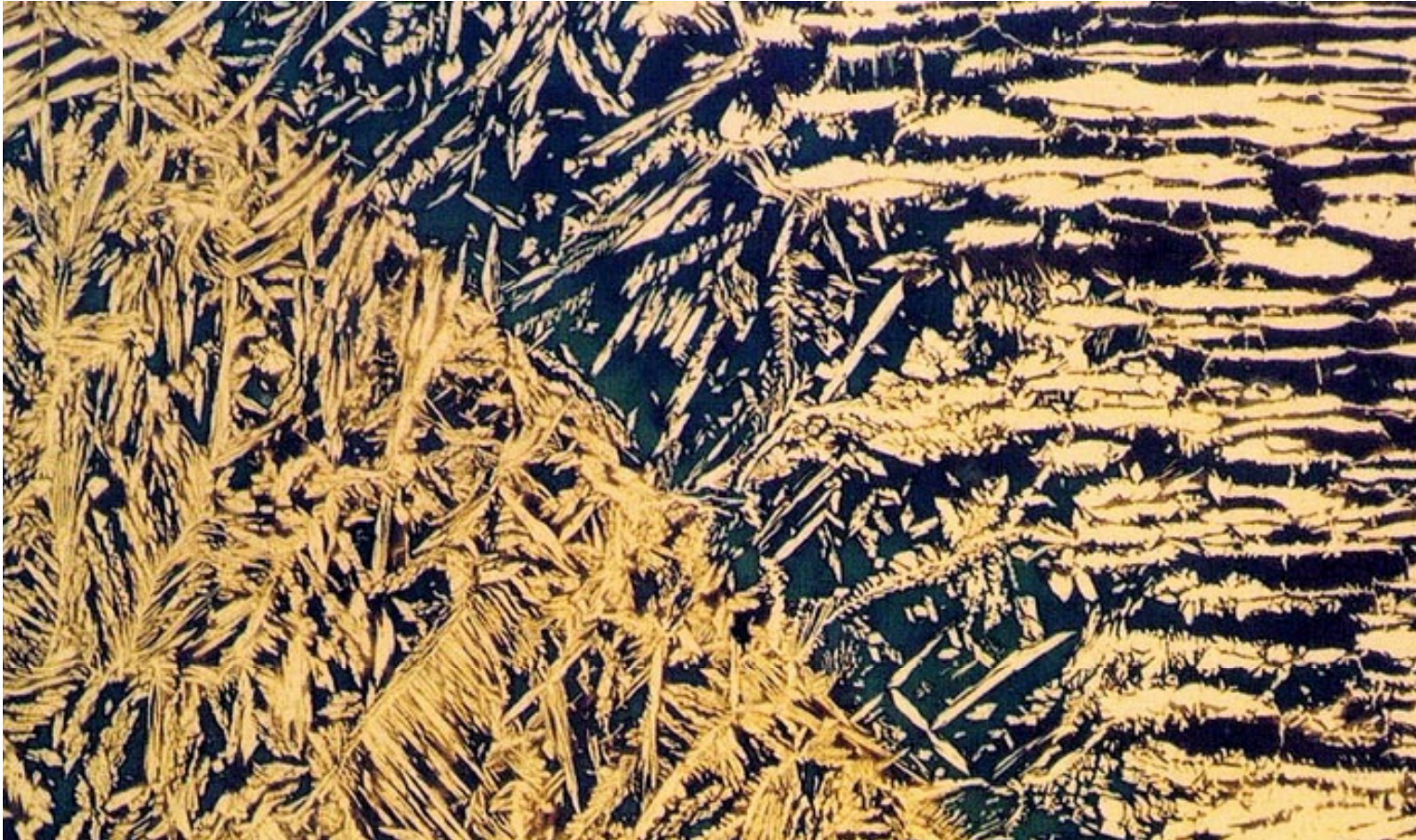


- As duplex stainless steels solidify the grain structure transform from a fully ferritic material to a balanced austenite and ferrite microstructure

