

# NorthWoods Software

**Program Name:** Load Combinations

**Project Name:** Name

**Project Number:** Number

**Project Description:** Describe

**Project Designer:** Dik

**Last Revised (yy-mm-dd):** 18-07-27

**Reference:** Reference?

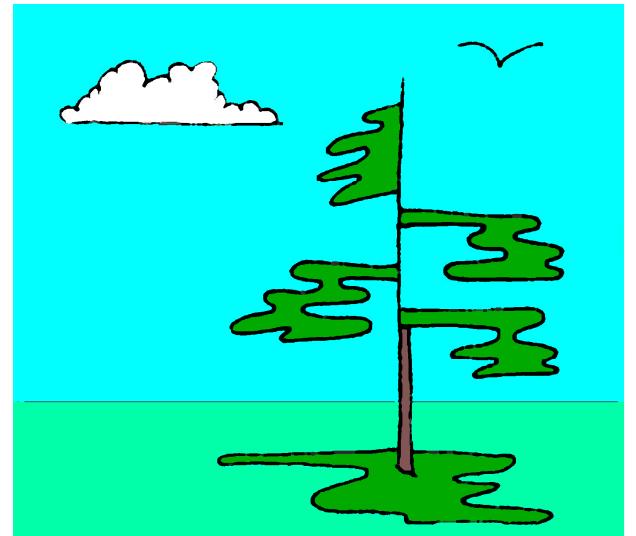
Created using SMath Studio, a MathCAD workalike from <https://en.smath.info/view/SMathStudio>  
The User is responsible to verify data using an alternative method

**Menu:**

[Yellow Box] Enter Data Space [Blue Box] Important Output [Green Box] Logical Constructs [Blue Text: Units]  
[Red Box] Summation

**Defined Units:**

$K := \text{kip}$	kilopounds (force)
$\text{kN\_m} := \text{kN m}$	kiloNewton-Metres (Moment)
$\text{Klf} := \frac{\text{kip}}{\text{ft}}$	Kips per Lineal Foot (Line Load)
$\text{kNpm} := \frac{\text{kN}}{\text{m}}$	kiloNewtons per Metre (Line Load)
$\text{kNsm} := \frac{\text{kN}}{\text{m}^2}$	kiloNewtons per Square Metre (Area Load)
$\text{ksf} := \frac{\text{kip}}{\text{ft}^2}$	Kips per Square Foot (Area Load)
$\text{Nsm} := \frac{\text{N}}{\text{m}^2}$	Newton's per Square Metre (Area Load)
$\text{lb} := \text{lbf}$	Pounds Force Override



