

PREINSULATED PIPES FOR LOW TEMPERATURE UTILITIES FLEXIBLE PIPE SYSTEMS M -PEX

made acc. Standard PN-EN 13941 (EN 13941) " Design and installation of preinsulated bonded pipe systems for district heating" - Appendix D

MR-6/I-110 (180)

Output data:

flow pipeline temp. t_f =	70,00	°C
return pipeline temp. t_r =	50,00	°C
soil temp. t_s =	10,00	°C
pipeline axis depth (caunting from soil surface) Z =	0,69	m
counting from soil surface) z =	0,60	m
Corrected value of depth Z , so that the surface transition insulance R_o at the soil surface is included Z_c =	0,77	m
Soil penetration coefficient λ_s =	1,20	W/mK
for wet soil from 1,5 W/(mK) to 2 W/(mK), for dry sand about . 1,0 W/(mK)		
Casing tube external diameter D_o =	0,1800	m
wall thickness of casing tube g_o =	0,0030	m
Insulation external diameter D_{iz} =	0,1740	m
Medium pipe diameter PEX D_{z1} =	0,1100	m
wall thickness of PEX tube g_1 =	0,0100	m
Distance in light between casing tubes a =	0,2000	m
Distance beetwen pipleine axes C =	0,3800	m
coefficient of thermal conductivity for PUR insulation systems M-PEX λ_{iz} =	0,0245	W/mK
coefficient of thermal conductivity for medium pipe PEX wg DIN 52612 λ_{PEX} =	0,3800	W/mK
coefficient of thermal conductivity for casing tube PE-LD λ_{PE-LD} =	0,4300	W/mK

Q_f - heat losses on flow pipeline

Q_r - heat losses on return pipeline

$$Q_f = U_1 \times (t_f - t_s) - U_2 \times (t_r - t_s)$$

$$Q_r = U_1 \times (t_r - t_s) - U_2 \times (t_f - t_s)$$

Overall heat loss is:

$$Q_f + Q_r = 2 \times (U_1 - U_2) \times \left(\frac{t_f + t_r}{2} - t_s \right)$$

gdzie:

U_1 i U_2 - heat loss coefficient

t_f i t_r - temp.in flow and return pipeline

t_s - undisturbed soil temp.at depth "z"

$$U_1 = \frac{R_s + R_i + R_{PEX} + R_{PE-LD}}{(R_s + R_i + R_{PEX} + R_{PE-LD})^2 - R_h^2}$$

$$U_2 = \frac{R_h}{(R_s + R_i + R_{PEX} + R_{PE-LD})^2 - R_h^2}$$

The overall heat loss coefficient:

$$U_1 - U_2 = \frac{1}{R_i + R_s + R_{PEX} + R_{PE-LD} + R_h}$$

where:

R_i - insulance of insulating material

$$R_{iz} = \frac{1}{2\pi\lambda_{iz}} \ln \frac{D_{iz}}{d_z}$$

R_{PEX} - insulance of medium pipe PEX

$$R_{PEX} = \frac{1}{2\pi\lambda_{PEX}} \ln \frac{D_z}{(D_z - 2 \times g)}$$

R_{PE-LD} - insulance of casing tube PE-LD

$$R_{PE-LD} = \frac{1}{2\pi\lambda_{PE-LD}} \ln \frac{D_o}{(D_o - 2 \times g_o)}$$

R_s - insulance of the soil

$$R_s = \frac{1}{2\pi\lambda_s} \ln \frac{4Z_c}{D_o} \quad \text{gdzie:} \quad Z_c = Z + R_o \times \lambda_{gr}$$

Z_c - Corrected value of depth Z , so that the surface transition insulance R_o at the soil surface is included

$$R_o = 0,0685 \text{ m}^2\text{K/W}$$

R_h - insulance of heat exchange between flow and return pipe

$$R_h = \frac{1}{4\pi\lambda_y} \ln \left(1 + \left(\frac{2Z_c}{C} \right)^2 \right)$$

Heat loss of pipeline laying directly in the ground

$$R_{iz} = \frac{1}{2 \times 3,1416 \times 0,0245} \ln \frac{0,1740}{0,1100} = 2,9790 \text{ mK/W}$$

$$R_{PE-LD} = \frac{1}{2 \times 3,1416 \times 0,4300} \ln \frac{0,1800}{0,1740} = 0,0125 \text{ mK/W}$$

$$R_{PEX} = \frac{1}{2 \times 3,1416 \times 0,3800} \ln \frac{0,1100}{0,0900} = 0,0840 \text{ mK/W}$$

$$R_h = \frac{1}{4 \times 3,1416 \times 1,2000} \ln \left(1,00 + \left(\frac{2 \times 0,7700}{0,3800} \right)^2 \right) = 0,1895 \text{ mK/W}$$