# Solidification mechanism of a Duplex Stainless Steel

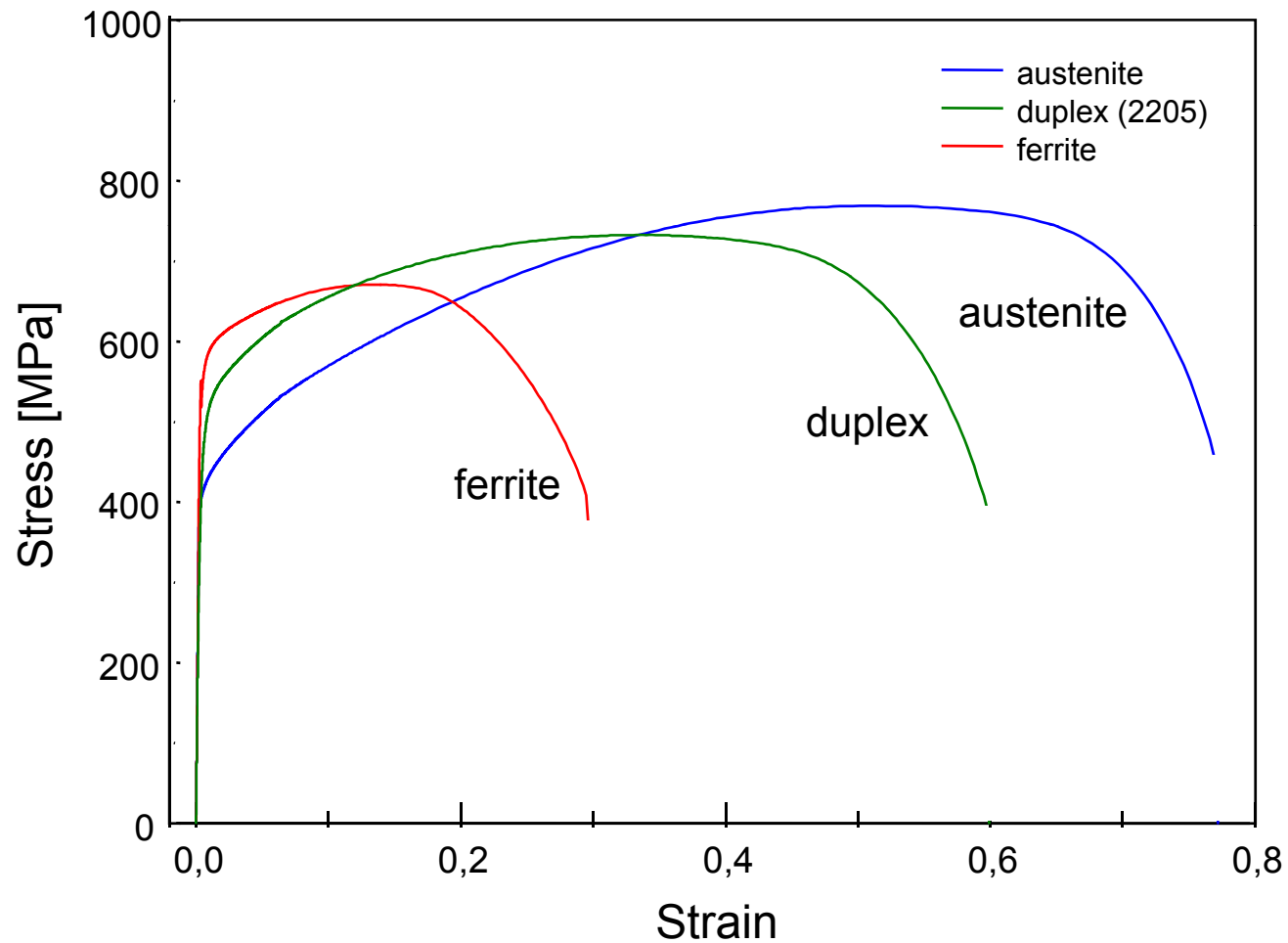


## HAZ of weld in SAF 2507



# Stress strain curves

## Austenite, ferrite and duplex



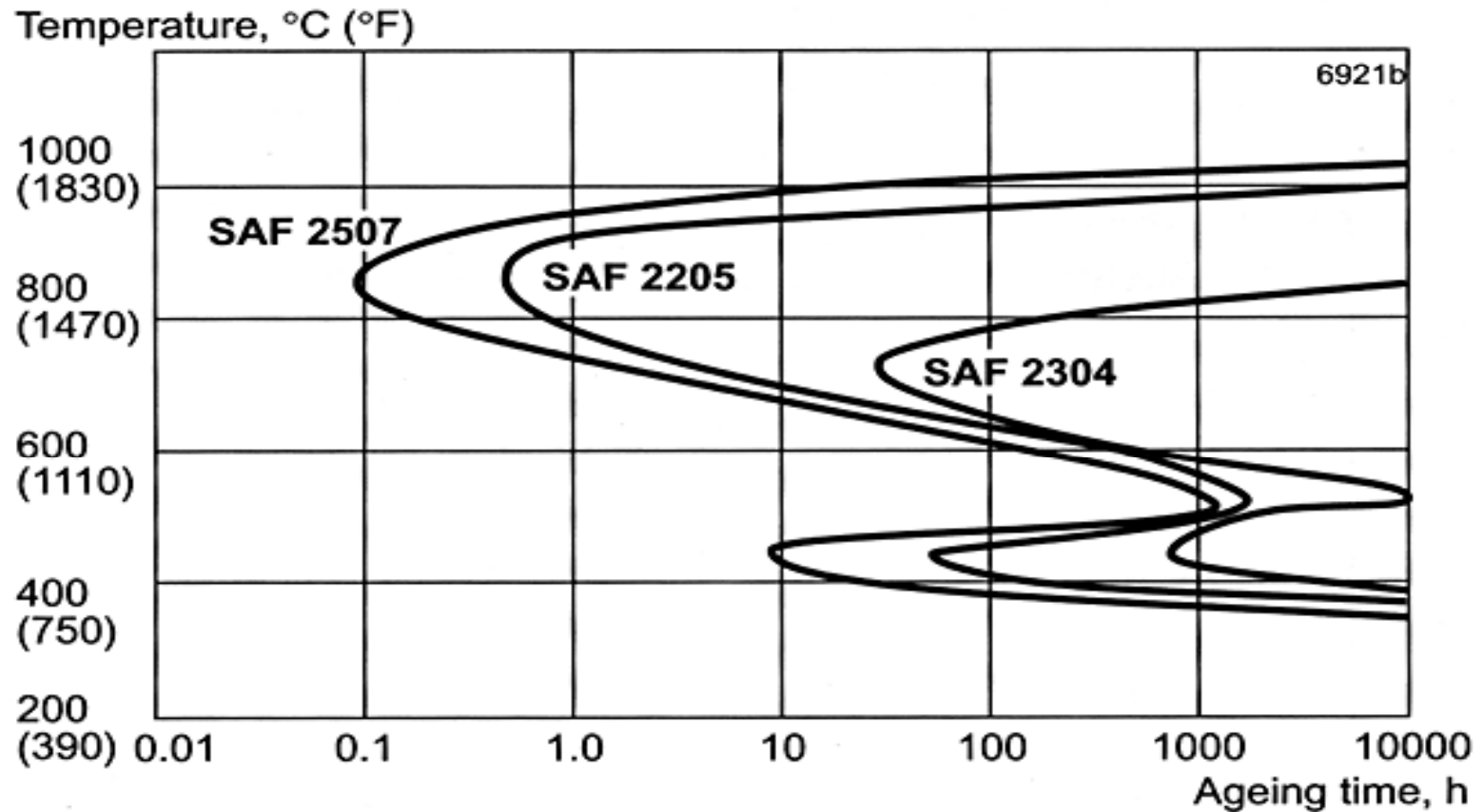


# Reasons for the high strength of duplex stainless steels

- **Content of ferrite**
- **Fine grained structure**
- **Nitrogen**



# Embrittling of Duplex Stainless Steels



# Welding Processes

## Conventional Processes

- GTAW
- GMAW
- SAW
- SMAW
- FCAW

## Avoid

- Autogenous
- Low Energy Processes
- Or Perform PWHT

# Filler Metals for the Welding of Duplex Stainless Steels

Parent metal Sandvik	Welding process	Filler metal Sandvik	Chemical composition, wt-%									Ferrite All weld metal, %
			C max.	Si	Mn	P max.	S max.	Cr	Ni	Mo	N	
SAF 2304	TIG, MIG, SAW MMA	23.7.L	0,020	0,4	1,5	0,020	0,015	23	7	-	0,14	30-40
		23.8.LR	0,030	<0,9	0,5	0,030	0,025	25	9	-	0,12	30-40
SAF 2304 and SAF 2205	TIG, MIG, SAW MMA	2209	0,020	0,5	1,6	0,020	0,015	22,5	8	3	0,14	30-40
		2209-16,17	0,030	<1,0	0,8	0,030	0,025	22,5	9	3	0,12	30-40
	FCAW	2209-15	0,04	<0,5	0,8	0,030	0,025	22	9	3	0,15	30-40
		2209LT	0,030	<1,0	1,5	0,030	0,025	22,5	9	3	0,15	30-40
SAF 2507	TIG, (MIG), SAW MMA	25.10.4.L	0,020	0,3	0,4	0,020	0,020	25	10	4	0,25	30-40
		25.10.4.LR	0,030	0,5	0,7	0,030	0,025	25	10	4	0,25	30-40
		25.10.4.LB	0,040	0,4	0,9	0,030	0,025	25,5	9,5	4	0,25	30-40



## Mechanical properties of the Duplex Stainless Steels

Sandvik	UNS	Yield strength				Tensile strength		Elong.	Hardness
		0,2% offset		1,0% offset				A5	Vickers
		MPa	ksi.	MPa	ksi.	MPa	ksi.	%	
		min.	min.	min.	min.	min.	min.	min.	approx.
SAF 2304	S32304	400	58	450	65	600-820	87-119	25	230
SAF 2205	S31803	450	65	500	73	680-880	99-128	25	260
SAF 2507	S32750	550	80	640	93	800-1000	116-145	25	290

# Mechanical Properties of All Weld Metal

Filler metal Sandvik	Welding process	R <sub>po,2</sub> MPa	R <sub>p1,0</sub> MPa	R <sub>m</sub> MPa	A <sub>5</sub> %	Z %	Impact strength, J	
							RT	-40°C
23.7.L	TIG	525	595	708	34	58	171	156
23.7.L	SAW <sup>1)</sup>	503		671	34		101	72
23.8.LR	MMA	627	681	773	26	46	62	46
22.8.3.L	TIG	610		760	28		207	160
22.8.3.L	SAW <sup>1)</sup>	578	664	775	33	53	139	84
22.9.3.LR	MMA	512		734	33		52	44
22.9.3.LT	FCAW	620	-	816	30	44	56	43
25.10.4.L	TIG	672		851	28	64	150	116
25.10.4.L	SAW <sup>1)</sup>	687	757	878	27	47	91	64
25.10.4.LR	MMA	645		850	28		46	33

<sup>1)</sup>Using Sandvik 15W flux

# Mechanical properties of welded joints.

## Cross-weld tensile test

Parent metal Sandvik	Filler metal Sandvik	Welding process	R <sub>p0.2</sub> min.	MPa typical
SAF 2304	23.7.L	TIG	400	446
	23.7.L	SAW <sup>1)</sup>	400	452
	23.8.LR	MMA	400	462
SAF 2205	22.8.3.L	TIG	450	553
	22.8.3.L	SAW <sup>1)</sup>	450	588
	22.9.3.LR	MMA	450	588
	22.9.3.LT	FCAW	450	585
SAF 2507	25.10.4.L	TIG	550	645
	25.10.4.L	SAW <sup>1)</sup>	550	628
	25.10.4.LR	MMA	550	628