## Loads (Area Load)

$D_A := 12 \text{ psf} = 0.5746 \text{ kPa}$  Dead Load

$L_A := 12 \text{ psf} = 0.5746 \text{ kPa}$  Live Load

$S_A := 12 \text{ psf} = 0.5746 \text{ kPa}$  Snow Load

$W_A := 12 \text{ psf} = 0.5746 \text{ kPa}$  Wind Load

$$PL_A := 12 \text{ psf} = 0.5746 \text{ kPa}$$

Pattern Load

$$E_A := 12 \text{ psf} = 0.5746 \text{ kPa}$$

Seismic Load

**Loads (Concentrated Load)**

$$D_C := 1 \text{ K} = 4.4482 \text{ kN}$$

Dead Load

$$L_C := 1 \text{ K} = 4.4482 \text{ kN}$$

Live Load

$$S_C := 1 \text{ K} = 4.4482 \text{ kN}$$

Snow Load

$$W_C := 1 \text{ K} = 4.4482 \text{ kN}$$

Wind Load

$$PL_C := 1 \text{ K} = 4.4482 \text{ kN}$$

Pattern Load

$$E_C := 1 \text{ K} = 4.4482 \text{ kN}$$

Seismic Load

**Loads (Line Load)**

$$D_L := 1 \text{ Kl}f = 14.5939 \text{ kNpm}$$

Dead Load

$$L_L := 1 \text{ Kl}f = 14.5939 \text{ kNpm}$$

Live Load

$$S_L := 1 \text{ Kl}f = 14.5939 \text{ kNpm}$$

Snow Load

$$W_L := 1 \text{ Kl}f = 14.5939 \text{ kNpm}$$

Wind Load

$$PL_L := 1 \text{ Kl}f = 14.5939 \text{ kNpm}$$

Pattern Load

$$E_L := 1 \text{ Kl}f = 14.5939 \text{ kNpm}$$

Seismic Load

## Load Combinations (Area Load)

$q_1 := 1.4 \cdot D_A$	8.3.2 Table C.1 Case 1
$q_2 := 1.25 \cdot D_A + 1.5 \cdot L_A$	8.3.2 Table C.1 Case 2
$q_3 := 1.25 \cdot D_A + 1.5 \cdot L_A + 0.5 \cdot S_A$	
$q_4 := 1.25 \cdot D_A + 1.5 \cdot L_A + 0.4 \cdot W_A$	
$q_5 := 1.25 \cdot D_A + 1.5 \cdot L_A - 0.4 \cdot W_A$	
$q_6 := 0.9 \cdot D_A + 1.5 \cdot L_A$	
$q_7 := 0.9 \cdot D_A + 1.5 \cdot L_A + 0.5 \cdot S_A$	
$q_8 := 0.9 \cdot D_A + 1.5 \cdot L_A + 0.4 \cdot W_A$	
$q_9 := 0.9 \cdot D_A + 1.5 \cdot L_A - 0.4 \cdot W_A$	
$q_{10} := 1.24 \cdot D_A + 1.5 \cdot (0.75 \cdot PL_A)$	13.8.4.3
$q_{11} := 1.25 \cdot D_A + 1.5 \cdot S_A$	8.3.2 Table C.1 Case 3
$q_{12} := 1.25 \cdot D_A + 1.5 \cdot S_A + 0.5 \cdot L_A$	
$q_{13} := 1.25 \cdot D_A + 1.5 \cdot S_A + 0.4 \cdot W_A$	
$q_{14} := 0.9 \cdot D_A + 1.5 \cdot S_A$	
$q_{15} := 0.9 \cdot D_A + 1.5 \cdot S_A + 0.5 \cdot L_A$	
$q_{16} := 0.9 \cdot D_A + 1.5 \cdot S_A + 0.4 \cdot W_A$	
$q_{17} := 0.9 \cdot D_A + 1.5 \cdot S_A - 0.4 \cdot W_A$	
$q_{18} := 1.25 \cdot D_A + 1.4 \cdot W_A$	8.3.2 Table C.1 Case 4
$q_{19} := 1.25 \cdot D_A - 1.4 \cdot W_A$	
$q_{20} := 1.25 \cdot D_A + 0.5 \cdot L_A + 1.4 \cdot W_A$	
$q_{21} := 1.25 \cdot D_A + 0.5 \cdot L_A - 1.4 \cdot W_A$	
$q_{22} := 1.25 \cdot D_A + 0.5 \cdot S_A + 1.4 \cdot W_A$	
$q_{23} := 1.25 \cdot D_A + 0.5 \cdot S_A - 1.4 \cdot W_A$	
$q_{24} := 0.9 \cdot D_A + 1.4 \cdot W_A$	
$q_{25} := 0.9 \cdot D_A - 1.4 \cdot W_A$	
$q_{26} := 0.9 \cdot D_A + 0.5 \cdot L_A + 1.4 \cdot W_A$	
$q_{27} := 0.9 \cdot D_A + 0.5 \cdot L_A - 1.4 \cdot W_A$	
$q_{28} := 0.9 \cdot D_A + 0.5 \cdot S_A + 1.4 \cdot W_A$	
$q_{29} := 0.9 \cdot D_A + 0.5 \cdot S_A - 1.4 \cdot W_A$	
$q_{30} := 1.0 \cdot D_A + 1.0 \cdot E_A$	8.3.2 Table C.1 Case 4
$q_{31} := 1.0 \cdot D_A - 1.0 \cdot E_A$	
$q_{32} := 1.0 \cdot D_A + 0.5 \cdot L_A + 1.0 \cdot E_A$	
$q_{33} := 1.0 \cdot D_A + 0.5 \cdot L_A - 1.0 \cdot E_A$	
$q_{34} := 1.0 \cdot D_A + 0.25 \cdot S_A + 1.0 \cdot E_A$	
$q_{35} := 1.0 \cdot D_A + 0.25 \cdot S_A - 1.0 \cdot E_A$	
$q_{36} := 1.0 \cdot D_A + 0.5 \cdot L_A + 0.25 \cdot S_A + 1.0 \cdot E_A$	

