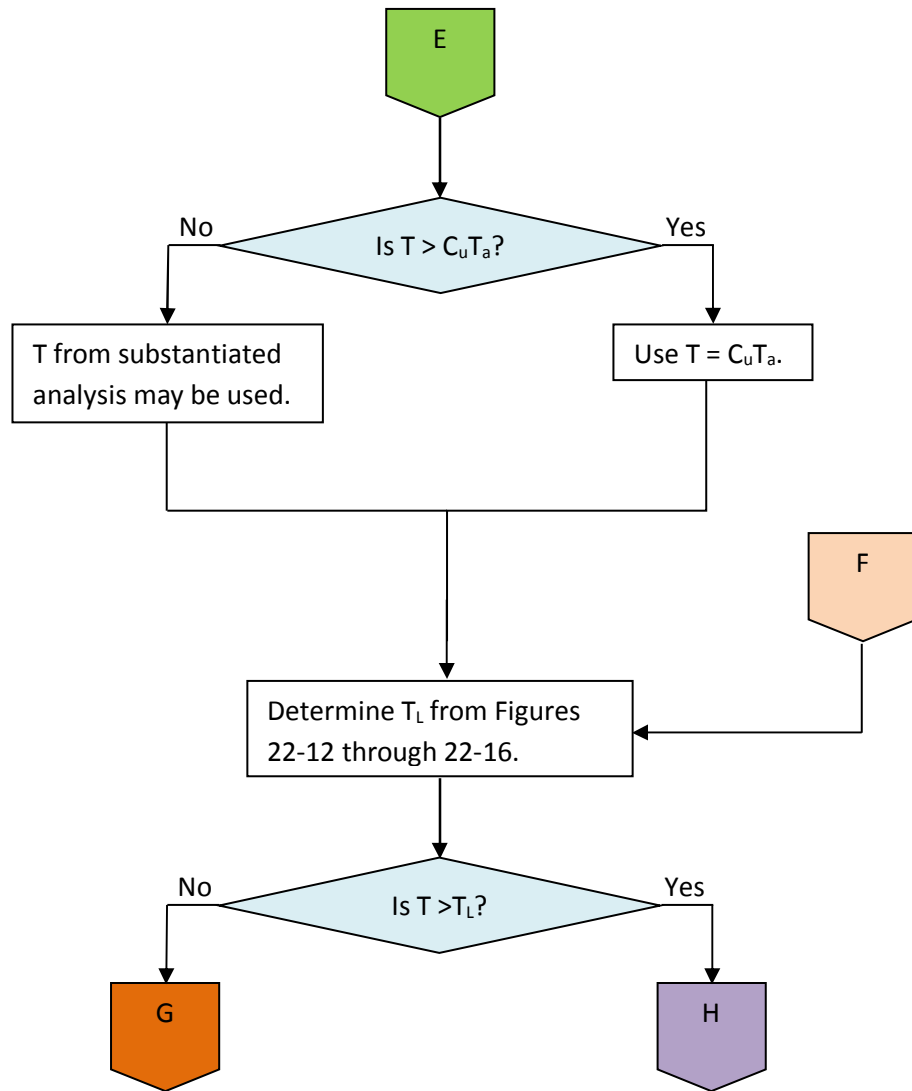
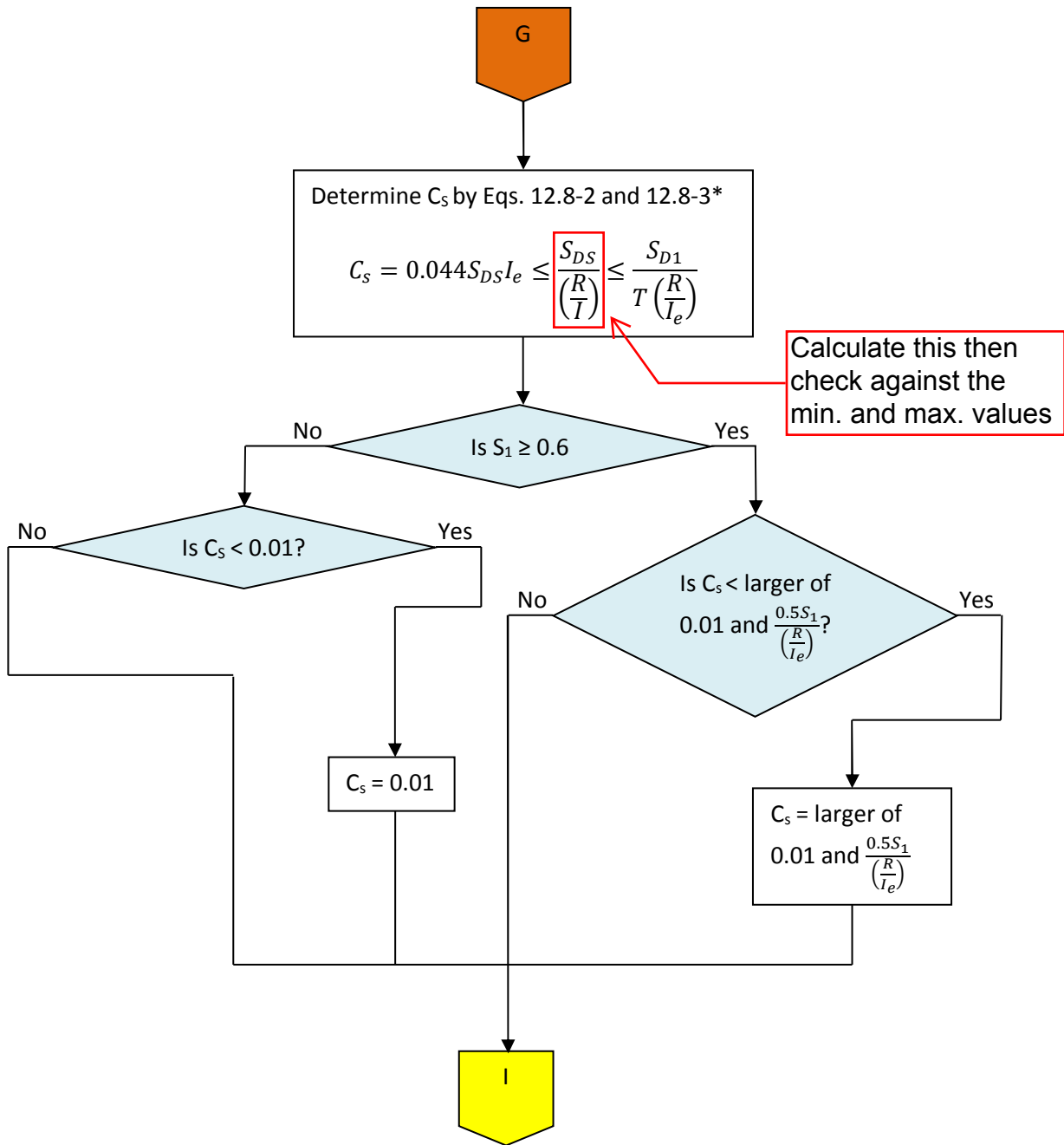
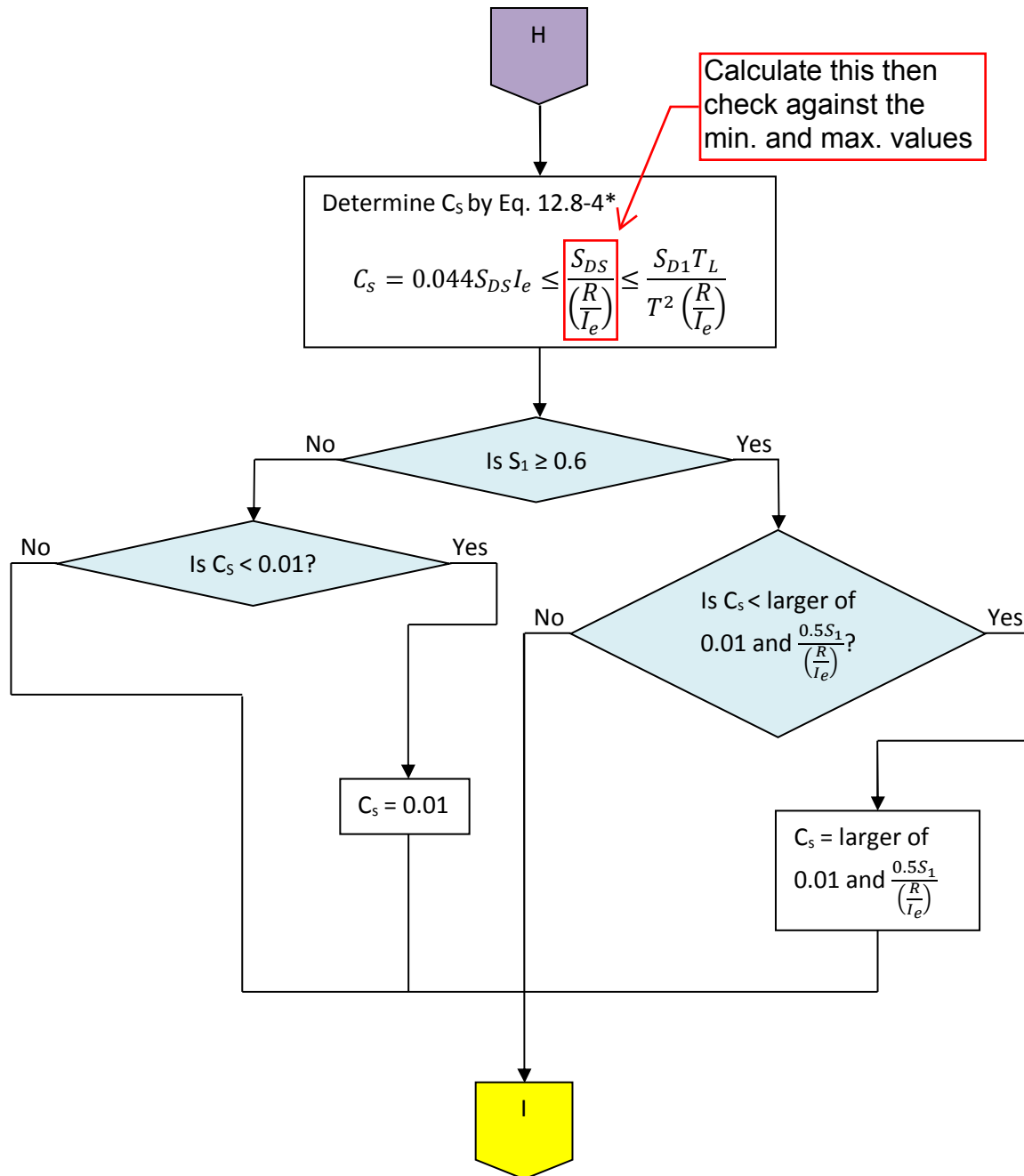