<sup>1)</sup>Using Sandvik 15W flux

# Charpy-V impact strength of welded joints

Parent metal Sandvik	Filler metal Sandvik	Welding process	Impact energy, J	
			RT	-40°C
SAF 2304	23.7.L	TIG	213	74
	23.7.L	SAW <sup>1)</sup>	105	17
	23.8.LR	MMA	46	38
SAF 2205	22.8.3.L	TIG	282	133
	22.8.3.L	SAW <sup>1)</sup>	54	42
	22.9.3.LR	MMA	52	43
	22.9.3.LT	FCAW55	44	
SAF 2507	25.10.4.L	TIG	110	78
	25.10.4.L	SAW <sup>1)</sup>	100	58
	25.10.4.LR	MMA	58	39

<sup>1)</sup>Using Sandvik 15W flux

## Typical CPT Values from G-48A Tests for Parent Metals and Welded Joints

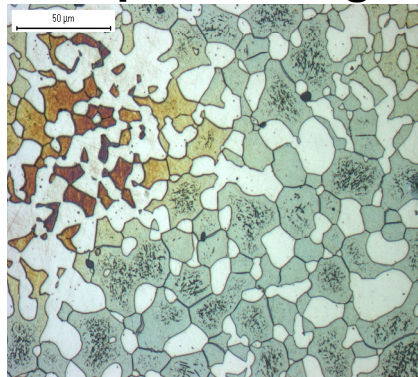
Sandvik	Filler metal	Welding process	Shielding gas	Root gas	CPT °C
<b>SAF 2304</b>					<b>~15</b>
All weld metal	23.7.L	TIG	Ar	-	<15
Joint	23.7.L	TIG	Ar	Ar	<15
Joint	23.7.L	SAW <sup>1)</sup>	-	-	<15
Joint	23.8.LR	MMA	-	-	<15
<b>SAF 2205</b>					<b>30</b> ← PM
All weld metal	22.8.3.L	TIG	Ar	-	20-23
Joint	22.8.3.L	TIG	Ar	Ar	20-23
Joint	22.8.3.L	TIG	Ar - 2% N <sub>2</sub>	90 N <sub>2</sub> + 10 H <sub>2</sub> (or pure N <sub>2</sub> )	23-25
All weld metal	22.8.3.L	SAW <sup>1)</sup>	-	-	20-25
Joint	22.8.3.L	SAW <sup>1)</sup>	-	-	20-25
All weld metal	22.9.3.LR	MMA	-	-	20-25
Joint	22.9.3.LR	MMA	-	-	20-25
<b>SAF 2507</b>					<b>80</b>
Autogenous TIG welding					40
All weld metal	25.10.4.L	TIG	Ar	-	40-45
Joint	25.10.4.L	TIG	Ar	Ar	40-45
Joint	25.10.4.L	TIG	Ar	90 N <sub>2</sub> + 10 H <sub>2</sub> (or pure N <sub>2</sub> )	40-50
Joint	25.10.4.L	TIG	Ar + 2% N <sub>2</sub>	90 N <sub>2</sub> + 10 H <sub>2</sub> (or pure N <sub>2</sub> )	45-55
All weld metal	25.10.4.L	SAW <sup>1)</sup>	-	-	40-50
Joint	25.10.4.L	SAW <sup>1)</sup>	-	-	40-50
All weld metal	25.10.4.LR	MMA	-	-	40-50
Joint	25.10.4.LR	MMA	-	-	40-50

<sup>1)</sup>Using Sandvik 15W flux

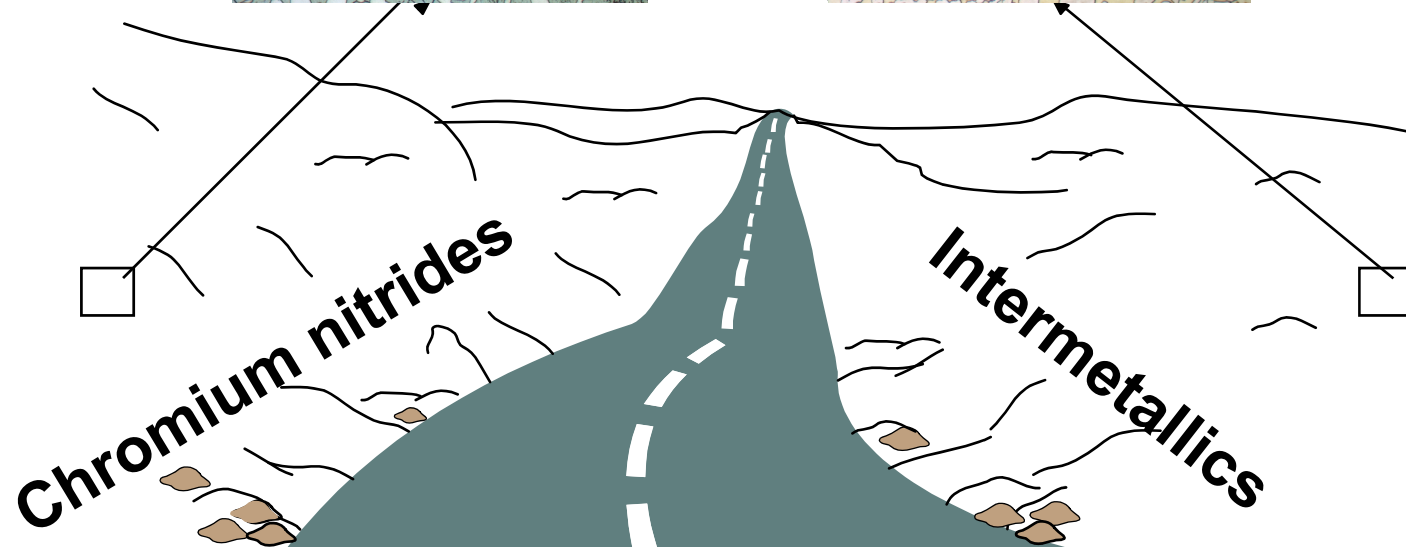
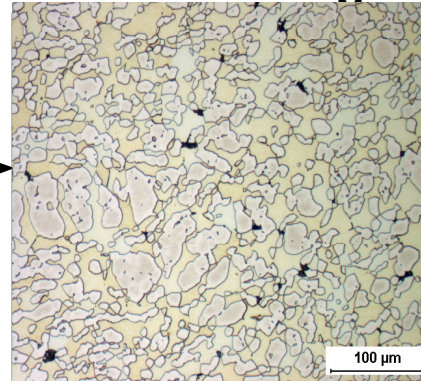
# Quench annealing of Duplex Steel welds

<b>Sandvik</b>	<b>Holding temperature °C</b>	<b>Quenching media</b>
<b>SAF 2304</b>	<b>930 - 1050</b>	<b>Water</b>
<b>SAF 2205</b>	<b>1020 - 1100</b>	<b>Water</b>
<b>SAF 2507</b>	<b>1080 - 1120</b>	<b>Water</b>