$$q_{37} := 1.0 \cdot D_A + 0.5 \cdot L_A + 0.25 \cdot S_A - 1.0 \cdot E_A$$

$$q_{1f} := \max \left( [ q_1 \ q_2 \ q_3 \ q_4 \ q_5 \ q_6 \ q_7 \ q_8 \ q_9 \ q_{10} \ q_{11} \ q_{12} \ q_{13} \ q_{14} \ q_{15} \ q_{16} \ q_{17} \ q_{18} \ q_{19} \ q_{20} ] \right)$$

$$q_{2f} := \max \left( [ q_{21} \ q_{22} \ q_{23} \ q_{24} \ q_{25} \ q_{26} \ q_{27} \ q_{28} \ q_{29} \ q_{30} \ q_{31} \ q_{32} \ q_{33} \ q_{34} \ q_{35} \ q_{36} \ q_{37} ] \right)$$

$$q_f := \max \left( [ q_{1f} \ q_{2f} ] \right)$$

$$q_f = 39 \text{ psf}$$

## Load Combinations (Concentrated Load)

$q_1 := 1.4 \cdot D_C$	8.3.2 Table C.1 Case 1
$q_2 := 1.25 \cdot D_C + 1.5 \cdot L_C$	8.3.2 Table C.1 Case 2
$q_3 := 1.25 \cdot D_C + 1.5 \cdot L_C + 0.5 \cdot S_C$	
$q_4 := 1.25 \cdot D_C + 1.5 \cdot L_C + 0.4 \cdot W_C$	
$q_5 := 1.25 \cdot D_C + 1.5 \cdot L_C - 0.4 \cdot W_C$	
$q_6 := 0.9 \cdot D_C + 1.5 \cdot L_C$	
$q_7 := 0.9 \cdot D_C + 1.5 \cdot L_C + 0.5 \cdot S_C$	
$q_8 := 0.9 \cdot D_C + 1.5 \cdot L_C + 0.4 \cdot W_C$	
$q_9 := 0.9 \cdot D_C + 1.5 \cdot L_C - 0.4 \cdot W_C$	
$q_{10} := 1.24 \cdot D_C + 1.5 \cdot (0.75 \cdot PL_C)$	13.8.4.3
$q_{11} := 1.25 \cdot D_C + 1.5 \cdot S_C$	8.3.2 Table C.1 Case 3
$q_{12} := 1.25 \cdot D_C + 1.5 \cdot S_C + 0.5 \cdot L_C$	
$q_{13} := 1.25 \cdot D_C + 1.5 \cdot S_C + 0.4 \cdot W_C$	
$q_{14} := 0.9 \cdot D_C + 1.5 \cdot S_C$	
$q_{15} := 0.9 \cdot D_C + 1.5 \cdot S_C + 0.5 \cdot L_C$	
$q_{16} := 0.9 \cdot D_C + 1.5 \cdot S_C + 0.4 \cdot W_C$	
$q_{17} := 0.9 \cdot D_C + 1.5 \cdot S_C - 0.4 \cdot W_C$	
$q_{18} := 1.25 \cdot D_C + 1.4 \cdot W_C$	8.3.2 Table C.1 Case 4
$q_{19} := 1.25 \cdot D_C - 1.4 \cdot W_C$	
$q_{20} := 1.25 \cdot D_C + 0.5 \cdot L_C + 1.4 \cdot W_C$	
$q_{21} := 1.25 \cdot D_C + 0.5 \cdot L_C - 1.4 \cdot W_C$	
$q_{22} := 1.25 \cdot D_C + 0.5 \cdot S_C + 1.4 \cdot W_C$	
$q_{23} := 1.25 \cdot D_C + 0.5 \cdot S_C - 1.4 \cdot W_C$	
$q_{24} := 0.9 \cdot D_C + 1.4 \cdot W_C$	
$q_{25} := 0.9 \cdot D_C - 1.4 \cdot W_C$	
$q_{26} := 0.9 \cdot D_C + 0.5 \cdot L_C + 1.4 \cdot W_C$	
$q_{27} := 0.9 \cdot D_C + 0.5 \cdot L_C - 1.4 \cdot W_C$	8.3.2 Table C.1 Case 4
$q_{28} := 0.9 \cdot D_C + 0.5 \cdot S_C + 1.4 \cdot W_C$	
$q_{29} := 0.9 \cdot D_C + 0.5 \cdot S_C - 1.4 \cdot W_C$	
$q_{30} := 1.0 \cdot D_C + 1.0 \cdot E_C$	
$q_{31} := 1.0 \cdot D_C - 1.0 \cdot E_C$	
$q_{32} := 1.0 \cdot D_C + 0.5 \cdot L_C + 1.0 \cdot E_C$	
$q_{33} := 1.0 \cdot D_C + 0.5 \cdot L_C - 1.0 \cdot E_C$	
$q_{34} := 1.0 \cdot D_C + 0.25 \cdot S_C + 1.0 \cdot E_C$	
$q_{35} := 1.0 \cdot D_C + 0.25 \cdot S_C - 1.0 \cdot E_C$	
$q_{36} := 1.0 \cdot D_C + 0.5 \cdot L_C + 0.25 \cdot S_C + 1.0 \cdot E_C$	