*Alternative methods for T_a are given in 12.8.2.1 for concrete and steel moment resisting frames and masonry or concrete shear wall structures.

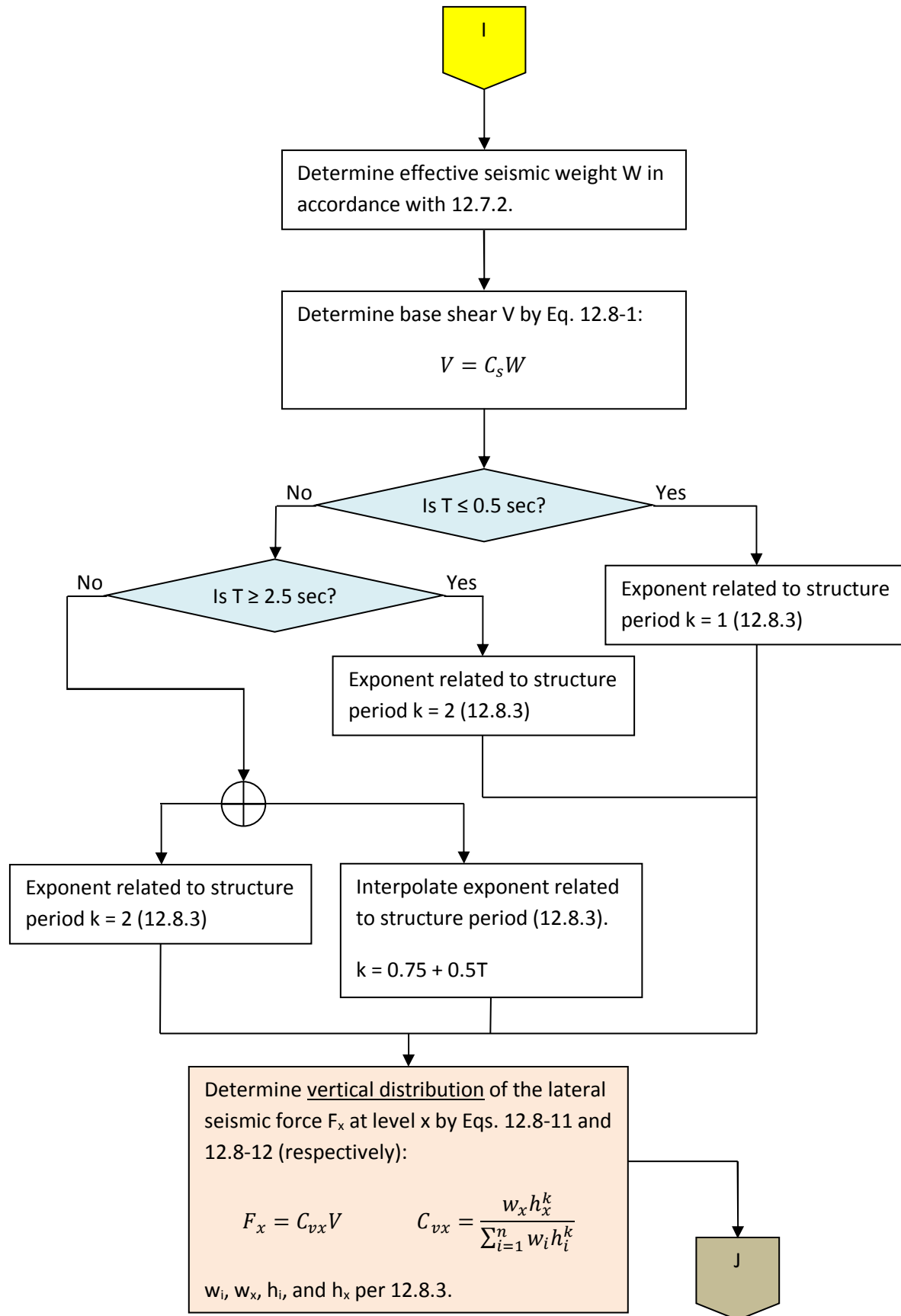




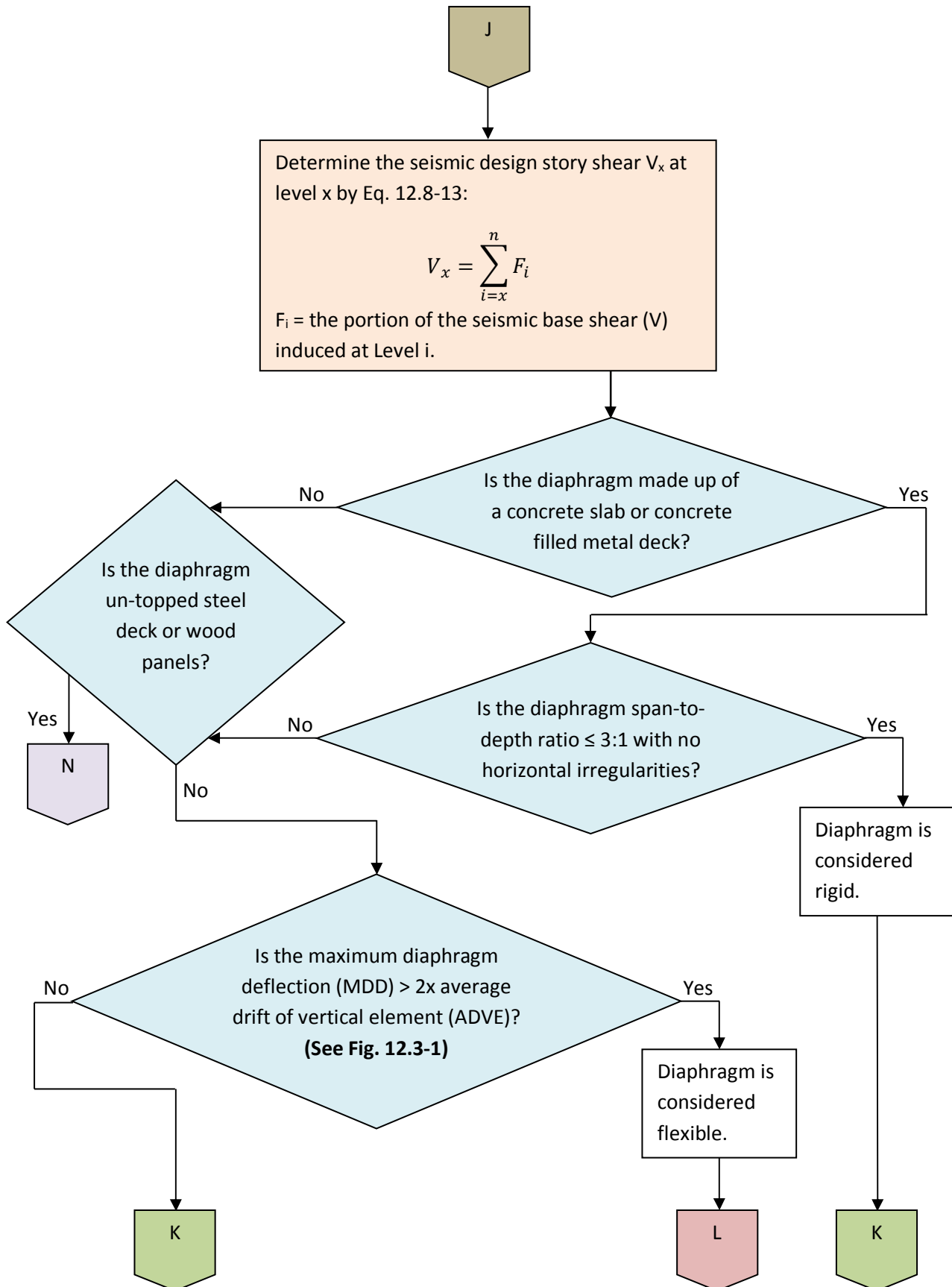
*For regular structures five stories or less above the base (see section 11.2) and having a period $T \leq 0.5$ sec, C_s is permitted to be calculated using a value of 1.5 for S_s (12.8.1.3).