**High quenching temp  
Rapid cooling**



**Low quenching temp.  
Slow cooling**





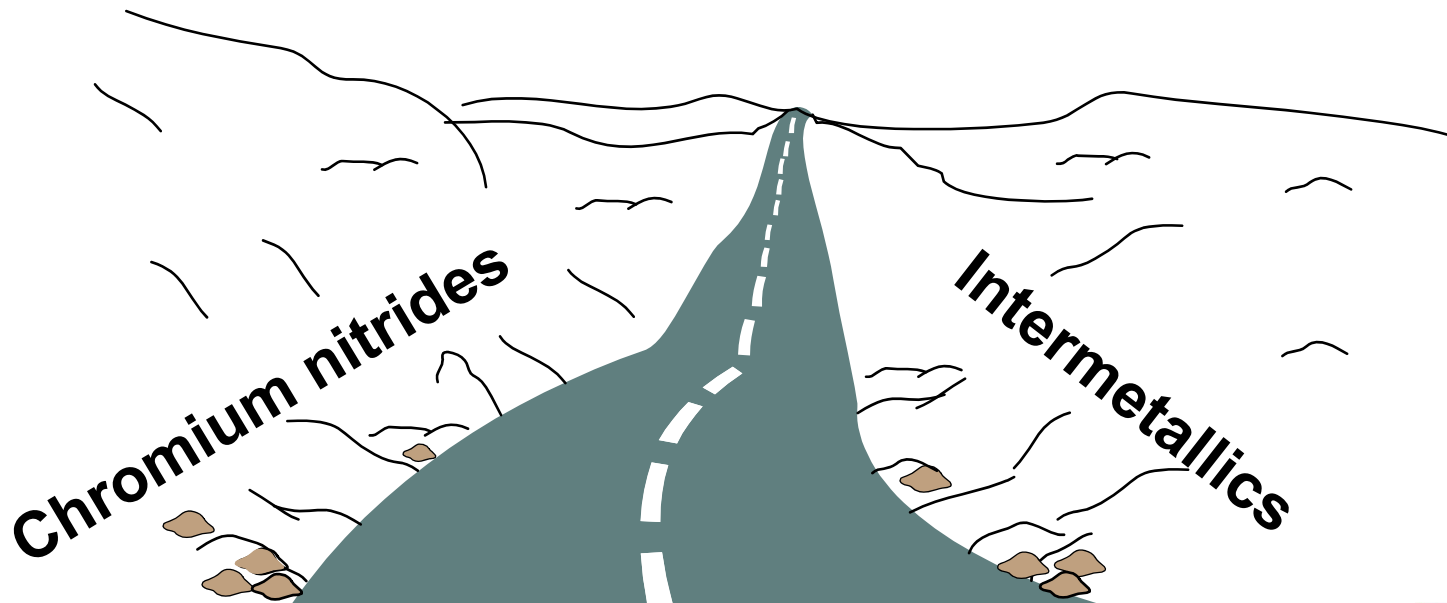
## Intermetallic phase





# Recommended heat input

Steel	Heat input	Interpass temperature
SAF 2304	0,5 - 2,5 kJ/mm	<250°C
SAF 2205	0,5 - 2,5 kJ/mm	<250°C
SAF 2507	0,2 - 1,5 kJ/mm	<150°C



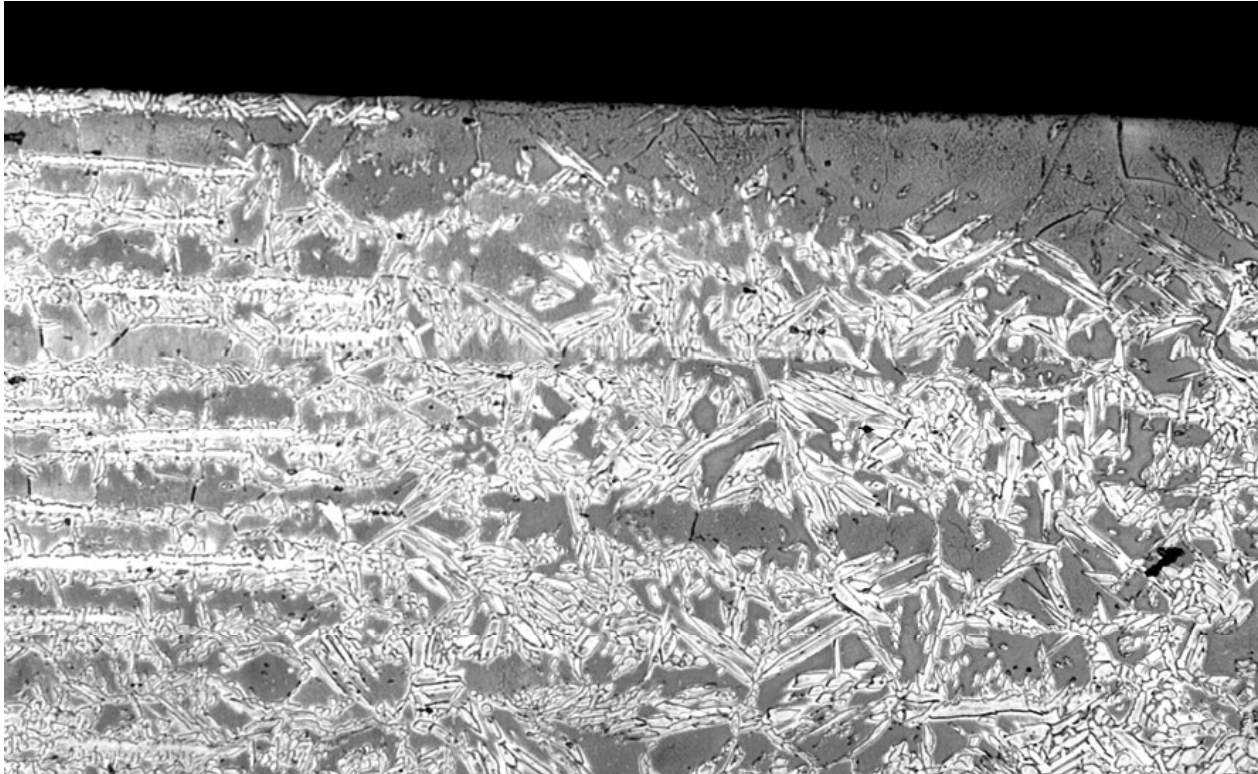
## Welding recommendations

<b>Sandvik</b>	<b>Heat input kJ/mm</b>	<b>Interpass temperature °C</b>
<b>SAF 2304</b>	<b>0,5 - 2,5</b>	<b>&lt;250</b>
<b>SAF 2205</b>	<b>0,5 - 2,5</b>	<b>&lt;250</b>
<b>SFA 2507</b>	<b>0,2 - 1,5</b>	<b>&lt;150</b>

# The roll of Nitrogen

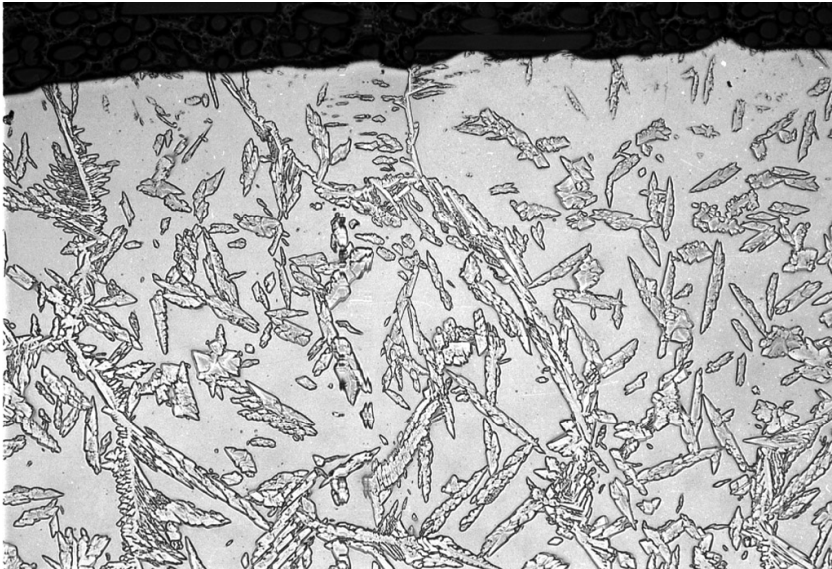
- Nitrogen is a very important alloying element in DSS
  - ✓ Improves corrosion resistance
  - ✓ Improves austenite reformation
- At TIG welding, the loss of nitrogen is compensated for by using Ar + 1 - 2%N<sub>2</sub> as a shielding gas

