TIE ROD END DESIGN TUTORIAL

- THE FOLLOWING IS A SIMPLIFIED STEP-BY-STEP GUIDE INTENDED TO ILLUSTRATE THE DECISIONS AND COMPROMISES INVOLVED IN DESIGNING A TIE ROD END.
- THE PROCESS FOR DESIGNING ANY BALL JOINT IS VERY SIMILAR

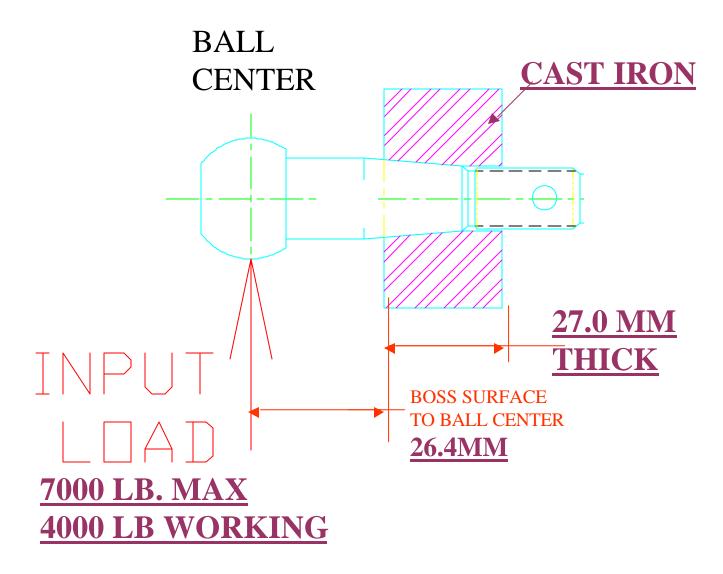
DESIGNING A ROD END FOR THE 20XX HYPTHETICAL LIGHT TRUCK • FROM THE CUSTOMER WE LEARN: - 1) PT 12 RELATIVE TO KNUCKLE <u>26.4MM</u> Inte code _____ 2) LOADS 7000 MAX, 4000 WORKING - 3) PACKAGE NO ISSUES, 30MM FROM BRAKE **ROTOR DUST SHIELD** - 4) ARTICULATION TRAVEL +/- 18 DEGREES - 5) MATING PARTS DETAIL CAST IRON 27MM THICK, STUD UP, CASTLE NUT/COTTERPIN - 6) APPLICATION COMMERCIAL LIGHT TRUCK, **R&P W/ M16X 1.5 ROD** - 7) GREASABLE / NON-GREASABLE <u>GREASABLE</u>





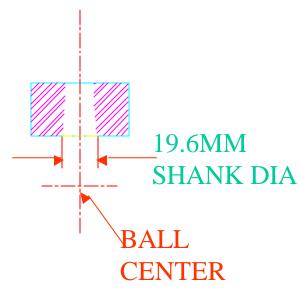


BALL STUD DESIGN INPUTS



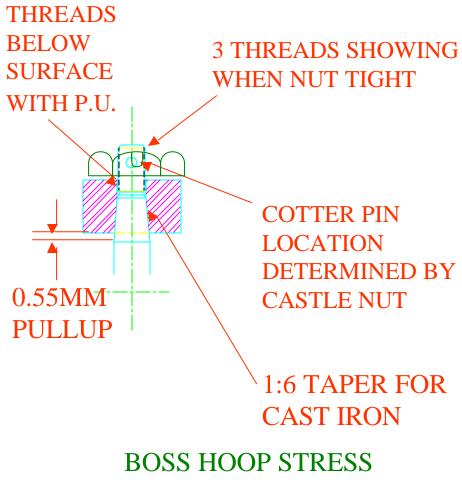
BALL STUD SHANK SIZING

- 7000 LB MAX LOAD
- 4000 LB WORKING LOAD
- 26.4MM CANTILEVER BEAM
- SHEAR-MOMENT CALCULATION
- 25% F.S.
- EFFECTIVE MATL ULT = 242KSI
- EFFECTIVE MATL YEILD = 129KSI
- => SHANK DIA = 19.6MM



TAPER SPECIFICATION

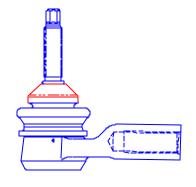
- STEEL BOSS
 - 1:8 TAPER
 - 1.25:1 THICK/DIA
- CAST IRON, ALUMINUM
 - 1:6 TAPER
 - 1.3-1.5 THICK/DIA
- PULL UP
 - STEEL => .4-.7MM
 - CAST IRON => .4-.7MM
 - ALUMINUM =>1.0MM