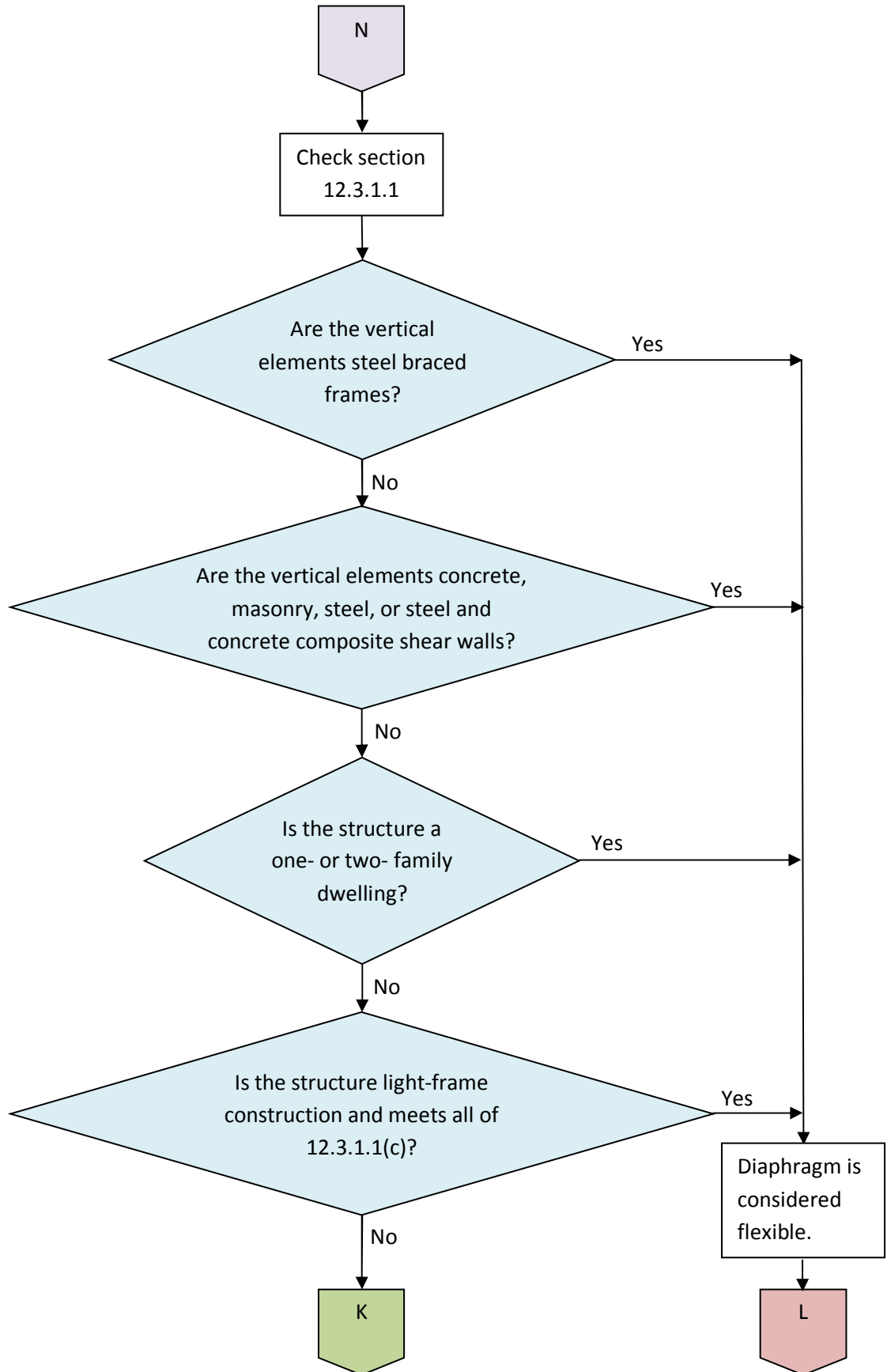
*For regular structures five stories or less above the base (see section 11.2) and having a period $T \leq 0.5$ sec, C_s is permitted to be calculated using a value of 1.5 for S_5 (12.8.1.3).