## Ferritic area in SAF 2507 weld owing to the loss of nitrogen in fusion line

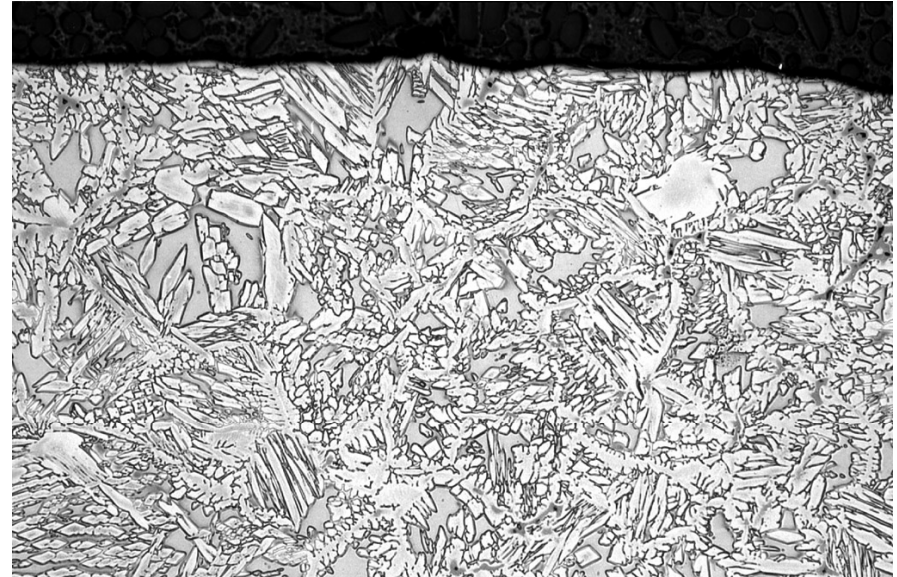


Shielding gas Ar 99,99%

# Nitrogen addition to the shielding gas



Ar 99,99%



Ar + 5% N<sub>2</sub>

Preferred,  
typically 2% N<sub>2</sub>

## Ferrite content in TIG-welds, SAF 2507

Filler metal Sandvik	Shielding gas	Root gas	Ferrite content, vol-% ± error with 95% confidence interval
25.10.4.L	Ar	Ar	55 ± 4,5
25.10.4.L	Ar	90% N <sub>2</sub> + 10% H <sub>2</sub>	59 ± 4,0
25.10.4.L	Ar + 5% N <sub>2</sub>	90% N <sub>2</sub> + 10% H <sub>2</sub>	33 ± 4,0

For Root Pass

## Nitrogen Content in TIG welds of SAF 2507. N=0,25% in the filler metal

Filler metal Sandvik	Shielding gas	Root gas	Weight-% N in deposit
25.10.4.L	Ar	90% N <sub>2</sub> + 10% H <sub>2</sub>	0,23
25.10.4.L	Ar + 3% N <sub>2</sub>	90% N <sub>2</sub> + 10% H <sub>2</sub>	0,27
25.10.4.L	Ar + 6% N <sub>2</sub>	90% N <sub>2</sub> + 10% H <sub>2</sub>	0,33



# GMAW SHIELDING GASES

- **General recommendations:**
  - ✓ **Short arc welding gives very convex beads.**  
**Ar+30 He+1 O<sub>2</sub>**
  - ✓ **Spray arc welding**  
**Ar+30 He+1 O<sub>2</sub> (22Cr duplex)**  
**Ar+2 CO<sub>2</sub>(Super duplex)**
  - ✓ **Pulsed arc welding**  
**Ar+30 He+1 O<sub>2</sub> (22Cr duplex)**  
**Ar(99,996%) for super duplex**



# Nitrogen Analysis from the Top of a TIG weld

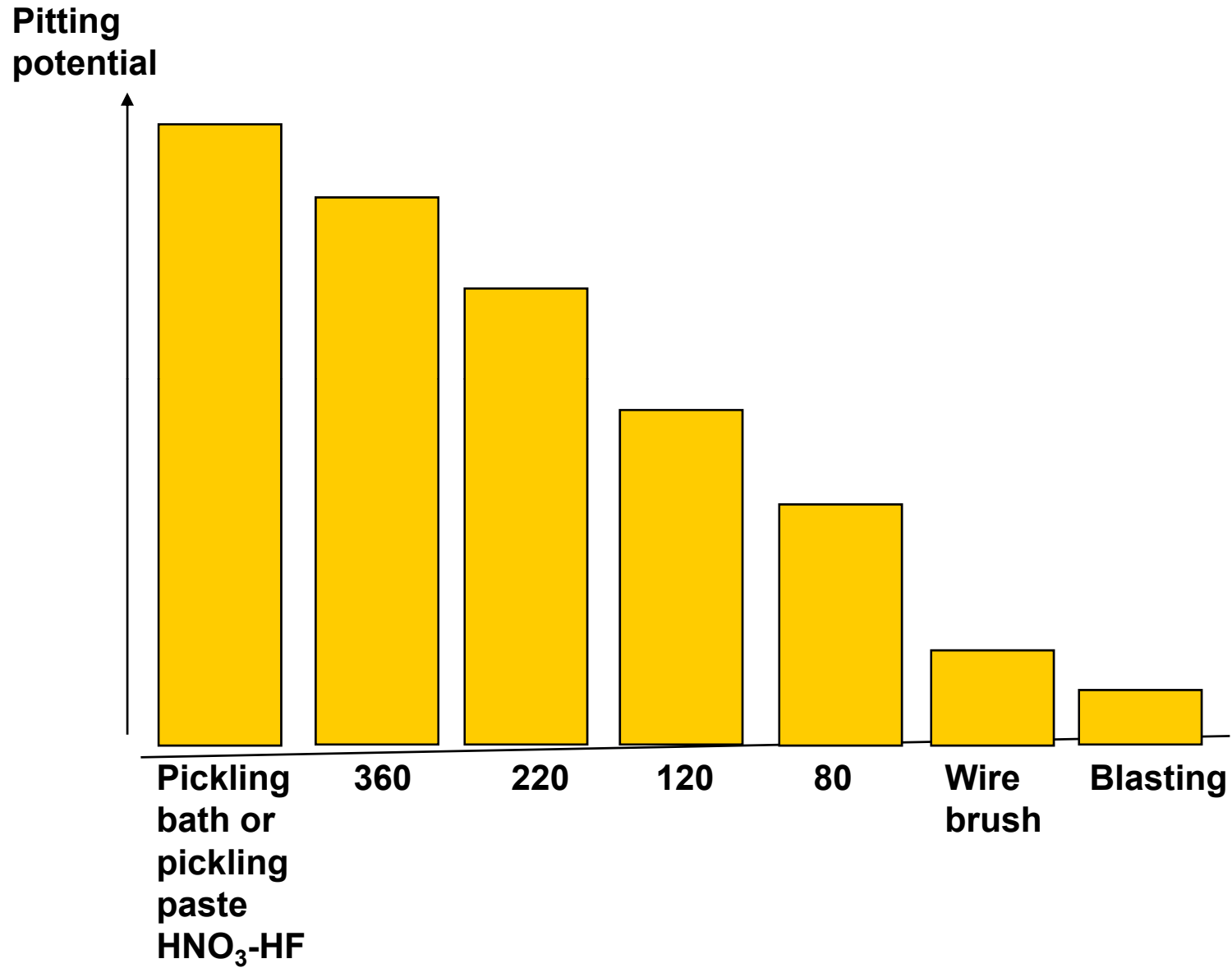
	% Nitrogen in position (o'clock)						Analysis at
	3	5	6	7	11	12	
Welder No. 1	0,17	0,18	0,15	0,16	0,19	0,19	Top side
Welder No. 2	0,18	-	0,19		0,19	-	Top side
	0,20	-	0,21		0,20	-	Root side
Welder No. 3	0,22	-	0,21		0,20	-	Top side
	0,21	-	0,21		0,20	-	Root side