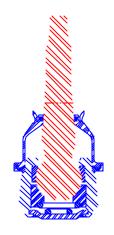


CONE WASHER VS. **TAPERED BALL STUD**

- CONE ADVANTAGES
 - EASY SERVICE REMOVAL
 - SEAL SURFACE **CONTROLLED**
 - CHANGE GAGE LENGTH EASILY
 - GT ADJUSTABLE

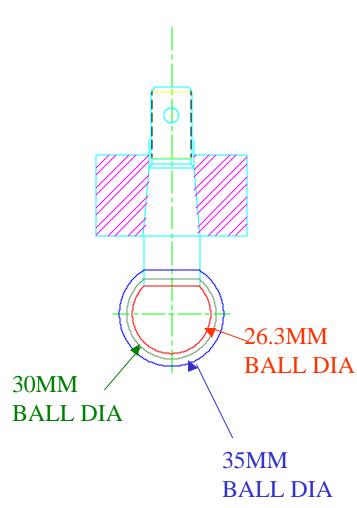
- TAPER ADVANTAGES
 - LOCKING TAPER
 - CARBONITRIDE H.T.
 - LOWER COST
 - LESS SENSITIVE TO NUT TORQUE





BALL SIZING

- LARGER DIA
 - IMPROVES PULL OUT **STRENGTH**
 - REDUCES **BEARING/LUBE** PRESSURE
 - NO ARTICULATION UNDERCUT
- SMALLER DIA
 - MORE ROOM FOR SEAL
 - BETTER PACKAGE
 - LESS EXPENSIVE

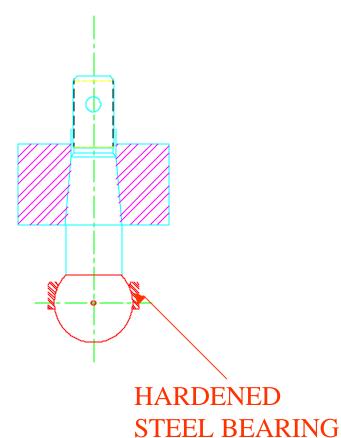


NOW IT GETS COMPLICATED

- BETWEEN THE TOP OF THE BALL AND THE KNUCKLE WE NEED TO PACKAGE:
 - BEARING
 - FORGING
 - SEAL
- AND, IT HAS TO ARTICULATE

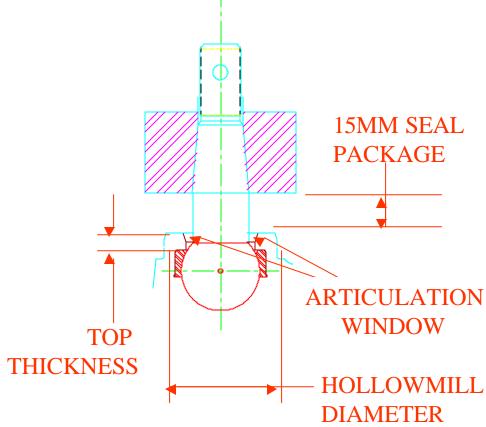
STEEL BEARING PACKAGE FOR A 26MM BALL

- STANDARD HARDENED STEEL **BEARING FOR** 26MM BALL
- EXCELLENT WEAR **CHARACTERISTICS**
- EXCELLENT PULL **OUT STRENGTH**
- HIGHER ROTATING TORQUES