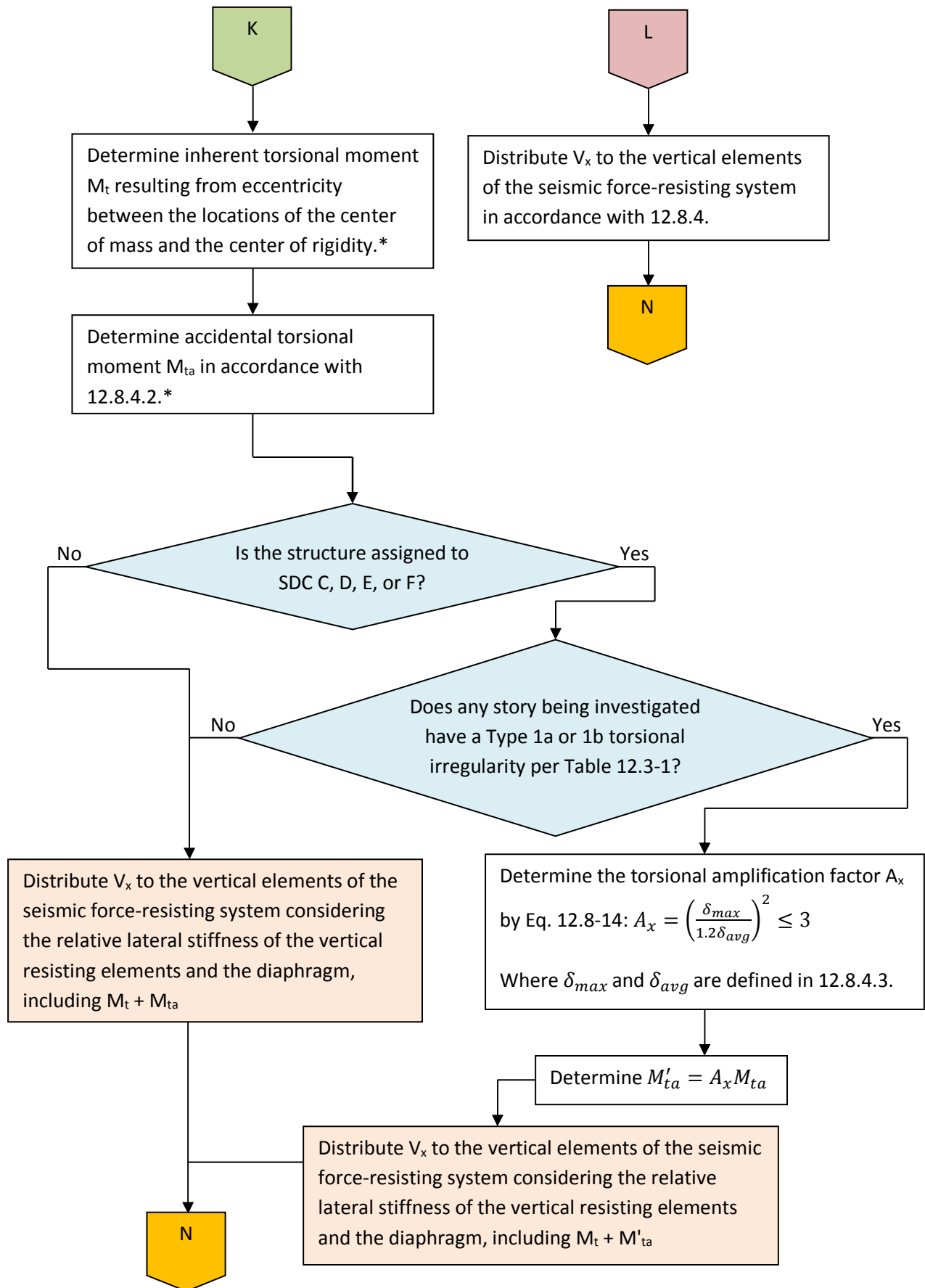
*See SEAOC 2012 IBC Structural/Seismic Design Manual, Vol. 1 (or other similar reference).



