FUEL OIL HANDLING SYSTEM DATA
Pressure Gauge Terminology

| "Pressure Gauge" Name: | "Compound" | "Gauge" | "Absolute" | "Gauge" | "Absolute" | "Gauge" |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Units | psig | psig | psia | " Hg | " Hg | " H20 |
|  | 20 | 20 | 34.7 | 40.72 | 70.649 | 554.2 |
|  | 19 | 19 | 33.7 | 38.684 | 68.613 | 526.49 |
|  | 18 | 18 | 32.7 | 36.648 | 66.577 | 498.78 |
|  | 17 | 17 | 31.7 | 34.612 | 64.541 | 471.07 |
|  | 16 | 16 | 30.7 | 32.576 | 62.505 | 443.36 |
|  | 15 | 15 | 29.7 | 30.54 | 60.469 | 415.65 |
|  | 14 | 14 | 28.7 | 28.504 | 58.433 | 387.94 |
|  | 13 | 13 | 27.7 | 26.468 | 56.397 | 360.23 |
|  | 12 | 12 | 26.7 | 24.432 | 54.361 | 332.52 |
|  | 11 | 11 | 25.7 | 22.396 | 52.325 | 304.81 |
|  | 10 | 10 | 24.7 | 20.36 | 50.289 | 277.1 |
|  | 9 | 9 | 23.7 | 18.324 | 48.253 | 249.39 |
|  | 8 | 8 | 22.7 | 16.288 | 46.217 | 221.68 |
|  | 7 | 7 | 21.7 | 14.252 | 44.181 | 193.97 |
|  | 6 | 6 | 20.7 | 12.216 | 42.145 | 166.26 |
|  | 5 | 5 | 19.7 | 10.18 | 40.109 | 138.55 |
|  | 4 | 4 | 18.7 | 8.144 | 38.073 | 110.84 |
|  | 3 | 3 | 17.7 | 6.108 | 36.037 | 83.13 |
|  | 2 | 2 | 16.7 | 4.072 | 34.001 | 55.42 |
|  | 1 | 1 | 15.7 | 2.036 | 31.965 | 27.71 |
| Atmospheric | 0 | 0 | 14.7 | 0 | 29.92 | 0 |
|  | 2 | -0.982 | 13.718 | -2 | 27.929 | -27.22 |
|  | 4 | -1.965 | 12.735 | -4 | 25.929 | -54.44 |
|  | 6 | -2.947 | 11.753 | -6 | 23.929 | -81.66 |
|  | 8 | -3.929 | 10.771 | -8 | 21.929 | -108.9 |
|  | 10 | -4.912 | 9.7884 | -10 | 19.929 | -136.1 |
|  | 12 | -5.894 | 8.8061 | -12 | 17.929 | -163.3 |
|  | 14 | -6.876 | 7.8238 | -14 | 15.929 | -190.5 |
|  | 16 | -7.859 | 6.8415 | -16 | 13.929 | -217.8 |
|  | 18 | -8.841 | 5.8591 | -18 | 11.929 | -245 |
|  | 20 | -9.823 | 4.8768 | -20 | 9.9292 | -272.2 |
|  | 22 | -10.81 | 3.8945 | -22 | 7.9292 | -299.4 |
|  | 24 | -11.79 | 2.9122 | -24 | 5.9292 | -326.6 |
|  | 26 | -12.77 | 1.9299 | -26 | 3.9292 | -353.9 |
|  | 28 | -13.75 | 0.9475 | -28 | 1.9292 | -381.1 |
| Outer Space Vacuum | 29.92 | -14.7 | 0 | -29.92 | 0 | -407.2 |
| Units | " Hg | psig | psia | " Hg | " Hg | " H20 |

## Traditional Compound Pressure Gauge

Reading is
Relative to Local Atmosphere

Reading is
Relative to
Outer Space Vacuum
$\left(60^{\circ} \mathrm{F}\right)$

FUEL OIL HANDLING SYSTEM DATA
Typical Fuel Oil Temperature-Viscosity Curves


The above chart should be used as a guide to determine the proper or minimum temperature to be maintained in oil storage tanks and pipe lines to ensure reliable oil pumping. It can also be used for establishing the required fuel temperature to maintain fuel oil viscosity at the level prescribed by the burner manufacturer.