UPPER FORGING PACKAGE FOR A **26MM BALL WITH STEEL BEARING**

- FORGING **CONSIDERATIONS:**
- 5.0MM MIN TOP THICKNESS
- HOLLOWMILL FOR SEAL RETAINER
- ARTICULATION WINDOW

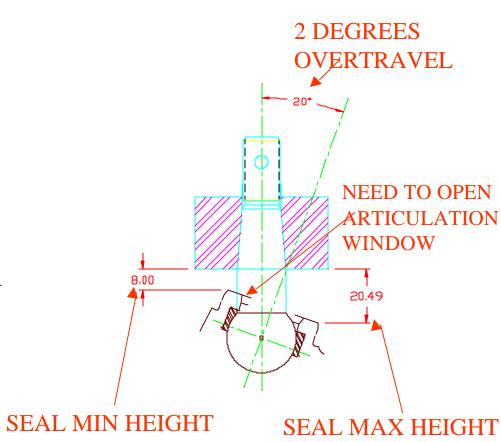




HOLLOWMILL

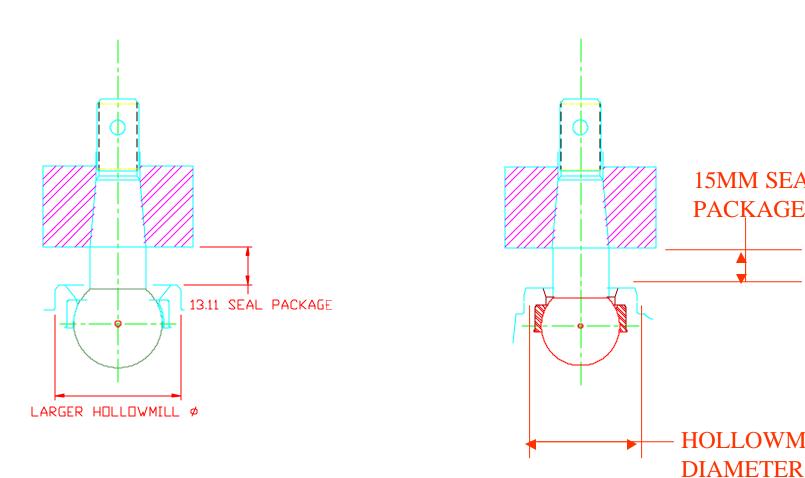
DON'T FORGET ARTICULATION

• SPECIFIED 18 DEGREE **ARTICULATION** ANGLE DRIVES: - SEAL DESIGN REQUIREMENTS - FORGING WINDOW



WHAT HAPPENS IF WE GO TO A 30MM BALL DIAMETER?

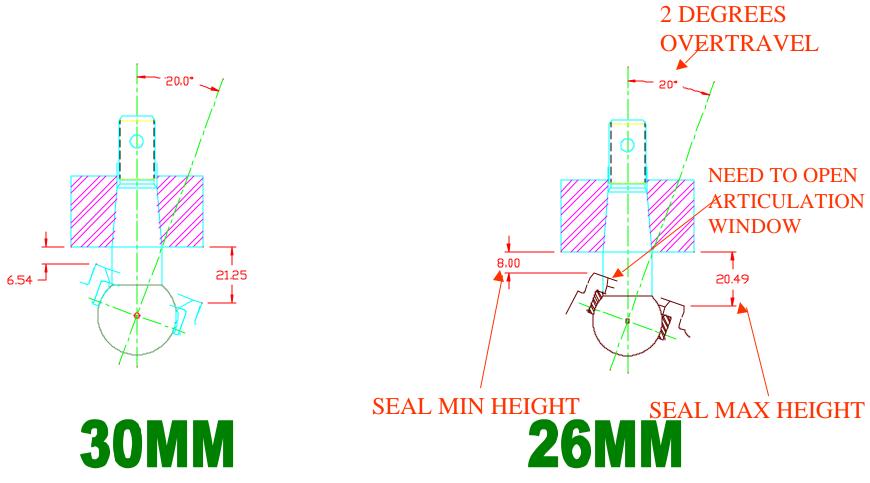
UPPER FORGING PACKAGE FOR 30MM BALL VS. 26MM BALL



15MM SEAL PACKAGE

HOLLOWMILL

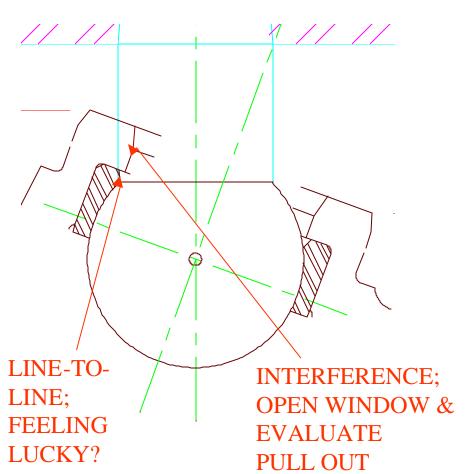
ARTICULATION STUDY 30MM VS 26MM BALL



TO AVOID PINCHING THE SEAL, WE'LL USE A 26MM BALL (BESIDES, IT'S CHEAPER)

