

Company		Project #	
Project		Sheet Number	
Subject		Total Sheets	
Name		Date	
Checked by		Check Date	

LOADING CONDITIONS Note: Calculations are per ACI 318-05 Appendix D. N_u and V_u were factored using factors from ACI 318-05? Factored tensile load (kips) = N_u = 116.865 Factored shear load (kips) = V_u = 10.5 Is there a built-up grout pad? <input checked="" type="checkbox"/> Yes		Section 9.2 used 1.5 load factor perpendicular to edge 10.5	
ANCHOR DATA, EMBEDMENT, AND THICKNESS OF MEMBER Anchor material type = A307-Type C, F_u = 58 Nominal anchor diameter (in.) = 2 1/2 Effective anchor embedment depth (in.) = h_{ef} = 46.00 = h Thickness of member in which anchor is anchored, (in.) = h = 51.00 = h Number of anchors in tension = $n(tension)$ = 1 Number of anchors in shear = $n(shear)$ = 2		Adequate supplementary reinf. provided to resist tension loads in anchors? <input checked="" type="checkbox"/> No Adequate reinforcement provided to resist shear loads in anchors? <input checked="" type="checkbox"/> No	
CONCRETE FAILURE AREAS Do you want to manually input the value of A_n ? <input checked="" type="checkbox"/> No Note: Units for A_n and A_v are sq. in. A_n = 2497.21605 Do you want to manually input the value of A_v ? <input checked="" type="checkbox"/> No A_v = 1631.28905		Cracking modification factor, γ_f = 1.4 - Located in region where there isn't cracking at service loads (ft < fr)	

DESIGN CONSIDERATIONS Ductility required? <input checked="" type="checkbox"/> No <input checked="" type="checkbox"/> Shear Intermediate or high seismic risk? <input checked="" type="checkbox"/> No <input checked="" type="checkbox"/> Yes Specified concrete strength (psi) = f_c = 5000 Cracking modification factor, γ_f = 1.4 - Located in region where there isn't cracking at service loads (ft < fr)		Eccentricity of tensile force on group of tensile anchors (in.) e_{t1} = 0 (0=single anchor) Eccentricity of shear force on group of anchors (in.) (Note e_t must be less than s perpendicular to shear) e_{v1} = 0	
EDGE DISTANCES AND SPACING Edge Distance, in. c_1 = 14.71 c_3 = 69.00 c_4 = 14.9 c_2 = 14.9 c_4 = 14.9 c_1 = minimum edge distance c_2 = least edge distance perpendicular to c_1		SHEAR Edge Distance, in. c_1 = 14.71 c_2 = 29.8 c_4 = 29.8 c_1 = edge distance in direction of V_n (perp.) c_2 = least edge distance perpendicular to c_1	

INTERACTION OF TENSILE AND SHEAR FORCES ϕN_n = 130.1 kips \geq N_u = 116.9 kips ϕV_n = 92.2 kips \geq V_u = 10.5 kips $N_u/(\phi N_n) + V_u/(\phi V_n) = 0.90 + 0.11 = 1.01 \leq 1.2$		RESULTS ANCHOR OK! 130.10	
DUCTILITY Tensile load - service (N) = 77.91 kip Factored Tensile load (N_u) = 116.865 kip Shear - service (V_s) = 7 kip Factored Shear = 10.5 kip Tension $C1 = 0.5(W \cdot BCD)^{1/2} = 14.71$ in $C2 = C4 = (P)^{1/2} \cdot BCD/n = 29.83$ in		ANCHORS HAVE ONLY ONE CONC EDGE Min Embedment length = (12d) in Min Embedment length = (Sleeve+6d) in	

Conservatively use half the distance		Shear PIP Appendix-page A-6 $C1 = 1.03W/2 \cdot BCD/2 = 19.70$ in $C2 = C4 = [(1.03W/2)^2 \cdot (BCD/2)^2]^{1/2} = 79.83$ Very conservative use	
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SUBJECT: VESSEL No 38-T-201
Anchor Rod design

BY: Chandra Date: 03/06/08
Chk By: _____ Date: _____

Define Units kipft := kip·ft

A) Concrete Pedestal Size

Diameter (BCD) - D $D := 25.313\text{ft}$ Pile = 18in Dia Auger -CIP
Anchor Bolt dia = d $d := 2.75\text{in}$ Flour Dwg: 6"x24" sleeve
Bolt Sleeve Dia = ds $ds := 6\text{in}$
Bolt Sleeve Length = Ls $Ls := 24\text{in}$

Face to Face Pedestal = (FF)

$$\begin{aligned}\underline{FF1} &:= \underline{D} + 8\text{in} & \underline{FF1} &= 25.98\text{ft} \\ \underline{FF2} &:= \underline{D} + 8\cdot\underline{d} & \underline{FF2} &= 27.146\text{ft} \quad (\text{ASTM 307 Type C Anchor Rod}) \\ \underline{FF3} &:= \underline{D} + \underline{ds} + 6\text{in} & \underline{FF3} &= 26.313\text{ft} \\ \underline{FF} &:= \max(\underline{FF1}, \underline{FF2}, \underline{FF3}) & \underline{FF} &= 27.146\text{ft}\end{aligned}$$