In all cases the filler metal had a nitrogen content of 0,25%

# Stress relieving temperatures

**$325 \pm 25^{\circ}\text{C}$  for 10 hours**

# Post Weld Cleaning



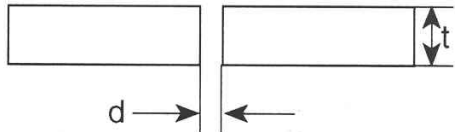
## Dissimilar Joints

<b>SAF</b>	<b>Carbon steel</b>	<b>AISI 200 and 300- series</b>	<b>AISI 904L, Sanicro 28, 254 SMO, etc.</b>
<b>2304</b>	<b>22.8.3.L 22.9.3.LR 22.9.3.LT</b>	<b>22.8.3.L 22.9.3.LR 22.9.3.LT</b>	<b>22.8.3.L 22.9.3.LR 22.9.3.LT</b>
<b>2205</b>	<b>22.8.3.L 22.9.3.LR 22.9.3.LT</b>	<b>22.8.3.L 22.9.3.LR 22.9.3.LT</b>	<b>22.8.3.L 22.9.3.LR 22.9.3.LT</b>
<b>2507</b>	<b>25.10.4.L 25.10.4.LR</b>	<b>25.10.4.L 25.10.4.LR</b>	<b>Sanicro 60 Sanicro 60</b>

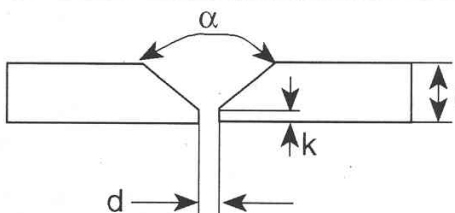
# Joint preparation

## One sided butt welding

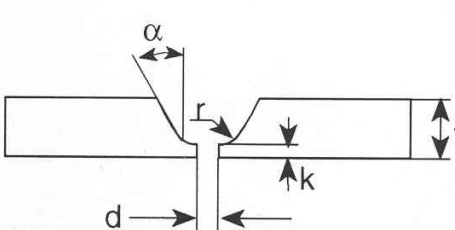
### Square groove

	t mm	d mm	
MMA	<3	1-2	
TIG	<3	1-2	
MIG	<3	1-2	

### V-groove

	t mm	d mm	k mm	$\alpha$	
MMA	3-15	2-3	1-2	60-70°	
TIG	2.5-8	2-3	1-2	60-70°	
MIG	3-12	2-3	1-2	60-70°	
SAW*	4-12	2-3	1-2	70-90°	

### U-groove

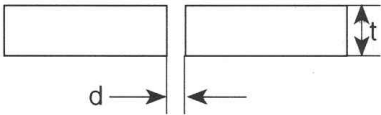
	t mm	d mm	k mm	r mm	$\alpha$	
MMA	>12	1-2	2-3	6	15°	
TIG	>6	1-2	1-2	6-8	15°	
MIG	>12	1-2	2-3	6	15°	
SAW*	>10	1-2	1-3	6-8	15°	

\*Root pass with TIG, MIG or MMA. SAF 2507: Contact Sandvik for advice.

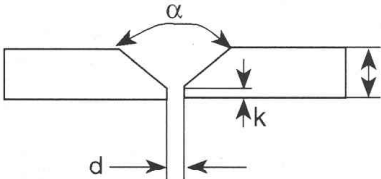
# Joint preparation

## Butt welding from both sides

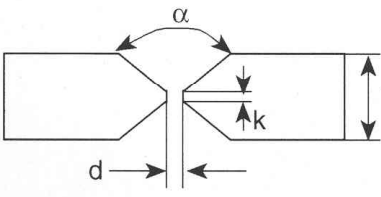
### Square groove

	t mm	d mm		
MMA	3-4	1.5-3		
TIG	3-5	1.5-3		
MIG	3-6	1.5-3		

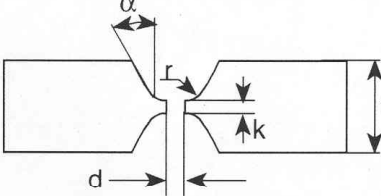
### V-groove

	t mm	d mm	k mm	$\alpha$	
MMA	4-15	1-3	1-2	60-70°	
TIG	2.5-8	1-3	1-2	60-70°	
MIG	5-12	1-3	1-2	60-70°	

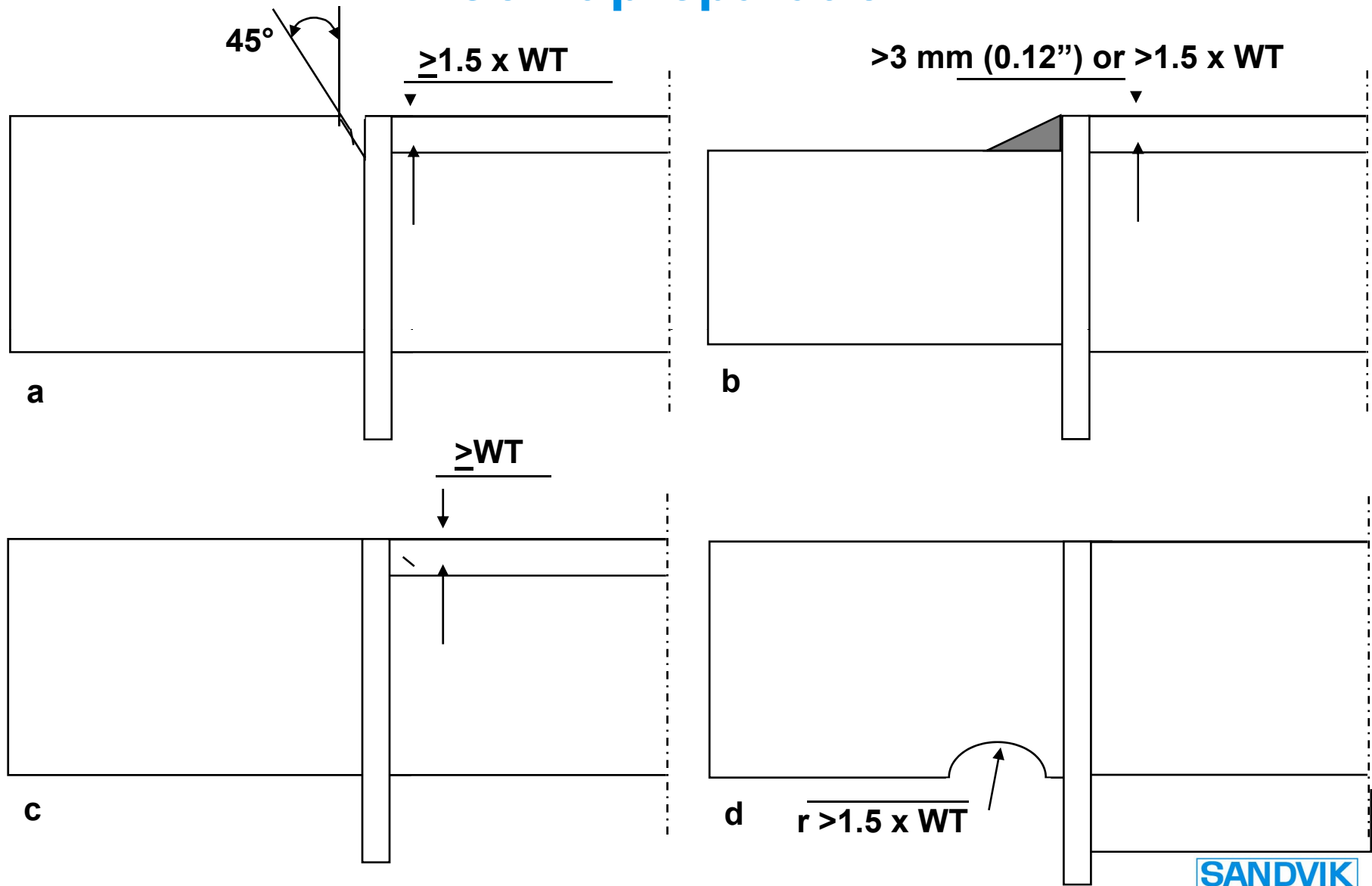
### Double V-groove

	t mm	d mm	k mm	$\alpha$	
MMA	>10	1.5-3	1-3	60-70°	
MIG	>10	1.5-3	1-3	60-70°	
SAW	>10	0	3-5	90°	