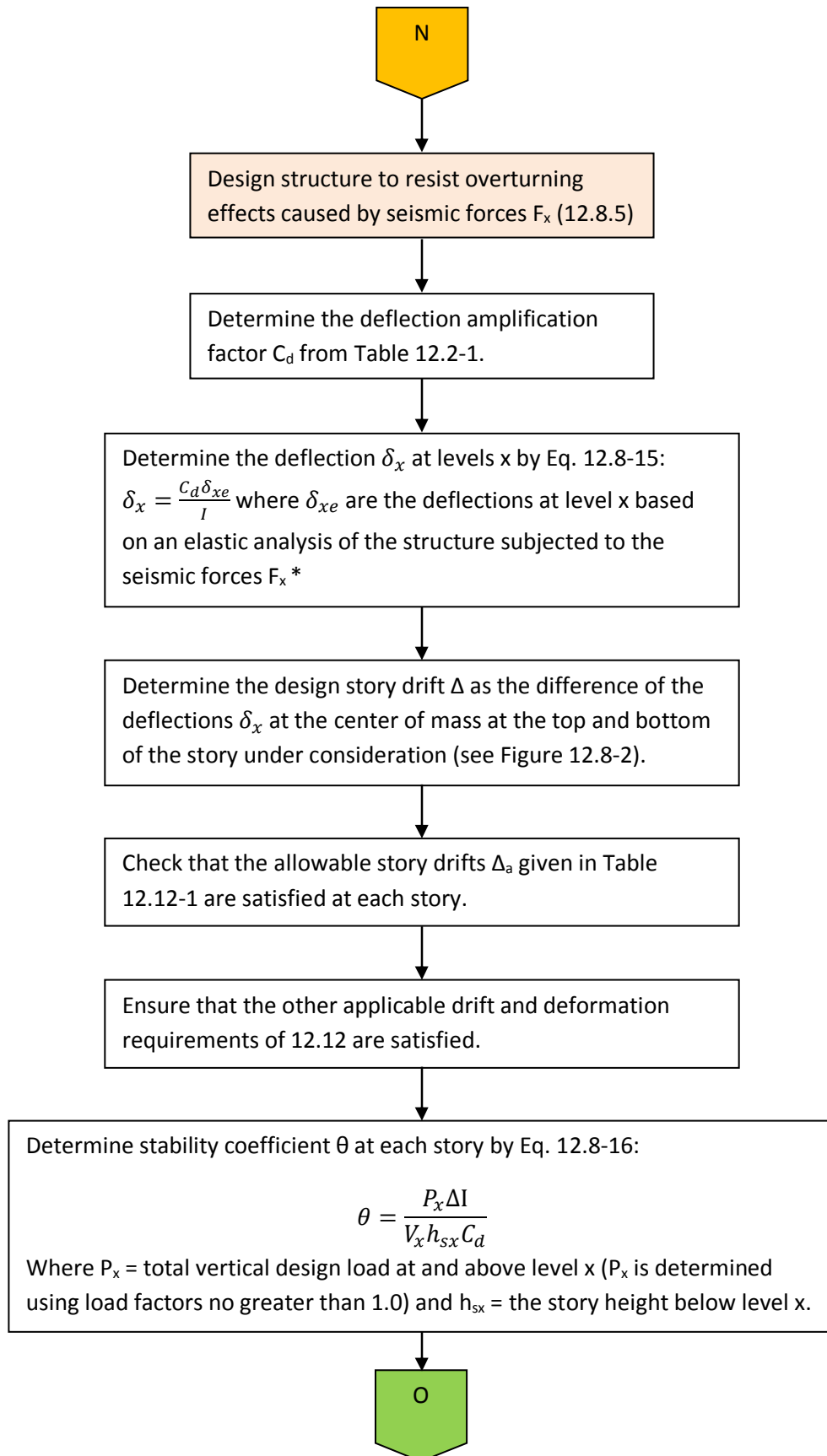
*See SEAOC 2012 IBC Structural/Seismic Design Manual, Vol. 1 (or other similar reference).