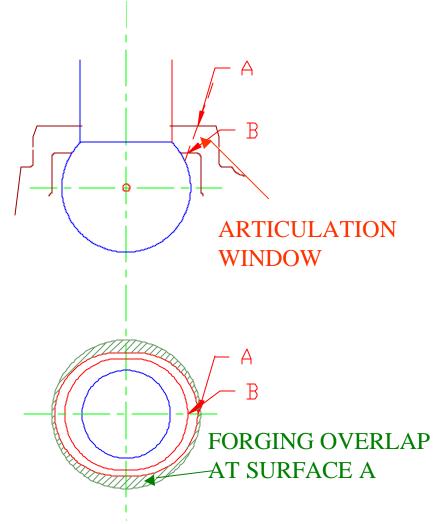
READDRESS ARTICULATION WITH 26MM BALL

- 2 ISSUES
 - SHANK-FORGING
 CRASH OPEN
 WINDOW
 - SHANK-BEARING
 LINE-TO-LINE @ 2
 DEGREE
 OVERTRAVEL LOW
 RISK
- COULD UNDERCUT STUD - ADDED \$\$\$



PULL OUT STRENGTH ANALYSIS

- **STUD ARTICULATED 20** • **DEGREES DEFINES WINDOW** SURFACE A-B
- FORGING OVERLAP = .199 SQ. IN
- PULL OUT FORCE = SIN(18DEG)*1.25*7000 LB =2704LB.
- RESISTING CROSS SECTION= .199 SQ. IN.
- PULL OUT STRESS = 2704 LB/.199 SQ IN = 13587 PSI
- MATERIAL YIELD >30000 PSI
- NO PROBLEM



ACCOMPLISHMENTS

- BALL STUD DESIGN COMPLETE
- SEAL REQUIREMENTS COMPLETE
- BEARING ARRANGEMENT 50%
- HOUSING 25%
- LUBRICATION 0%

BEARINGS AND LUBRICATION

- WE CHOSE A HARDENED STEEL **UPPER BEARING BECAUSE OF ROBUSTNESS.** THE APPLICATION (COMMERCIAL FLEET) PLACES A HIGH PRIORITY ON DURABILITY AND IS WILLING TO SACRIFICE SOME **ROTATING TORQUE**
- WE NOW NEED TO CHOSE A LOWER BEARING

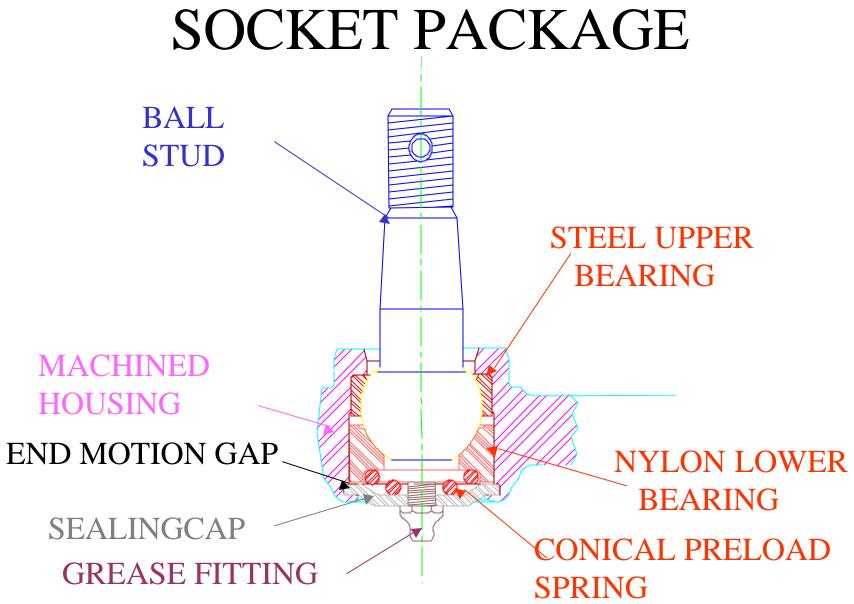
LOWER BEARING -STEEL OR PLASTIC?