Use Min Face to Face Pedestal Size of 27.5 feet min

B) Determine Max Tension on Anchor Rod

2-3/4 in Anchor Rod - ASTM A 307 Grade C - Galvanized/ with Sleeve (6x24)"

Moment of Intertia of Anchor Bolts

No of Anchor Bolts $n := 32$ $I := \frac{n \cdot D^2}{8}$ $I = 2.56 \times 10^3 \cdot \text{ft}^2$

Allowable loads

$$\begin{aligned}\underline{F_y} &:= 36\text{ksi} & \underline{F_u} &:= 60\text{ksi} & \underline{F_v} &:= 0.17 \cdot \underline{F_u} & \underline{F_v} &= 10.2\text{ksi} & \underline{A1} &:= \frac{\pi \cdot d^2}{4} \\ \underline{F_t} &:= 0.33 \underline{F_u} & \underline{F_t} &= 19.8\text{ksi}\end{aligned}$$

Area of Bolt = A1

$$\underline{A1} = 5.94 \cdot \text{in}^2 \quad \text{Use } \underline{F_t} = 15\text{ksi} \quad \text{Conservative}$$

$\underline{F_{tallow}} := \underline{F_t} \cdot \underline{A1}$

$$\underline{F_{tallow}} = 89.094 \cdot \text{kip}$$

$\underline{F_{vallow}} := 0.17 \cdot \underline{F_u} \cdot \underline{A1}$

$$\underline{F_{vallow}} = 60.584 \cdot \text{kip}$$

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Erection Case

Erection wt - Vertical load- Per

$$\underline{Per} := 1054 \text{kip}$$

Erection wt

Erection Moment - Me

$$\underline{Me} := 22448 \text{kipft}$$

Use Seismic Base Moment

Moment arm = Xm

$$\underline{Xm} := \frac{D}{2}$$

$$\underline{Xm} = 12.656 \cdot \text{ft}$$

$$\underline{Ftmax1} := \frac{\underline{Per}}{n} + \frac{\underline{Me} \cdot \underline{Xm}}{I}$$

$$\underline{Ftmax1} = 143.79 \cdot \text{kip} \quad (\text{Compression})$$

$$\underline{Ftmin1} := \frac{\underline{Per}}{n} - \frac{\underline{Me} \cdot \underline{Xm}}{I}$$

$$\underline{Ftmin1} = -77.915 \cdot \text{kip} \quad (\text{Tension})$$

Erection Shear - Fes

$$\underline{Fes} := 183 \text{kip}$$

Seismic shear

$$\underline{Fvmax} := \frac{\underline{Fes}}{n}$$

$$\underline{Fvmax} = 5.719 \cdot \text{kip}$$

$$\underline{IR} := \frac{-\underline{Ftmin1}}{\underline{Ftallow}} + \frac{\underline{Fvmax}}{\underline{Fvallow}}$$

$$\underline{IR} = 0.969$$

Operating Case

Operating wt - Vertical load - Pop

$$\underline{Pop} := 2194 \text{kip}$$

Operating wt

Operating Moment Mo

$$\underline{Mo} := 26967 \text{kipft}$$

Use Seismic moment

$$\underline{Ftmax2} := \frac{\underline{Pop}}{n} + \frac{\underline{Mo} \cdot \underline{Xm}}{I}$$

$$\underline{Ftmax2} = 201.73 \cdot \text{kip} \quad (\text{Compression})$$

$$\underline{Ftmin2} := \frac{\underline{Pop}}{n} - \frac{\underline{Mo} \cdot \underline{Xm}}{I}$$

$$\underline{Ftmin2} = -64.605 \cdot \text{kip} \quad (\text{Tension})$$

Operating Shear - Fos

$$\underline{Fos} := 226 \text{kip}$$

Seismic shear

$$\underline{Fvmax} := \frac{\underline{Fos}}{n}$$

$$\underline{Fvmax} = 7.063 \cdot \text{kip} \quad (\text{Lateral})$$

$$\underline{IR} := \frac{-\underline{Ftmin2}}{\underline{Ftallow}} + \frac{\underline{Fvmax}}{\underline{Fvallow}}$$

$$\underline{IR} = 0.842$$

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C) Anchor Rod Design: Embedment length

Reference PIP STE05121 /2003

ACI 318 /05 Appendix D

Wind Loads and Anchor Bolt Design for Petro Chemical Facilities - ASCE Task Committee
 on wind induced forces & task committee on Anchor bolt Design

Design Criteria:

Min Embedment length d_o = Anchor rod dia d_s = Sleeve dia L_s = Sleeve length
 $\underline{d_o} := \underline{d}$ $\underline{d} = 2.75 \cdot \underline{in}$ $\underline{d_s} := 6 \underline{in}$ $\underline{L_s} = 24 \cdot \underline{in}$

a) $L_1 = 12 \cdot d_o$ $\underline{L_1} := 12 \cdot \underline{d}$ $\underline{L_1} = 33 \cdot \underline{in}$
 b) $L_2 = L_s + 6d_o$ $\underline{L_2} := \underline{L_s} + 6 \cdot \underline{d_o}$ $\underline{L_2} = 40.5 \cdot \underline{in}$

Min Edge distance

a) $4d_o$
 b) $4d_o + 0.5(d_s - d_o)$

Min Bolt spacing

a) $8d_o$

Check Transfer of Tension Force - From Anchor Rod to Pedestal Rebar

Max Tension T_{max} (use load factor of 1.5)

$$\underline{T_{max}} := (1.5) \cdot -\min(\underline{F_{tmin1}}, \underline{F_{tmin2}})$$

$$\underline{T_{max}} = 116.872 \cdot \underline{kip}$$

Rebar yield = f_y

$$\underline{f_y} := 60 \underline{ksi}$$

Area of rebar required to sufficient to transfer the tension = A_{st}

$$\underline{A_{st}} := \frac{\underline{T_{max}}}{(0.9 \cdot \underline{f_y})}$$

$$\underline{A_{st}} = 2.164 \cdot \underline{in}^2$$

Select

Nos Bar required

Use

#9: $\underline{dp9} := 1.128 \underline{in}$ $\underline{Ap9} := \left(\frac{22}{7} \right) \cdot \frac{(\underline{dp9})^2}{4}$ $\underline{Ap9} = 1 \cdot \underline{in}^2$ $\underline{n9} := \frac{\underline{A_{st}}}{\underline{Ap9}}$ $\underline{n9} = 2.165$ $\underline{n9} := 3$

#8: $\underline{dp8} := 1.0 \underline{in}$ $\underline{Ap8} := \left(\frac{22}{7} \right) \cdot \frac{(\underline{dp8})^2}{4}$ $\underline{Ap8} = 0.786 \cdot \underline{in}^2$ $\underline{n8} := \frac{\underline{A_{st}}}{\underline{Ap8}}$ $\underline{n8} = 2.755$ $\underline{n8} := 3$

#7: $\underline{dp7} := 0.875 \underline{in}$ $\underline{Ap7} := \left(\frac{22}{7} \right) \cdot \frac{(\underline{dp7})^2}{4}$ $\underline{Ap7} = 0.602 \cdot \underline{in}^2$ $\underline{n7} := \frac{\underline{A_{st}}}{\underline{Ap7}}$ $\underline{n7} = 3.598$ $\underline{n7} := 4$

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Select smaller dia bars with smaller development lengths for vertical reinforcement in the pedestal. USE # 7 bars

USE 4 # 7 bars to transfer the tension in the Anchor into the pedestal

Note

- 1) The # 7 bars must be developed within the pedestal - See cad sketch - OK

From Cad sketch Use 4.25 ft Pedestal With # 7 Rebar for vertical reinforcement

Min Embedment length of Anchor = L_{e1}

$$L_{e1} := 3.84 \text{ ft} \quad L_{e1} = 46.08 \text{ in}$$

Min embedment L_e

$$L_e := \max(L_1, L_2, L_{e1}) \quad L_e = 46.08 \text{ in}$$

- 2) Check Anchor rod embedment length Per ACI 318- Appendix D -See Spread Sheet - OK

Use Min required embedment length from cad sketch (L_{e1}) and check for compliance with Appendix D OK

- 3) Total Length of Anchor Rod

Anchor Rod Total Length = L $L = \text{Projection}(p) + \text{Embedment}(L_m) + \text{bottom plate}(l_m)$

Projection = $p = \text{Grout}(1") + \text{Skirt ht}(H_s) + (2 \times \text{nuts}) + 1"$

Grout thk = Gr $Gr := 1 \text{ in}$

Skirt ht H_s $H_s := 20.25 \text{ in}$

Nut thk = nt $nt := d$

$$p := (Gr + H_s + 2 \cdot d + 1 \text{ in}) \quad d = 2.75 \text{ in}$$

$$p = 27.75 \text{ in}$$

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Bottom length $L_b = \text{nut} + 1"$

$$\underline{L_b} := d + 1 \text{ in}$$

$$\underline{L_b} = 3.75 \text{ in}$$

Anchor rod Total length - L_b

$$\underline{L_{bolt}} := p + \underline{L_e} + \underline{L_b}$$

$$\underline{L_{bolt}} = 77.58 \text{ in}$$

USE

$$\underline{p} := 28 \text{ in}$$

$$\underline{L_e} := 46 \text{ in}$$

$$\underline{L_b} := 4.0 \text{ in}$$

$$\underline{L_{bolt}} := p + \underline{L_e} + \underline{L_b}$$

$$\underline{L_{bolt}} = 78 \text{ in}$$

USE 6'-6" = 78" ANCHOR ROD