

## Adjustment Factors for Reference Design

### 8.4.4.1 General

Adjusted design values shall be obtained by adjusting reference design values by applicable adjustment factors in accordance with the following equations:

$$F \approx F_{bo} C_{KF} C_M (C_F \text{ or } C_V) C_{fu} C_i C_d C_\lambda \quad (8.4.4.1-1)$$

$$F \approx F_{vo} C_{KF} C_M C_i C_\lambda \quad (8.4.4.1-2)$$

$$F \approx F_{to} C_{KF} C_M C_F C_i C_\lambda \quad (8.4.4.1-3)$$

$$F \approx F_{co} C_{KF} C_M C_F C_i C_\lambda \quad (8.4.4.1-4)$$

$$F_q = F_{cpo} C_{KF} C_M C_i C_\lambda \quad (8.4.4.1-5)$$

$$E \approx E_o C_M C_i \quad (8.4.4.1-6)$$

where:

$F$  = applicable adjusted design values  $F_b$ ,  $F_v$ ,  $F_t$ ,  $F_c$  or  $F_{cp}$  (ksi)

$F_o$  = reference design values  $F_{bo}$ ,  $F_{vo}$ ,  $F_{to}$ ,  $F_{co}$  or  $F_{cpo}$  specified in Article 8.4 (ksi)

$E$  = adjusted modulus of elasticity (ksi)

$E_o$  = reference modulus of elasticity specified in Article 8.4. (ksi)

$C_{KF}$  = format conversion factor specified in Article 8.4.4.2

$C_M$  = wet service factor specified in Article 8.4.4.3

$C_F$  = size factor for visually-graded dimension lumber and sawn timbers specified in Article 8.4.4.4

$C_V$  = volume factor for structural glued laminated timber specified in Article 8.4.4.5

$C_{fu}$  = flat-use factor specified in Article 8.4.4.6

$C_i$  = incising factor specified in Article 8.4.4.7

$C_d$  = deck factor specified in Article 8.4.4.8

$C_\lambda$  = time effect factor specified in Article 8.4.4.9

### 8.4.4.2 Format Conversion Factor, $C_{KF}$

The reference design values in Table 1 and 2 and reference design values specified in the *NDS*<sup>®</sup> shall be multiplied by a format conversion factor,  $C_{KF}$ , for use with load and resistance factor design (LRFD).  $C_{KF} = 2.5/\phi$ , except for compression perpendicular to grain which shall be obtained by multiplying the allowable stress by a format conversion factor of  $C_{KF} = 2.1/\phi$ .

### C8.4.4.2

The conversion factors were derived so that LRFD design will result in same size member as the allowable stress design (ASD) specified in *NDS*<sup>®</sup>. For example, a rectangular component in flexure has to satisfy:

$$1.25 M_{DL} + 1.75 M_{LL} \leq \phi S F_{bo} C_{KF} C_M (C_F \text{ or } C_v) C_{fu} C_i C_d C_\lambda C_L \quad (\text{C8.4.4.2-1})$$

or:

$$(1.25 M_{DL} + 1.75 M_{LL}) / (\phi C_{KF} C_\lambda) \leq S F_{bo} C_M (C_F \text{ or } C_v) C_{fu} C_i C_d C_L \quad (\text{C8.4.4.2-2})$$

where:

$M_{DL}$  = moment due to dead load

$M_{LL}$  = moment due to live load

On the other hand, the allowable stress design (ASD) has to satisfy:

$$M_{DL} + M_{LL} \leq S F_{bo} C_M (C_F \text{ or } C_v) C_{fu} C_i C_d C_D C_L \text{ or } (M_{DL} + M_{LL}) / (C_D) \leq S F_{bo} C_M (C_F \text{ or } C_v) C_{fu} C_i C_d C_L \quad (\text{C8.4.4.2-3})$$

Therefore:

$$(1.25 M_{DL} + 1.75 M_{LL}) / (\phi C_{KF} C_\lambda) = (M_{DL} + M_{LL}) / (C_D) \quad (\text{C8.4.4.2-4})$$

$$C_{KF} = [(1.25 M_{DL} + 1.75 M_{LL})(C_D)] / [(M_{DL} + M_{LL})(\phi C_\lambda)] \quad (\text{C8.4.4.2-5})$$

The format conversion factor is calculated assuming the ratio of  $M_{DL}$  and  $M_{LL}$  is 1:10,  $\phi = 0.85$ ,  $C_\lambda = 0.8$ , and  $C_D = 1.15$ .

Table 8.4.4.4-1 Size Effect Factor,  $C_F$ , for Sawn Dimension Lumber.

Table 8.4.4.4-1 Size Effect Factor, $C_F$ , for Sawn Dimension Lumber.						
Grade	Width (in.)	$F_{bo}$		$F_{t0}$	$F_{co}$	All Other Properties
		Thickness				
		2.0 in. and 3.0 in.	4.0 in.	All	All	All
		Structural Light Framing: 2.0 in. $\times$ 2.0 in. through 4.0 in. $\times$ 4.0 in.				
		Structural Joists and Planks: 2.0 in. $\times$ 5.0 in. through 4.0 in. $\times$ 16.0 in.				
	$\leq 4$	1.5	1.54	1.5	1.15	1.00
Sel. Str.	5	1.4	1.4	1.4	1.1	
	6	1.3	1.3	1.3	1.1	
No. 1	8	1.2	1.3	1.2	1.05	
No. 2	10	1.1	1.2	1.1	1.0	
	12	1.0	1.1	1.0	1.0	
	$\geq 14$	0.9	1.0	0.9	0.9	