

$$\varepsilon_0 := 8.854 \cdot 10^{-12} \quad \mu_0 := 4 \cdot \pi \cdot 10^{-7} \quad \text{c} := \frac{1}{\sqrt{\varepsilon_0 \cdot \mu_0}} \quad \eta_0 := \sqrt{\frac{\mu_0}{\varepsilon_0}} \quad \text{fundamental constants}$$

$$j := \sqrt{-1} \quad \epsilon_r := 2.05 \quad \tan\delta := 2 \cdot 10^{-4} \quad \text{dielectric properties of PTFE spacer}$$

$$a := 0.8 \cdot 10^{-3} \quad b := 2.65 \cdot 10^{-3} \quad \text{inner and outer diameters of RG402/U (note 0.255 mm and 0.84 mm, respectively, for RG405/U)}$$

$$K := 2\pi \cdot 10^3 \quad M := 2\pi \cdot 10^6 \quad G := 2 \cdot \pi \cdot 10^9 \quad \text{frequency multiplication and conversion}$$

$$Z := 10^{-9}$$

$$\rho_a := 1.59 \cdot 10^{-8} \quad \rho_b := 1.69 \cdot 10^{-8} \quad \begin{aligned} &\text{resistivities of conductors (inner silver, outer copper);} \\ &\text{values are those of pure metals at 293 K} \end{aligned}$$

$$R_{sa}(f) := \sqrt{\frac{1}{2} \cdot \mu_0 \cdot \rho_a \cdot f \cdot M} \quad R_{sb}(f) := \sqrt{\frac{1}{2} \cdot \mu_0 \cdot \rho_b \cdot f \cdot M} \quad \text{surface resistance of inner and outer conductors}$$

Note: in what follows, frequency has units of MHz (i.e. multiplier M has been chosen)

$$Z_0 := \frac{\eta_0}{2 \cdot \pi \cdot \sqrt{\epsilon_r}} \cdot \ln\left(\frac{b}{a}\right) \quad Z_0 = 50.157 \quad \text{characteristic impedance when lossless}$$

$$R(f) := \frac{1}{2 \cdot \pi} \cdot \left(\frac{R_{sa}(f)}{a} + \frac{R_{sb}(f)}{b} \right) \quad \text{resistance per unit length}$$

$$\alpha_c(f) := \frac{R(f)}{2 \cdot Z_0} \quad \beta(f) := \frac{M \cdot f \cdot \sqrt{\epsilon_r}}{c} \quad \alpha_d(f) := \frac{1}{2} \cdot \beta(f) \cdot \tan\delta \quad \begin{aligned} &\text{conductor and dielectric} \\ &\text{attenuation constants;} \\ &\text{wavenumber in PTFE} \end{aligned}$$

$$\alpha(f) := \alpha_c(f) + \alpha_d(f) \quad \gamma(f) := \alpha(f) + j \cdot \beta(f) \quad \begin{aligned} &\text{total attenuation constant and} \\ &\text{propagation constant} \end{aligned}$$

$$L := 83.8 \cdot 10^{-3} \quad \text{length of coaxial probe}$$

$$n := 1, 2..6$$

$$f_0 := \frac{c \cdot 10^{-6}}{2 \cdot L \cdot \sqrt{\epsilon_r}} \quad f_0 = 1.249 \times 10^3 \quad \text{Fundamental resonant frequency based on actual length}$$

$$g1 := 1.1467$$

$$g2 := 1.1467$$

$$Q_o(n) := \frac{n \cdot \pi \cdot g1}{2 \cdot 0.0549^2}$$

$$\begin{array}{lll} Qo(1) = 597.62 & Qo(2) = 1.195 \times 10^3 & Qo(5) = 2.988 \times 10^3 \\ Qo(3) = 1.793 \times 10^3 & Qo(4) = 2.39 \times 10^3 & Qo(6) = 3.586 \times 10^3 \end{array}$$

Unloaded
quality factor
of each mode

$$F_0(f) := \frac{(f - f_0) \cdot Qo(1)}{f_0}$$

$$S_{21_0}(f) := \frac{2 \cdot \sqrt{g_1 \cdot g_2}}{1 + g_1 + g_2 + j \cdot 2 \cdot F_0(f)}$$

$$P_0(f) := (|S_{21_0}(f)|)^2 \quad P_0(5000) = \blacksquare \quad \text{power absorption coefficients}$$

The following graphs show reflected power as a function of permittivity of sample. The final graphs show the curve fitting used to obtain resonator parameters.

$$f := 1000, 1001..8500 \quad \varepsilon := 80 - 20 \cdot j$$