$$q_{37} := 1.0 \cdot D_C + 0.5 \cdot L_C + 0.25 \cdot S_C - 1.0 \cdot E_C$$

$$Q_{1f} := \max \left( [ q_1 \ q_2 \ q_3 \ q_4 \ q_5 \ q_6 \ q_7 \ q_8 \ q_9 \ q_{10} \ q_{11} \ q_{12} \ q_{13} \ q_{14} \ q_{15} \ q_{16} \ q_{17} \ q_{18} \ q_{19} \ q_{20} ] \right)$$

$$Q_{2f} := \max \left( [ q_{21} \ q_{22} \ q_{23} \ q_{24} \ q_{25} \ q_{26} \ q_{27} \ q_{28} \ q_{29} \ q_{30} \ q_{31} \ q_{32} \ q_{33} \ q_{34} \ q_{35} \ q_{36} \ q_{37} ] \right)$$

$$Q_f := \max \left( [ Q_{1f} \ Q_{2f} ] \right)$$

$$Q_f = 14.4567 \text{ kN}$$

**Load Combinations (Line Load)**

$q_1 := 1.4 \cdot D_L$	8.3.2 Table C.1 Case 1
$q_2 := 1.25 \cdot D_L + 1.5 \cdot L_L$	8.3.2 Table C.1 Case 2
$q_3 := 1.25 \cdot D_L + 1.5 \cdot L_L + 0.5 \cdot S_L$	
$q_4 := 1.25 \cdot D_L + 1.5 \cdot L_L + 0.4 \cdot W_L$	
$q_5 := 1.25 \cdot D_L + 1.5 \cdot L_L - 0.4 \cdot W_L$	
$q_6 := 0.9 \cdot D_L + 1.5 \cdot L_L$	
$q_7 := 0.9 \cdot D_L + 1.5 \cdot L_L + 0.5 \cdot S_L$	
$q_8 := 0.9 \cdot D_L + 1.5 \cdot L_L + 0.4 \cdot W_L$	
$q_9 := 0.9 \cdot D_L + 1.5 \cdot L_L - 0.4 \cdot W_L$	
$q_{10} := 1.24 \cdot D_L + 1.5 \cdot (0.75 \cdot PL_L)$	13.8.4.3
$q_{11} := 1.25 \cdot D_L + 1.5 \cdot S_L$	8.3.2 Table C.1 Case 3
$q_{12} := 1.25 \cdot D_L + 1.5 \cdot S_L + 0.5 \cdot L_L$	
$q_{13} := 1.25 \cdot D_L + 1.5 \cdot S_L + 0.4 \cdot W_L$	
$q_{14} := 0.9 \cdot D_L + 1.5 \cdot S_L$	
$q_{15} := 0.9 \cdot D_L + 1.5 \cdot S_L + 0.5 \cdot L_L$	
$q_{16} := 0.9 \cdot D_L + 1.5 \cdot S_L + 0.4 \cdot W_L$	
$q_{17} := 0.9 \cdot D_L + 1.5 \cdot S_L - 0.4 \cdot W_L$	
$q_{18} := 1.25 \cdot D_L + 1.4 \cdot W_L$	8.3.2 Table C.1 Case 4