When using the chart for determining the proper oil temperature for atomization, the operator should obtain from his fuel oil supplier (or by an independent laboratory analysis) the viscosity of the fuel expressed in Centistokes, Saybolt Seconds Universal (SSU) or Saybolt Seconds Furol units. (NOTE: All are expressed referenced to a specific temperature) With this information, the application-specific fuel oil "viscosity vs. temperature" line can be drawn by plotting the
one point provided by the oil supplier and drawing a line through it which is parallel to the others on the graph. At the point where this diagonal line crosses the horizontal line marked with the burner manufacturer's recommended viscosity, read vertically down and note the proper temperature at which this oil should be burned.

When using the chart as a basis for the design of storage tank and piping layouts, a similar minimum temperature can be determined by reading vertically down from that point where the diagonal line crosses the horizontal line marked "Limit of Easy Pumpability." For example, a fuel oil having a viscosity of 30 Centistokes at $154^{\circ} \mathrm{F}$ should be kept in storage and in the pipe lines at a minimum temperature of $99.5^{\circ} \mathrm{F}$ to assure reliable pumping of the fuel.

| Grade of Fuel Oil | No. 1 | No. 2 | No. 4 Light | No. 4 Heavy | No. 5 Light | No. 5 Heavy | No. 6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Percent by Weight |  |  |  |  |  |  |  |
| Sulphur | 0.01 to 0.5 | 0.05 to 1.0 | 0.2 to 2.0 | 0.2 to 2.0 | 0.5 to 3.0 | 0.5 to 3.0 | 0.7 to 3.5 |
| Hydrogen | 13.3 to 14.1 | 11.8 to 13.9 | 10.6 to 13.0 | 10.6 to 13.0 | 10.5 to 12.0 | 10.5 to 12.0 | 9.5 to 12 |
| Carbon | 85.9 to 86.7 | 86.1 to 88.2 | 86.5 to 89.2 | 86.5 to 89.2 | 86.5 to 89.2 | 86.5 to 89.2 | 86.5 to 90.2 |
| Nitrogen | 0.0 to 0.1 | 0.0 to 0.1 | --- | --- | --- | --- | 0.0 to 0.5 |
| Oxygen | --- | --- | --- | --- | --- | --- | 0.0 to 1.5 |
| Ash | --- | --- | 0.0 to 0.1 | 0.0 to 0.1 | 0.0 to 0.1 | 0.0 to 0.1 | 0.0 to 0.5 |
| Gravity |  |  |  |  |  |  |  |
| Degrees API | 40 to 44 | 30 to 40 | 25 to 30 | 20 to 28 | 17 to 22 | 14 to 18 | 8 to 15 |
| Specific Gravity @ 60 F | 0.825 to 0.806 | 0.887 to 0.825 | . 904 to 876 | . 934 to . 887 | . 953 to .922 | . 972 to . 947 | 1.014 to . 9659 |
| $\mathrm{lb} / \mathrm{gal}$ at $60^{\circ} \mathrm{F}$ | 6.87 to 6.71 | 7.39 to 6.87 | 7.529 to 7.296 | 7.778 to 7.387 | 7.935 to 7.676 | 8.099 to 7.882 | 8.448 to 8.043 |
| Pour Point, ${ }^{\circ} \mathrm{F}$ | 0 to -50 | 0 to -40 | -10 to +30 | -10 to +50 | -10 to +50 | -10 to +80 | +15 to +85 |
| Viscosity |  |  |  |  |  |  |  |
| Centistokes at $104^{\circ} \mathrm{F}$ | 1.3 to 2.1 | 1.9 to 3.4 | 1.9 to 5.5 | 5.0 to 24.0 | 24.0 to 58.0 | 58.0 to 168.0 | 260 to 750 |
| SSU at $100^{\circ} \mathrm{F}$ | --- | 32.6 to 37.9 | 32.6 to 45.0 | 45 to 125 | 125 to 300 | 300 to 900 | 900 to 9000 |
| SSF at $122^{\circ} \mathrm{F}$ | --- | --- | --- | --- | --- | 23 to 40 | 45 to 300 |
| BS\&W | --- | 0.0 to 0.1 | 0.01 to 1.0 | 0.01 to 1.0 | 0.05 to 1.0 | 0.05 to 1.0 | 0.05 to 2.0 |
| (\% by vol) |  |  |  |  |  |  |  |
| HHV, Btu/gal, calculated |  |  |  |  |  |  |  |
| Max. | 137,000 | 141,800 | 145,000 | 148,100 | 150,000 | 152,000 | 155,900 |
| Min. | 132,900 | 135,800 | 143,100 | 145,000 | 146,800 | 149,400 | 151,300 |

Grade of Fuel Oil: The American Society for Testing and Materials (ASTM) has standardized on five basic grades, designated as Nos. 1, 2, 4, 5, and 6. Grades Nos. 4 and 5 are subdivided into light and heavy. The oil's viscosity determines into which subdivision it is classed.