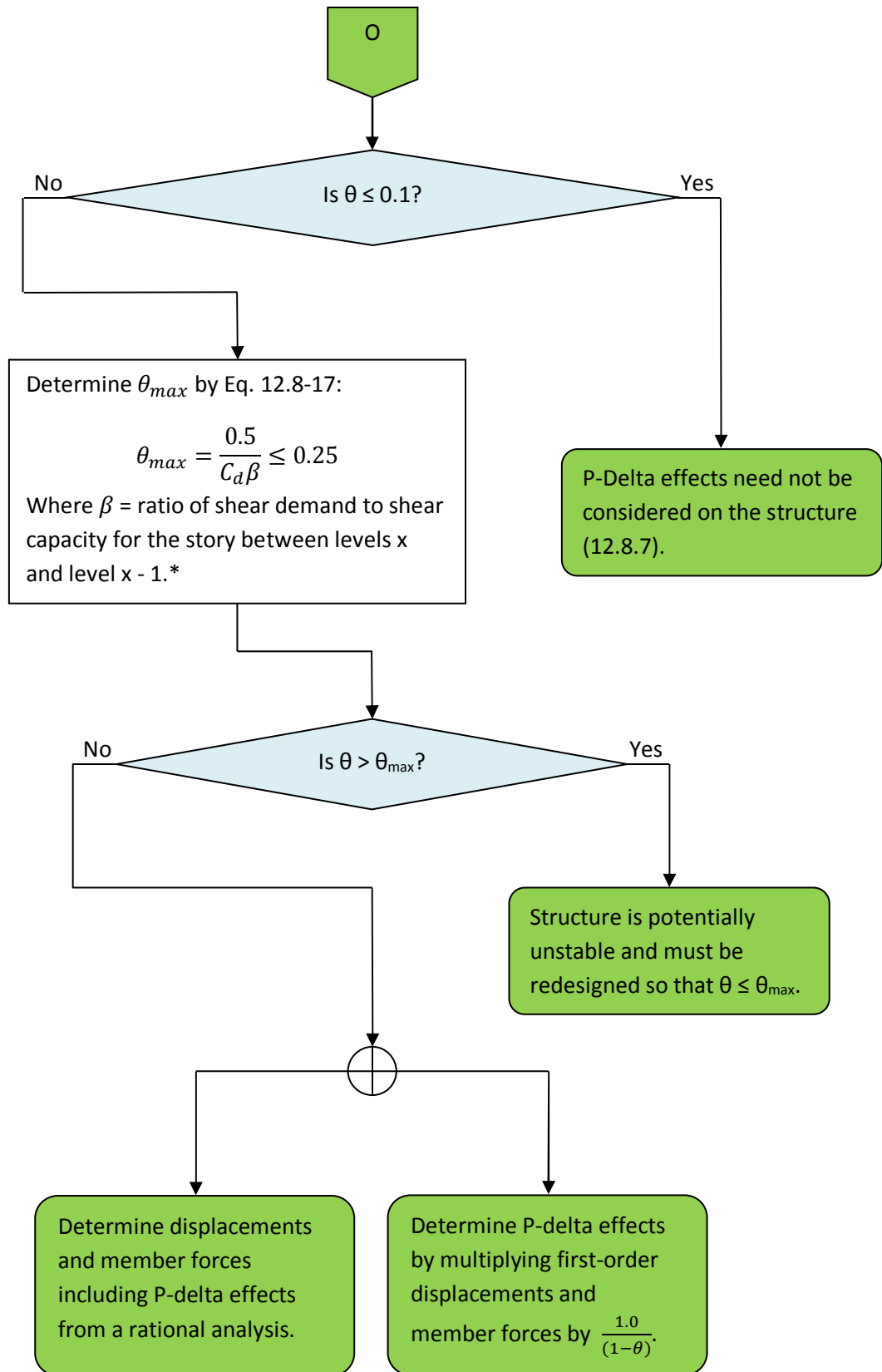
*See SEAOC 2012 IBC Structural/Seismic Design Manual, Vol. 1 (or other similar reference).



*See SEAOC 2012 IBC Structural/Seismic Design Manual, Vol. 1 (or other similar reference).



*It is permitted to determine δ_{xe} using seismic design forces based on the computed fundamental period of the structure without the upper limit $C_u T_a$ specified in 12.8.2 (12.8.6.2).



* β can conservatively be taken as 1.0. Where P-delta effects are included in an automated analysis, the value of θ computed by Eq. 12.8-16 is permitted to be divided by $(1 - \theta)$ before checking Eq. 12.8-17 (12.8.7)