### Double U-groove

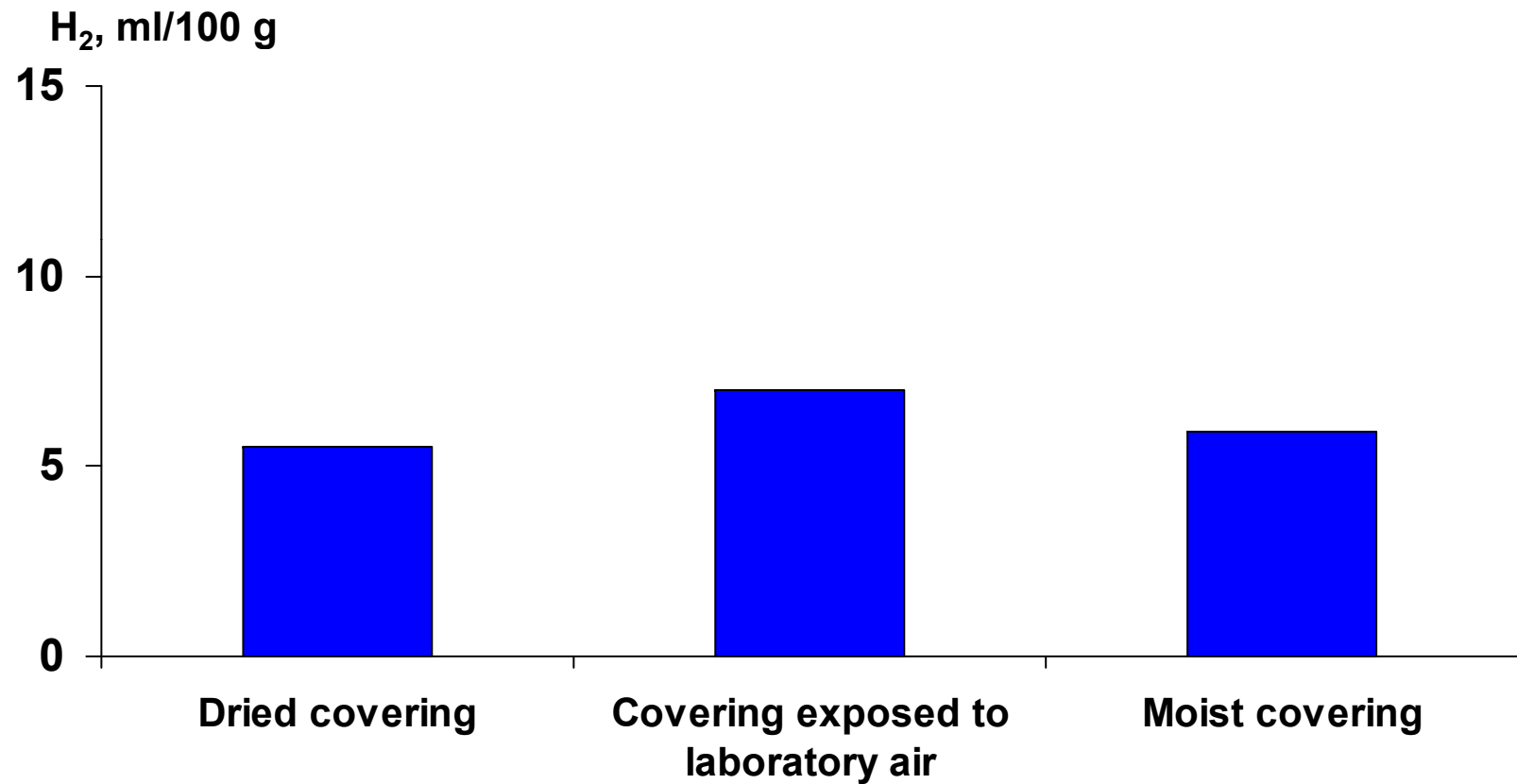
	t mm	d mm	k mm	r mm	$\alpha$	
MMA	>25	1-3	1-3	6-8	10-15°	
SAW	>25	0	3-5	6-8	10-15°	