$$R_s = \frac{1}{2 \times 3,1416 \times 1,2000} \ln \left(\frac{4 \times 0,7700}{0,1800} \right) = 0,3766 \text{ mK/W}$$

$$U1 = \frac{2,9790 + 0,0125 + 0,0840 + 0,3766}{(0,3766 + 2,9790 + 0,0125 + 0,0840)^2 - (0,1895)^2} = 0,2906 \text{ W/mK}$$

$$U2 = \frac{0,1895}{(0,3766 + 2,9790 + 0,0125 + 0,0840)^2 - (0,1895)^2} = 0,0159 \text{ W/mK}$$

$$U1-U2 = \frac{1}{2,9790 + 0,0125 + 0,0840 + 0,1895 + 0,3766} = 0,2746 \text{ W/mK}$$

Heat losses in flow pipeline:

$$Q_f = 0,2906 \times (70,00 - 10,00) - 0,0159 \times (50,0000 - 10,00) = 16,8000 \text{ W/m}$$

Heat losses in return pipeline:

$$Q_r = 0,2906 \times (50,00 - 10,00) - 0,0159 \times (70,00 - 10,00) = 10,6700 \text{ W/m}$$

Heat loss in both pipelines:

$$Q_f + Q_r = 27,4700 \text{ W/m}$$

The overall heat loss:

$$Q_f + Q_r = 2,00 \times \left(\frac{70,00 + 50,00}{2} - 10,00 \right) = 27,4700 \text{ W/m}$$

made acc. Standard PN-EN 13941+A1 (EN 13941:2009+A1:2010) " Design and installation of preinsulated bonded pipe systems for district heating" - Appendix D

MR-6/T-110(180)

flow pipeline temp. t_f =	70,00	°C
return pipeline temp. t_r =	50,00	°C
soil temp. t_s =	10,00	°C
counting from soil surface z =	0,60	m
pipeline axis depth (caunting from soil surface) Z =	0,69	m
Corrected value of depth Z , so that the surface transition insulance R_o at the soil surface is included Z_c =	0,77	m
Soil penetration coefficient λ_s =	1,20	W/mK
for wet soil from 1,5 W/(mK) to 2 W/(mK), for dry sand about . 1,0 W/(mK)		
Casing tube external diameter D_c =	0,1800	m
wall thickness of casing tube g_o =	0,0030	m
Insulation external diameter D_{PUR} =	0,1740	m
Medium pipe diameter d_o =	0,1100	m
Distance in light between casing tubes a =	0,2000	m
Distance beetwen pipeline axes C =	0,3800	m
coefficient of thermal conductivity for PUR insulation λ_i =	0,0245	W/mK

Q_f - heat losses on flow pipeline

Q_r - heat losses on return pipeline

$$Q_f = U_1 \times (t_f - t_s) - U_2 \times (t_r - t_s) \quad Q_r = U_1 \times (t_r - t_s) - U_2 \times (t_f - t_s)$$

Overall heat loss is:

$$Q_f + Q_r = 2 \times (U_1 - U_2) \times \left(\frac{t_f + t_r}{2} - t_s \right) \quad U_1 - U_2 = \frac{1}{R_s + R_i + R_h}$$

where:

U_1 i U_2 - heat loss coefficient

t_f i t_r - temp.in flow and return pipeline

t_s - undisturbed soil temp.at depth "z"

$$U_1 = \frac{R_s + R_i}{(R_s + R_i)^2 - R_h^2}$$

$$U_2 = \frac{R_h}{(R_s + R_i)^2 - R_h^2}$$

where:

R_i - insulance of insulating material

$$R_i = \frac{1}{2\pi\lambda_i} \ln \frac{D_{PUR}}{d_o}$$

R_s - insulance of the soil

$$R_s = \frac{1}{2\pi\lambda_s} \ln \frac{4Z_c}{D_c}$$

where: $Z_c = Z + R_o \times \lambda_s$

Z_c - Corrected value of depth Z , so that the surface transition insulance R_o at the soil surface is included

$$R_o = 0,0685 \quad m^2K/W$$

R_h - insulance of heat exchange between flow and return pipe

$$R_h = \frac{1}{4\pi\lambda_s} \ln \left(1 + \left(\frac{2Z_c}{C} \right)^2 \right)$$

