

FIGURE 7-23
Schematic for Example 7-5.

## TABLE 7-1

Empirical correlations for the average Nusselt number for forced convection over circular and noncircular cylinders in cross flow (from Zukauskas, Ref. 14, and Jakob, Ref. 6)

| Cross-section <br> of the cylinder | Fluid | Range of Re | Nusselt number |
| :--- | :--- | :--- | :--- |
| Circle | $0.4-4$ <br> $4-40$ | $\mathrm{Nu}=0.989 \mathrm{Re}^{0.330} \mathrm{Pr}^{1 / 3}$ <br> $\mathrm{Nu}=0.911 \mathrm{Re}^{0.385} \mathrm{Pr}^{1 / 3}$ <br> $\mathrm{Nu}=0.683 \mathrm{Re}^{0.466} \mathrm{Pr}^{1 / 3}$ |  |
| $\mathrm{Nu}=0.193 \mathrm{Re}^{0.618} \mathrm{Pr}^{1 / 3}$ |  |  |  |
| $\mathrm{Nu}=0.027 \mathrm{Re}^{0.805} \mathrm{Pr}^{1 / 3}$ |  |  |  |

## EXAMPLE 7-5 Heat Loss from a Steam Pipe in Windy Air

A long $10-\mathrm{cm}$-diameter steam pipe whose external surface temperature is $110^{\circ} \mathrm{C}$ passes through some open area that is not protected against the winds (Fig. 7-23). Determine the rate of heat loss from the pipe per unit of its length
when the air is at 1 atm pressure and $10^{\circ} \mathrm{C}$ and the wind is blowing across the pipe at a velocity of $8 \mathrm{~m} / \mathrm{s}$.

SOLUTION A steam pipe is exposed to windy air. The rate of heat loss from the steam is to be determined.
Assumptions 1 Steady operating conditions exist. 2 Radiation effects are negligible. 3 Air is an ideal gas.
Properties The properties of air at the average film temperature of $T_{f}=$ $\left(T_{s}+T_{\infty}\right) / 2=(110+10) / 2=60^{\circ} \mathrm{C}$ and 1 atm pressure are (Table A-15)

$$
\begin{array}{ll}
k=0.02808 \mathrm{~W} / \mathrm{m} \cdot{ }^{\circ} \mathrm{C} & \operatorname{Pr}=0.7202 \\
v=1.896 \times 10^{-5} \mathrm{~m}^{2} / \mathrm{s} &
\end{array}
$$

Analysis The Reynolds number is

$$
\operatorname{Re}=\frac{\mathscr{V} D}{v}=\frac{(8 \mathrm{~m} / \mathrm{s})(0.1 \mathrm{~m})}{1.896 \times 10^{-5} \mathrm{~m}^{2} / \mathrm{s}}=4.219 \times 10^{4}
$$

The Nusselt number can be determined from

$$
\begin{aligned}
\mathrm{Nu} & =\frac{h D}{k}=0.3+\frac{0.62 \mathrm{Re}^{1 / 2} \mathrm{Pr}^{1 / 3}}{\left[1+(0.4 / \operatorname{Pr})^{2 / 3}\right]^{1 / 4}}\left[1+\left(\frac{\mathrm{Re}}{282,000}\right)^{5 / 8}\right]^{4 / 5} \\
& =0.3+\frac{0.62\left(4.219 \times 10^{4}\right)^{1 / 2}(0.7202)^{1 / 3}}{\left[1+(0.4 / 0.7202)^{2 / 3}\right]^{1 / 4}}\left[1+\left(\frac{4.219 \times 10^{4}}{282,000}\right)^{5 / 8}\right]^{4 / 5} \\
& =124
\end{aligned}
$$

and

$$
h=\frac{k}{D} \mathrm{Nu}=\frac{0.02808 \mathrm{~W} / \mathrm{m} \cdot{ }^{\circ} \mathrm{C}}{0.1 \mathrm{~m}}(124)=34.8 \mathrm{~W} / \mathrm{m}^{2} \cdot{ }^{\circ} \mathrm{C}
$$

Then the rate of heat transfer from the pipe per unit of its length becomes

$$
\begin{aligned}
A_{s} & =p L=\pi D L=\pi(0.1 \mathrm{~m})(1 \mathrm{~m})=0.314 \mathrm{~m}^{2} \\
\dot{Q} & =h A_{s}\left(T_{s}-T_{\infty}\right)=\left(34.8 \mathrm{~W} / \mathrm{m}^{2} \cdot \mathrm{C}\right)\left(0.314 \mathrm{~m}^{2}\right)(110-10)^{\circ} \mathrm{C}=1093 \mathbf{W}
\end{aligned}
$$

The rate of heat loss from the entire pipe can be obtained by multiplying the value above by the length of the pipe in $m$.
Discussion The simpler Nusselt number relation in Table 7-1 in this case would give $\mathrm{Nu}=128$, which is 3 percent higher than the value obtained above using Eq. 7-35.

## EXAMPLE 7-6 Cooling of a Steel Ball by Forced Air

A 25 -cm-diameter stainless steel ball ( $\rho=8055 \mathrm{~kg} / \mathrm{m}^{3}, C_{p}=480 \mathrm{~J} / \mathrm{kg} \cdot{ }^{\circ} \mathrm{C}$ ) is removed from the oven at a uniform temperature of $300^{\circ} \mathrm{C}$ (Fig. 7-24). The ball is then subjected to the flow of air at 1 atm pressure and $25^{\circ} \mathrm{C}$ with a velocity of $3 \mathrm{~m} / \mathrm{s}$. The surface temperature of the ball eventually drops to $200^{\circ} \mathrm{C}$. Determine the average convection heat transfer coefficient during this cooling process and estimate how long the process will take.


FIGURE 7-24
Schematic for Example 7-6.

