

BECAUSE WELD IS  
ON BOTH SIDES

## WELDING TORSION

USE WELDS AS PROPERTIES OF  
LINES

$$\therefore J = \frac{Z}{12} - \frac{b^4}{2b+d} \quad b=4" \quad d=2"$$

$$Z = 8b^3 + 6bd^2 + d^3$$

$$J = \underline{\underline{25.733 \text{ in}^3}}$$

$$\frac{T \times r}{J} = \tau_{\text{Tor}} = \frac{0.5 \times (5.5 + 1.33)}{25.733}$$

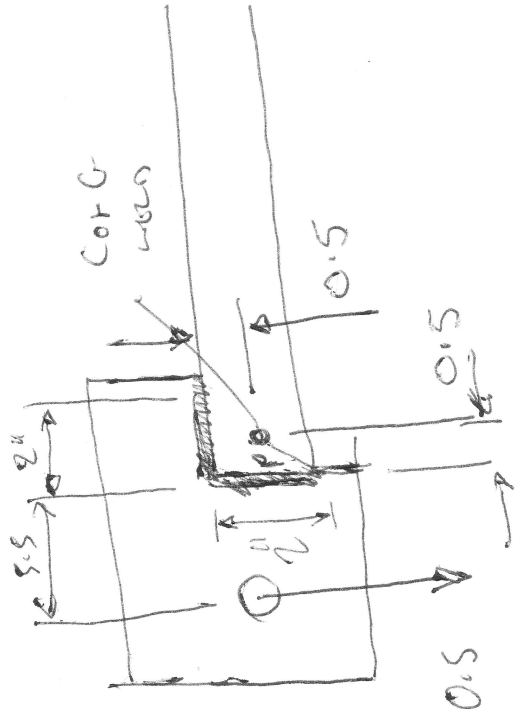
$$\tau_{\text{Torsion}} = \underline{\underline{0.1327 \text{ lb/in}^2}}$$

SHEET 1

$$\tau_{\text{Direct}} = \frac{\text{Force}}{\text{Area}} = \frac{0.5}{0.707 \times 0.25 \times 11"} = 0.2572 \text{ lb/in}^2$$

$$\text{MAX RESULTANT STRESS} = \sqrt{\tau_{\text{Torsion}}^2 + \tau_{\text{Direct}}^2}$$

$$= \sqrt{0.1327^2 + 0.25716^2} = \underline{\underline{0.2894 \text{ lb/in}^2}}$$



SIMILAR TO PREVIOUS AND  
USING ROY MECH SITE FOR  
WELDS AS LINE PROPERTIES

$$r = 4.5'' \quad J = \frac{(b+d)^4 - 6b^2d^2}{12(b+d)} \quad b = 2'' \quad d = 2''$$

$$r = \frac{I_{xT}}{J} = \frac{0.5 \times 6 \times 4.5^3}{3.337} \quad J = 3.333 \text{ in}^3$$

SHEET 2

$$r = \frac{4.05 \text{ in}^2}{1.9094 \text{ lb/in}^2} \quad \text{Torsion}$$

$$r_{\text{direct}} = \frac{F}{A} = \frac{0.5}{0.707 \times 0.5 \times 5} = 0.2829 \text{ lb/in}^2$$

$$\text{Max Resultant Stress} = \sqrt{1.9094^2 + 0.2829^2}$$

$$r = 1.9302 \text{ lb/in}^2$$