- STEEL / POWDERED METAL
 BETTER WEAR

 - LESS COMPLIANCE

- NYLON
 - NOISE ISOLATION
 - LESS EXPENSIVE
 - MORE COMPLIANCE
 - LESS MASS
 - LOWER FRICTION

NYLON IS CHOSEN



GREASE SELECTION

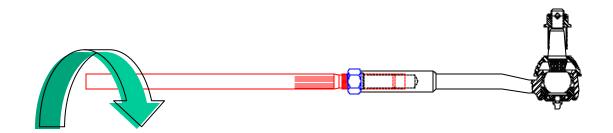
- LUBRICANT IS AN ESSENTIAL ELEMENT OF JOINT DESIGN
- GREASABLE VS. NON-GREASABLE
- TRIBOLOGY STUDIES
- COSTS

FINISHING THE MACHINED FORGING DESIGN

- INTERNAL/ EXTERNAL THREADS
- **STEM LENGTH**
- STEM ANGLE
- MATING FASTENERS
- "COBRA" SECTION
- INPUT REQUIREMENTS
 - LOADS 7000 MAX, 4000 WORKING
 - **STEM ANGLE 90 DEGREES @ CURB**
 - PACKAGE REQUIREMENTS STRAIGHT, 150MM LONG
 - APPEARANCE PROTECTION 240 HR SALT SPRAY
- **MATING PARTS DETAIL**
 - ROD / SLEEVE THREAD SIZE & LENGTH M16X1.5

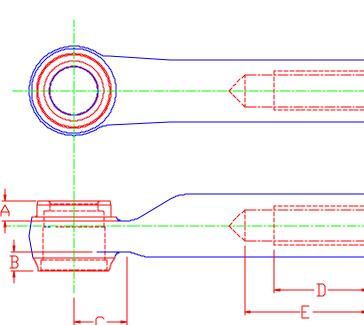
LENGTH ADJUSTMENT FOR TOE SET

- RACK AND PINION JAM NUT
- INNER END ROTATES
- 1.5MM/REV



DETAILING THE MACHINED FORGING

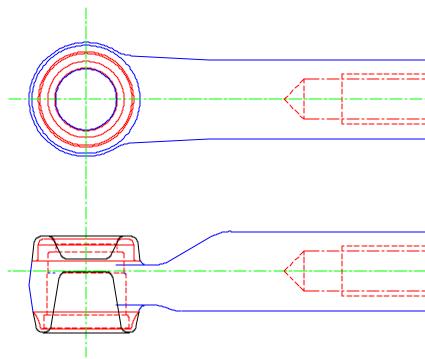
- STEM ANGLE & LENGTH ARE GIVEN
- COBRA THICKNESS & LENGTH DEFINED BY "A", "B" AND "C" TOOL RADIUS
- D=2.5*THD SIZE +TOE ADJUST
- E FOR PILOT HOLE + THREAD RUN OUT
- F= WASHER FACE OF MATING JAM NUT





FORGING DESIGN - ADDING WHAT WE WILL MACHINE AWAY

- FORGING TOLERANCES +/-.75MM
- DRAFT ANGLES **- 7-9 DEGREES**
- DIE SHIFT .75MM
- ANGULAR +/-2DEGREES
- E-COAT BEFORE MACHINING

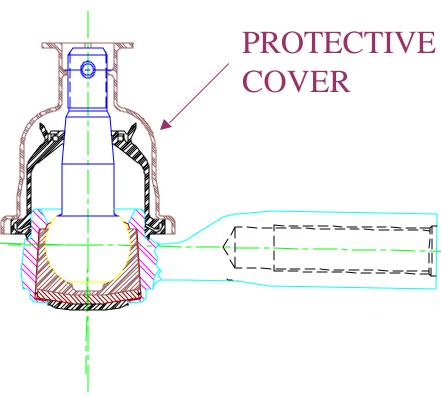


QUOTATION CHECKLIST

- FORGING
 - DRAWING COMPLETE RFQ ISSUED
- BALL STUD
 - DRAWING COMPLETE RFQ ISSUED
- SEAL
 - DRAWING COMPLETE RFQ ISSUED
- BEARINGS
 - DRAWING COMPLETE RFQ ISSUED
- MACHINING / ASSEMBLY
 TIME STUDIES COMPLETE
- PACKAGING
 - 2000 PIECE BULK NEED PROTECTIVE COVER

PACKAGING

- PROTECTIVE COVER
 - MUST NOT FALL **OFF IN TRANSIT**
 - MUST COME OFF EASILY AT ASSY PLANT
- COST OF EXPENDABLE SHIPPING CONTAINER



CONGRATULATE YOURSELF

- DESIGN IS DONE
- PART IS QUOTED
- READY TO START PROTOTYPES