Percent by Weight: The fuel's elements are expressed as a percentage of the fuel's total weight.

Gravity: The unit weight of a liquid in Ibs./gal. is the density of that liquid. The ratio of unit weight, or density of any liquid to the density of water is the Specific Gravity (SG) of that liquid. The density of water at $60^{\circ} \mathrm{F}$ is 8.328 lbs . The oil industry uses the API Gravity or "Gravity" scale. The relationship between API Gravity and specific gravity is as follows:

Degrees API Gravity $=\left(141.5 \div\right.$ SG at $\left.60^{\circ} \mathrm{F}\right)-131.5$.
Thus, an oil with a specific gravity of 1.0 would have an API Gravity of ( $141.5 \div 1.0$ ) - $131.5=10.0$ degrees API.

Pour Point: The Pour Point temperature is $5^{\circ} \mathrm{F}$ above the point where the oil congeals into a semi-fluid or a solid.

Viscosity: Viscosity is the measure of the oil's resistance to flow, or simply expressed as its "thickness" or "thinness." Kinematic Viscosity is usually given in terms of Centistokes,

SSU (Saybolt Seconds Universal at $100^{\circ} \mathrm{F}$ ) or SSF (Saybolt Seconds Furol at $122^{\circ} \mathrm{F}$ ). Absolute viscosity is given in terms of Centipoises and can be used to calculate Kinematic Viscosity as follows:

Kinematic viscosity (centistokes) = Absolute viscosity (centipoises) $\div$ specific gravity (SG)

## AND

Kinematic viscosity (SSU) = Kinematic viscosity (centistokes) 4.6347

## OR

Kinematic viscosity (SSF) = Kinematic viscosity (centistokes) x 0.4717

BS\&W or Bottom Sediments and Water: BS\&W are non-petroleum contaminates sometimes found in fuel oils. Some of the problems that can be associated with high levels of BS\&W are erratic and unsteady combustion, sparking and spitting of the flame, flashback, plugging of burner tips and screens, loss of heat release and/or erosion of burner tips and mechanical parts.

HHV or Higher Heating Value: The HHV is the total heat content of a given measure of fuel including the latent heat of evaporation of the water vapor formed during combustion. The Lower Heating Value assumes that the latent heat is not recovered because the water vapor is not condensed. When performing calculations for combustion or appliance sizing, always use the HHV.

Due to the thermal expansion and contraction of petroleum products, all are purchased and sold based on its volume at $60^{\circ} \mathrm{F}$. Therefore, all petroleum products are corrected to this temperature by using a "correction factor". This factor converts quantities of oil at different temperatures to a comparable volume at a standard temperature.

When mechanical flow meters or differential pressure type flow elements are used for determining usage or for efficiency calculations, the reading must be temperature compensated to provide an accurate reading.

To convert gross gallons at the loading and unloading temperature to net gallons at $60^{\circ} \mathrm{F}$, the temperature, the API Gravity of the oil and the coefficient of expansion factor must be known. A "rough approximation" of net gallons can be obtained from the equation provided. For a more precise conversion consult the Factory or the "Manual of Petroleum Measurement Standards" jointly issued by the American Society for Testing and Materials, the American Petroleum Institute and the Institute of Petroleum. Included in these Standards are Table 5B (Correction of Observed API Gravity to API Gravity at $60^{\circ} \mathrm{F}$ ) and Table 6B (Correction of Volume to $60^{\circ} \mathrm{F}$ against API Gravity at $60^{\circ} \mathrm{F}$ ). Table 5 B is used to
correct the observed gravity and temperature to the gravity at $60^{\circ} \mathrm{F}$. Table 6 B is used to obtain the coefficient of expansion factor from the observed gravity and temperature and is used to convert gross to net gallons.
"Rough Approximation" Method:
Correction Factor $=1-(\Delta \mathrm{T} \times$ Multiplier $)$

| Oil API | Multiplier |
| :---: | :---: |
| $0^{\circ}$ to $14.9^{\circ} \mathrm{API}$ | 0.00035 |
| $15^{\circ}$ to $34.9^{\circ} \mathrm{API}$ | 0.0004 |
| $35^{\circ}$ to $50.9^{\circ} \mathrm{API}$ | 0.0005 |