# Tube to tube sheet welding. Joint preparation



# Hydrogen pick-up from covered electrodes Sandvik 25.10.4.LR

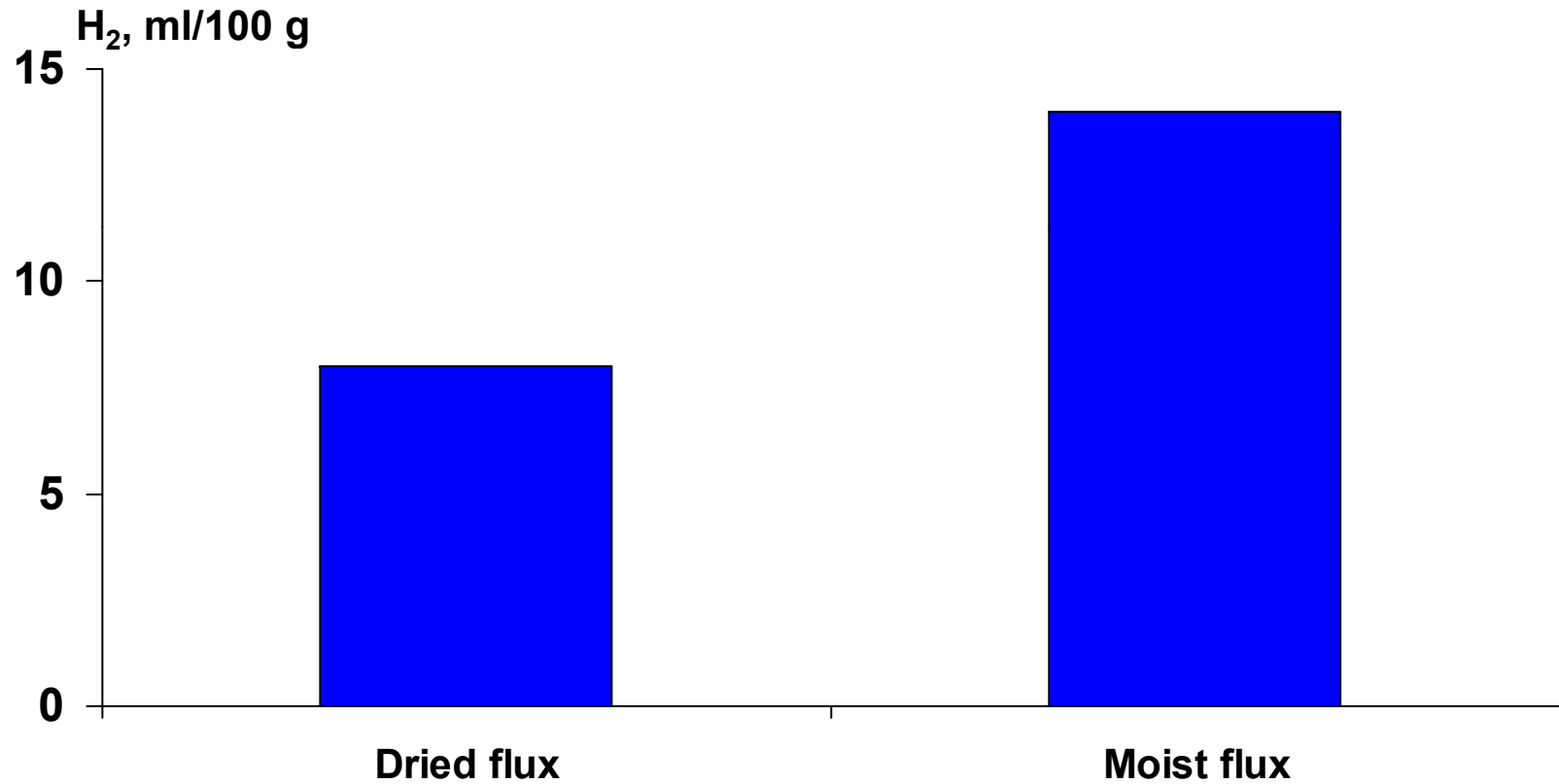
**MMA**



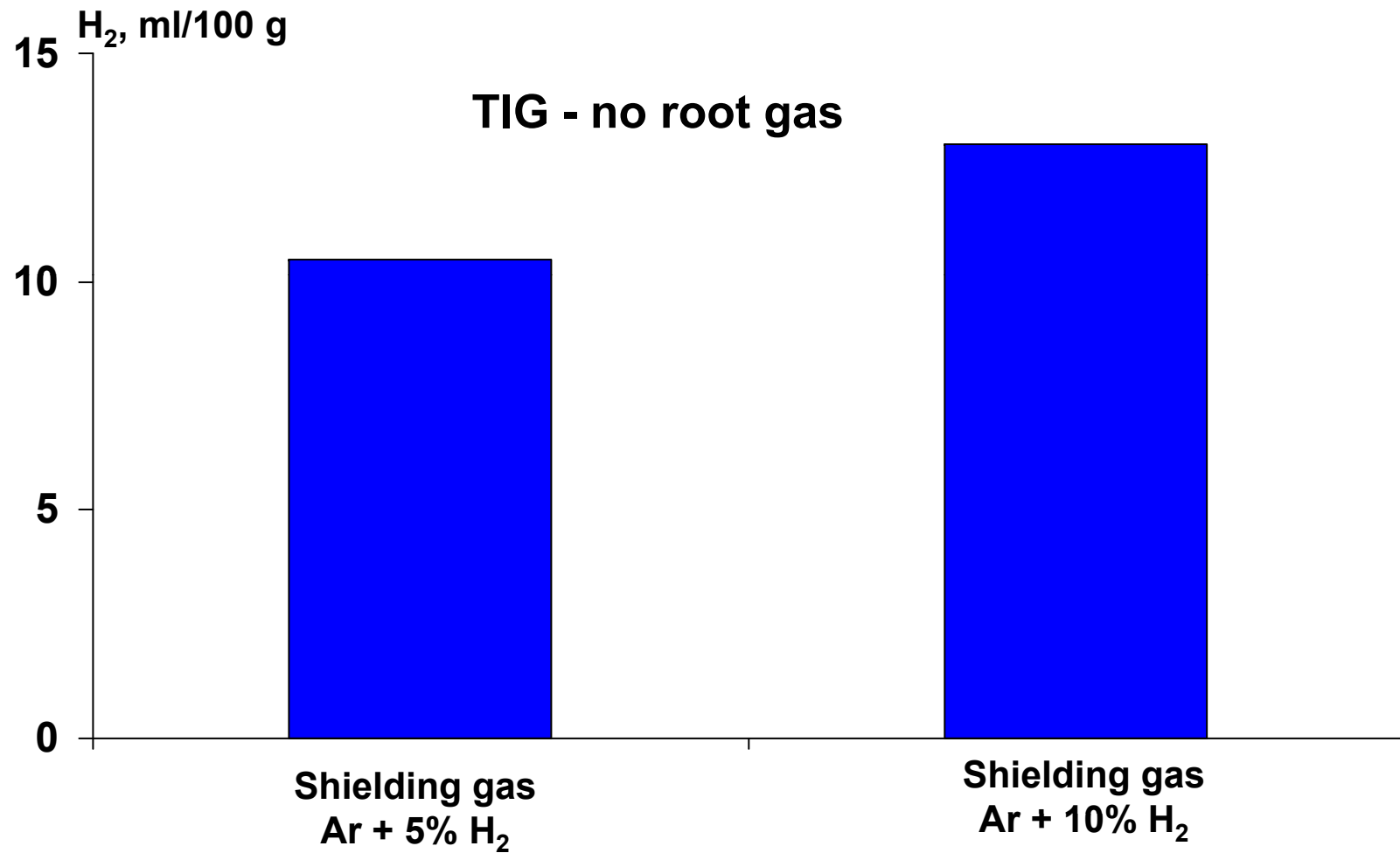


# Hydrogen pick-up from SAW flux

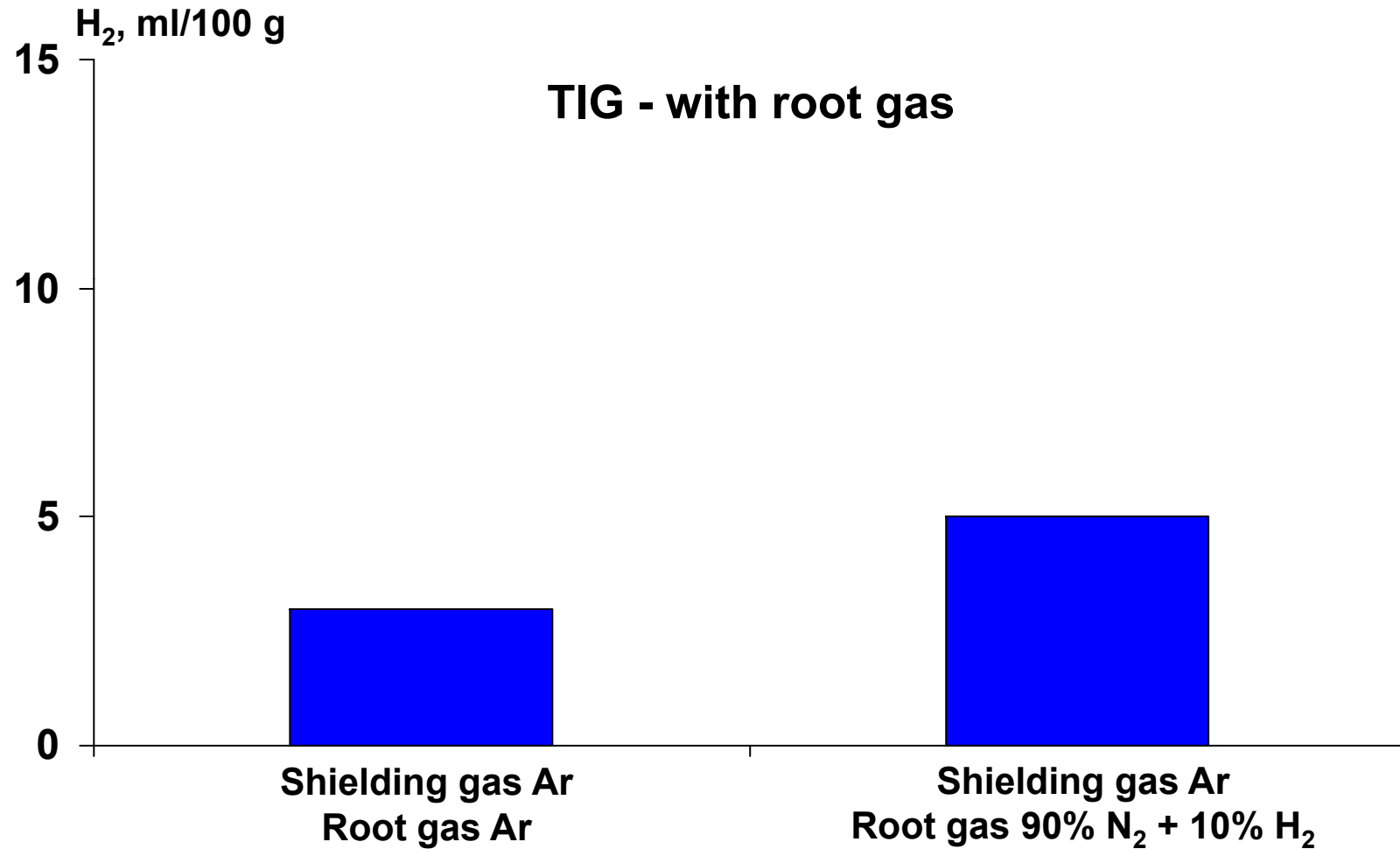
**SAW**



## Hydrogen pick up from shielding gas at TIG welding



# Hydrogen pick up from shielding gas and root gas at TIG welding



# Conclusions

## Key Areas

- **Good Weldability**
- **Uses Conventional Welding Processes**
- **Joint Design**
- **Role of Nitrogen**
- **Heat Input Important**
- **Interpass Temperature**