$q_{19} := 1.25 \cdot D_L - 1.4 \cdot W_L$	
$q_{20} := 1.25 \cdot D_L + 0.5 \cdot L_L + 1.4 \cdot W_L$	
$q_{21} := 1.25 \cdot D_L + 0.5 \cdot L_L - 1.4 \cdot W_L$	
$q_{22} := 1.25 \cdot D_L + 0.5 \cdot S_L + 1.4 \cdot W_L$	
$q_{23} := 1.25 \cdot D_L + 0.5 \cdot S_L - 1.4 \cdot W_L$	
$q_{24} := 0.9 \cdot D_L + 1.4 \cdot W_L$	
$q_{25} := 0.9 \cdot D_L - 1.4 \cdot W_L$	
$q_{26} := 0.9 \cdot D_L + 0.5 \cdot L_L + 1.4 \cdot W_L$	
$q_{27} := 0.9 \cdot D_L + 0.5 \cdot L_L - 1.4 \cdot W_L$	
$q_{28} := 0.9 \cdot D_L + 0.5 \cdot S_L + 1.4 \cdot W_L$	8.3.2 Table C.1 Case 4
$q_{29} := 0.9 \cdot D_L + 0.5 \cdot S_L - 1.4 \cdot W_L$	
$q_{30} := 1.0 \cdot D_L + 1.0 \cdot E_L$	
$q_{31} := 1.0 \cdot D_L - 1.0 \cdot E_L$	
$q_{32} := 1.0 \cdot D_L + 0.5 \cdot L_L + 1.0 \cdot E_L$	
$q_{33} := 1.0 \cdot D_L + 0.5 \cdot L_L - 1.0 \cdot E_L$	
$q_{34} := 1.0 \cdot D_L + 0.25 \cdot S_L + 1.0 \cdot E_L$	
$q_{35} := 1.0 \cdot D_L + 0.25 \cdot S_L - 1.0 \cdot E_L$	
$q_{36} := 1.0 \cdot D_L + 0.5 \cdot L_L + 0.25 \cdot S_L + 1.0 \cdot E_L$	

$$q_{37} := 1.0 \cdot D_L + 0.5 \cdot L_L + 0.25 \cdot S_L - 1.0 \cdot E_L$$

$$Q_{1f} := \max \left( [ q_1 \ q_2 \ q_3 \ q_4 \ q_5 \ q_6 \ q_7 \ q_8 \ q_9 \ q_{10} \ q_{11} \ q_{12} \ q_{13} \ q_{14} \ q_{15} \ q_{16} \ q_{17} \ q_{18} \ q_{19} \ q_{20} ] \right)$$

$$Q_{2f} := \max \left( [ q_{21} \ q_{22} \ q_{23} \ q_{24} \ q_{25} \ q_{26} \ q_{27} \ q_{28} \ q_{29} \ q_{30} \ q_{31} \ q_{32} \ q_{33} \ q_{34} \ q_{35} \ q_{36} \ q_{37} ] \right)$$

$$Q_f := \max \left( [ Q_{1f} \ Q_{2f} ] \right)$$

$$Q_f = 3.25 \text{ kNf}$$

$$Q_f = 47.43 \text{ kNpm}$$