## Example:

Oil having $17^{\circ} \mathrm{API}$ is clocked through a positive displacement meter at 565 GPH . The oil is $190^{\circ} \mathrm{F}$ at the meter. Find the corrected (i.e. $60^{\circ} \mathrm{F}$ ) volumetric flow.

$$
190-60=130^{\circ} \Delta \mathrm{T}
$$

Correction Factor $=1-(130 \times 0.0004)=0.9480$
Corrected Volumetric Flow $=565 \times 0.9480=535.62$ GPH

## Energy Required To Heat \#6 Oil

## Electric

Watts $=1.25 \times \operatorname{GPH} \times \Delta \mathrm{T}\left({ }^{\circ} \mathrm{F}\right)$
Amps (single phase) $=\frac{\text { watts }}{\text { volts }}$
Amps (three phase) $=\frac{\text { watts }}{\text { volts } \times 1.73}$

## Example:

To heat 600 GPH of $\# 6$ oil from $90^{\circ} \mathrm{F}\left(32^{\circ} \mathrm{C}\right)$ to $150^{\circ} \mathrm{F}$
( $65.5^{\circ} \mathrm{C}$ ):
$\Delta \mathrm{T}=60^{\circ} \mathrm{F}\left(15.5^{\circ} \mathrm{C}\right)$
Watts $=1.25 \times 600 \times 60=45,000$
KW = 45
Amps at $460 / 3 / 60=56.5$

## Steam

$\mathrm{lbs} / \mathrm{hr}$ steam $=\frac{\mathrm{lbs} / \mathrm{hr} \text { oil } \mathrm{x} \Delta \mathrm{T}}{1920}(\# 6$ oil $\& 5$ psi steam $)$

$$
=\frac{\mathrm{gph} \times \mathrm{lb} / \mathrm{gal} \mathrm{x} \Delta \mathrm{~T}}{1920}
$$

## Example:

To heat 600 GPH of $\# 6$ oil from $90^{\circ} \mathrm{F}\left(32^{\circ} \mathrm{C}\right)$ to $150^{\circ} \mathrm{F}$ ( $65.5^{\circ} \mathrm{C}$ ):


## FUEL OIL HANDLING SYSTEM DATA

Simplex Strainer Model No. 72
Approximate Strainer Pressure Drops in Inches of Mercury
(1" $\mathrm{Hg}=0.49 \mathrm{PSI}=13.622 \mathrm{IN}_{2} \mathrm{O}$ )

Number 2 Fuel Oil
(with clean 40 mesh baskets)

| $\begin{gathered} \text { FLOW } \\ \text { GPH } \end{gathered}$ | 1/2" | $3 / 4 "$ | 1" | $11 / 4 "$ | $11 / 2^{\prime \prime}$ | 2" |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | *** | *** | *** | *** | *** | *** |
| 45 | *** | *** | *** | *** | *** | *** |
| 90 | 0.1 | *** | *** | *** | *** | *** |
| 160 | 0.4 | 0.2 | *** | *** | *** | *** |
| 350 | 0.9 | 0.4 | 0.2 | *** | *** | *** |
| 700 | 2.8 | 1.1 | 0.5 | 0.3 | *** | *** |
| 1100 | 6.1 | 2.4 | 1.2 | 0.6 | 0.3 | *** |
| 1900 | $x X X$ | 7.1 | 3.2 | 1.7 | 0.9 | 0.4 |
| 3000 | $x X X$ | $x x x$ | 8.1 | 4 | 2.4 | 1 |
| 5000 | XXX | XXX | $x X X$ | 11.2 | 6.1 | 2.5 |
| 7500 | $x x x$ | $x x x$ | $x x x$ | $x x x$ | 11.2 | 4.2 |
| 10000 | $x x x$ |  | $x x x$ | $x \times x$ | $x x x$ | 8.1 |