Heat loss of single pipeline laying directly in the ground

$$R_i = \frac{1}{2,00 \times 3,1416 \times 0,0245} \ln \frac{0,1740}{0,1100} = 2,9790 \text{ mK/W}$$

$$R_s = \frac{1}{2,00 \times 3,1416 \times 1,2000} \ln \frac{4 \times 0,7722}{0,1800} = 0,3770 \text{ mK/W}$$

$$R_h = \frac{1}{4,00 \times 3,1416 \times 1,2000} \times \ln \left[1,00 + \left(\frac{1,54}{0,38} \right)^2 \right] = 0,1899 \text{ mK/W}$$

$$U_1 \cdot U_2 = \frac{1}{0,3770 + 2,9790 + 0,1899} = 0,2820 \text{ W/mK}$$

$$U_1 = \frac{0,3770 + 2,9790}{(0,3770 + 2,9790)^2 - 0,1899^2} = 0,2989 \text{ W/mK}$$

$$U_2 = \frac{0,1899}{(0,3770 + 2,9790)^2 - 0,1899^2} = 0,0169 \text{ W/mK}$$

Heat losses in flow pipeline:

$$Q_f = 0,30 \times [70,00 - 10,00] - 0,02 \times [50,00 - 10,00] = 17,26 \text{ W/m}$$

Heat losses in return pipeline:

$$Q_r = 0,30 \times [50,00 - 10,00] - 0,02 \times [70,00 - 10,00] = 10,94 \text{ W/m}$$

Heat loss in both pipelines:

$$Q_f + Q_r = 28,201 \text{ W/m}$$

$$U_1 \cdot U_2 = \frac{1,00}{0,3770 + 2,9790 + 0,1899} = 0,2820 \text{ W/mK}$$

Overall heat loss:

$$Q_f + Q_r = 2,00 \times \left(0,30 - 0,02 \times \left[\frac{70,00 + 50,00}{2} - 10,00 \right] \right) = 28,20 \text{ W/m}$$

wykonane wg normy PN-EN 15698-1 luty 2009 (EN-15698-1:2009), PN-EN 15698-1:2008

Rura MR-6/IF2x50(160)

Temperatura rurociagu zasilającego $T_{1=}$	70	°C
Temperatura rurociagu zasilającego $T_{2=}$	50	°C
Temperatura gruntu $T_{0=}$	10	°C
Półowa odległości między środkami rur D	0,03	m
Średnica rury osłonowej D_z	0,16	m
Grubość ścianki rury osłonowej g_z	0,003	m
Średnica rury przewodowej D_{p1}	0,05	m
Grubość ścianki rury przewodowej g_{p1}	0,0046	m
Średnica rury przewodowej D_{p2}	0,05	m
Grubość ścianki rury przewodowej g_{p2}	0,0046	m
Odległość między rurami przewodowymi s	0,01	m
Promień rury osłonowej r_1	0,077	m
Promień rury przewodowej r_2	0,0204	m
Promień rury przewodowej r_3	0,0204	m
Przewodność pianki PUR λ_{PU}	0,0245	W*m ⁻¹ *K ⁻¹

Liniowy współczynnik przenikania ciepła (U) można opisać w następujący sposób:

$$U = \frac{q_{\text{całkowity}}}{\left(\frac{T_1 + T_2}{2} - T_0 \right)} \quad [\text{W} \cdot \text{m}^{-1} \cdot \text{K}^{-1}]$$

Przewodność cieplną λ_{PU} można wyrazić następująco:

$$q_{\text{całkowity}} = 4\pi * \lambda_{PU} * h_s * \left(\frac{T_1 + T_2}{2} - T_0 \right) \quad [\text{W} \cdot \text{m}^{-1}]$$

Przy tym:

$$h_s^{-1} = \ln \left(\frac{r_1^2}{2D * r_2} \right) - \ln \left(\frac{r_1^4}{r_1^4 - D^4} \right) - \frac{\left(\frac{r_2}{2 * D} + \frac{2r_2 * D^3}{r_1^4 - D^4} \right)^2}{1 + \left(\frac{r_2}{2D} \right)^2 - \left(\frac{2r_2 * r_1^2 * D}{r_1^4 - D^4} \right)^2}$$

Obliczenie współczynnika utraty ciepła

$$h_s^{-1} = \ln \frac{0,00593}{0,00122} - \ln \frac{0,00003515}{0,00003434} - \frac{\left(\frac{0,02040}{0,06000} + \frac{0,00000110}{0,00003434} \right)^2}{1 + \left(\frac{0,02040}{0,06000} \right)^2 - \left(\frac{0,00000726}{0,00003434} \right)^2} =$$

$$= 1,58117 - 0,0233138 - \frac{0,13841}{1,07090} = 1,4286$$

Obliczenie utraty ciepła

$$q_{\text{całkowity}} = 12,5664 * 0,0245 * 0,7000 * \left(\frac{120}{2} - 10 \right) = 10,7757 \quad [\text{W*m-1}]$$

Obliczenie liniowego współczynnika przenikania ciepła

$$U = \frac{10,7757}{\left(\frac{120}{2} - 10 \right)} = 0,2155 \quad [\text{W*m-1*K-1}]$$