Number 6 Fuel Oil at 5000 SSU
(with clean 3/64" perforated baskets)

| FLOW <br> GPH | $\mathbf{1} / \mathbf{2}^{\prime \prime}$ | $3 / \mathbf{4}^{\prime \prime}$ | $\mathbf{1 "}$ | $\mathbf{1} 1 / \mathbf{4}^{\prime \prime}$ | $\mathbf{1} 1 / \mathbf{2}^{\prime \prime}$ | $\mathbf{2 "}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 45 | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 90 | 0.9 | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 160 | 1.0 | 0.4 | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 350 | 1.3 | 0.7 | 0.5 | $* * *$ | $* * *$ | $* * *$ |
| 700 | 2.0 | 0.8 | 0.6 | 0.2 | $* * *$ | $* * *$ |
| 1100 | 5.7 | 2.5 | 1.0 | 0.6 | 0.3 | $* * *$ |
| 1900 | $x x x$ | 5.7 | 2.8 | 1.7 | 0.8 | 0.3 |
| 3000 | $x x x$ | $x x x$ | 7.7 | 4.0 | 2.2 | 0.9 |
| 5000 | $x x x$ | $x x x$ | $x x x$ | 9.8 | 5.1 | 2.1 |
| 7500 | $x x x$ | $x x x$ | $x x x$ | $x x x$ | $x x x$ | 11.2 |
| 10000 | $x x x$ | $x x x$ | $x x x$ | $x x x$ | $x x x$ | $x x x$ |

FUEL OIL HANDLING SYSTEM DATA
Duplex Strainer Model No. 53
Approximate Strainer Pressure Drops in Inches of Mercury

Number 2 Fuel Oil
(with clean 40 mesh baskets)

| FLOW <br> GPH | $\mathbf{3} / \mathbf{4}^{\prime \prime}$ | $\mathbf{1 "}$ | $\mathbf{1} \mathbf{1 / 4 \prime}$ | $\mathbf{1} \mathbf{1 / 2 "}$ | $\mathbf{2 "}$ | $\mathbf{2} \mathbf{1 / 2 "}$ | $\mathbf{3 "}$ | $\mathbf{4 "}$ | $\mathbf{5 "}$ | $\mathbf{6 " \prime}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 45 | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 90 | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 160 | 0.1 | 0.1 | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 350 | 0.4 | 0.3 | 0.2 | 0.1 | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 700 | 2 | 1.8 | 0.8 | 0.5 | 0.15 | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 1100 | 4.2 | 4 | 1.8 | 1.2 | 0.4 | 0.2 | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 1900 | $x x x$ | 12 | 5 | 3.2 | 1.6 | 0.4 | 0.2 | $* * *$ | $* * *$ | $* * *$ |
| 3000 | $x x x$ | $x x x$ | 12 | 7.6 | 2.5 | 1.1 | 0.5 | 0.2 | $* * *$ | $* * *$ |
| 5000 | $x x x$ | $x x x$ | $x x x$ | $x x x$ | 7.2 | 3 | 1.5 | 0.4 | 0.2 | $* * *$ |
| 7500 | $x x x$ | $x x x$ | $x x x$ | $x x x$ | $x x x$ | 6 | 3 | 0.9 | 0.4 | 0.2 |
| 10000 | $x x x$ | $x x x$ | $x x x$ | $x x x$ | $x x x$ | 10.4 | 5 | 1.5 | 0.7 | 0.3 |

Number 6 Fuel Oil at 5,000 SSU
(with clean $3 / 64$ " perforated baskets)

| FLOW <br> GPH | $\mathbf{3} / \mathbf{4}^{\prime \prime}$ | $\mathbf{1 "}$ | $\mathbf{1} \mathbf{1 / 4 "}$ | $\mathbf{1} \mathbf{1 / 2 "}$ | $\mathbf{2 "}$ | $\mathbf{2} \mathbf{1 / 2 "}$ | $\mathbf{3 "}$ | $\mathbf{4 "}$ | $\mathbf{5 "}$ | $\mathbf{6 " \prime}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{2 5}$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 45 | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 90 | 0.1 | 0.1 | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 160 | 0.4 | 0.3 | 0.1 | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 350 | 1.3 | 1.2 | 0.5 | 0.3 | 0.1 | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 700 | 4.2 | 4 | 1.7 | 1.1 | 0.4 | $* * *$ | $* * *$ | $* * *$ | $* * *$ | $* * *$ |
| 1100 | $x x x$ | 9.5 | 4 | 2.5 | 0.8 | 0.4 | 0.2 | $* * *$ | $* * *$ | $* * *$ |
| 1900 | $x x x$ | $x x x$ | 11.4 | 7.1 | 2.4 | 1.1 | 0.5 | 0.2 | $* * *$ | $* * *$ |
| 3000 | $x x x$ | $x x x$ | $x x x$ | 16.3 | 5.5 | 2.4 | 1.1 | 0.4 | $* * *$ | $* * *$ |
| 5000 | $x x x$ | $x x x$ | $x x x$ | $x x x$ | 15.3 | 6.6 | 3.3 | 1 | 0.4 | 0.2 |
| 7500 | $x x x$ | $x x x$ | $x x x$ | $x x x$ | $x x x$ | 13.9 | 6.5 | 2 | 0.9 | 0.4 |
| 10000 | $x x x$ | $x x x$ | $x x x$ | $x x x$ | $x x x$ | $x x x$ | 11.2 | 3.5 | 1.5 | 0.8 |

*** Indicates insignificant pressure loss
xxx Indicates excessive pressure loss

FUEL OIL HANDLING SYSTEM DATA
Contents of Horizontal Cylindrical Tanks
Percent of Total Volume Filled vs. Percent of Liquid Depth

| Depth \% | Gallons \% | Depth \% | Gallons \% | Depth \% | Gallons \% | Depth \% | Gallons \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0 | 0.00 | 25 | 19.6 | 50 | 50.0 | 76 | 81.5 |
| 1 | 0.2 | 26 | 20.7 | 51 | 51.3 | 77 | 82.6 |
| 2 | 0.5 | 27 | 21.8 | 52 | 52.5 | 78 | 83.7 |
| 3 | 0.9 | 28 | 22.9 | 53 | 53.8 | 79 | 84.7 |
| 4 | 1.3 | 29 | 24.1 | 54 | 55.1 | 80 | 85.8 |
| 5 | 1.9 | 30 | 25.2 | 55 | 56.4 | 81 | 86.8 |
| 6 | 2.4 | 31 | 26.4 | 56 | 57.6 | 82 | 87.8 |
| 7 | 3.1 | 32 | 27.6 | 57 | 58.9 | 83 | 88.8 |
| 8 | 3.7 | 33 | 28.8 | 58 | 60.1 | 84 | 89.7 |
| 9 | 4.5 | 34 | 30.0 | 59 | 61.4 | 85 | 90.6 |
| 10 | 5.2 | 35 | 31.2 | 60 | 62.6 | 86 | 91.5 |
| 11 | 6.0 | 36 | 32.4 | 61 | 63.9 | 87 | 92.4 |
| 12 | 6.8 | 37 | 33.6 | 62 | 65.1 | 88 | 93.2 |
| 13 | 7.6 | 38 | 34.9 | 63 | 66.4 | 89 | 94.0 |
| 14 | 8.5 | 39 | 36.1 | 64 | 67.6 | 90 | 94.8 |
| 15 | 9.4 | 40 | 37.4 | 65 | 68.8 | 91 | 95.5 |
| 16 | 10.3 | 41 | 38.6 | 66 | 70.0 | 92 | 96.3 |
| 17 | 11.3 | 42 | 39.9 | 68 | 72.4 | 93 | 96.9 |
| 18 | 12.2 | 43 | 41.1 | 69 | 73.6 | 94 | 97.6 |
| 19 | 13.2 | 44 | 42.4 | 70 | 74.8 | 95 | 98.1 |
| 20 | 14.2 | 45 | 43.6 | 71 | 75.9 | 96 | 98.7 |
| 21 | 15.3 | 46 | 44.9 | 72 | 77.1 | 97 | 99.1 |
| 22 | 16.3 | 47 | 46.2 | 73 | 78.2 | 98 | 99.5 |
| 23 | 17.4 | 48 | 47.5 | 74 | 79.3 | 99 | 99.8 |
| 24 | 18.5 | 49 | 48.7 | 75 | 80.4 | 100 | 100.0 |

Note: These figures apply only to tanks with flat ends, not to tanks with dished ends. For greater accuracy, consult the stick chart prepared by the tank manufacturer.

Tank With
Flat Ends

## Example:

A 12 foot (144") diameter tank has 98.5 inches of oil as measured by the stick. Dividing the depth (98.5") by the tank inside diameter (144"), yields 68\% tank depth. From the table, the volume is $72.4 \%$ of capacity. For a 20,000 gallon tank, the contents would be approximately 14,480 gallons.

