

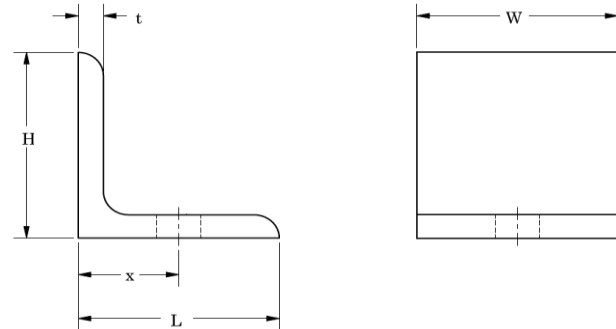
Seismic Leg Clips

Pressure Vessel Design Manual - 4rd Edition - Dennis Moss: Procedure 4-15

Description: Seismic Legs (2)

Leg Data:

	Material
16,600	S [psi] - allowable stress
3	N - number of legs
4.00	L [in] - base length
4.00	W [in] - leg width
4.00	H [in] - height
2.00	x [in] - hole location from back
0.50	t [in] - thickness
0.50	leg [in] - weld leg



Bolt Data:

	Material:
7,000	Sb [psi] - bolt strength
0.75-10 UNC 2A	Bolt - bolt size

Seismic Load Data:

54.00	D [in] - skirt outside diameter
0.375	ts [in] - skirt thickness
11,946.30	Wb [lb] - vessel weight
1,156.00	Ss [lbf] - seismic shear, skirt bottom
6,959.00	Mb [lbf-ft] - bending moment, skirt bottom

Variables:

1	FT [psi] = $1.33 * S$	$1.33 * 16600 =$	22,078
2	FC [psi] = $1.33 * S$	$1.33 * 16600 =$	22,078
3	d [in] = $D + (2 * x)$ bolt circlce diameter	$54 + (2 * 2) =$	58.0000
4	deg [°] = $IF(N=3,30,IF(N=4,45,0))$	$IF(3=3,30,IF(3=4,45,0)) =$	30.0000

Anchor Bolts:

5	fs [lb] = $(48 * Mb) / (d * N) - (Wb / N)$ tension force per bolt	$(48 * 6959) / (58 * 3) - (11946.3 / 3) =$	-2062.3759
6	Ab [in²] = Lookup("B1.1Table2", "RootArea", Bolt) bolt root area		0.3024
7	Abr [in²] = fs / Sb required bolt area	$-2062.376 / 7000 =$	-0.2946
8	ckAb = $Ab \geq Abr$	$0.302 \geq -0.295 =$	Ok

Base Plate:

9	h [in] = $(d / 2) * \cos(\text{RAD}(\text{deg}))$	$(58 / 2) * \cos(\text{RADIANS}(30)) =$	25.1147
10	I [lbf-in] = $2 * h^2$ moment of inertia at clips	$2 * 25.115^2 =$	1,261.50
11	Pmax [lb] = $((Mb * 12 * h) / I) + (Wb / N)$	$((6959 * 12 * 25.115) / 1261.5) + (11946.3 / 3) =$	5,644.63
12	f'c [psi] = $((48 * Mb) / (\pi * d^2 * L)) + (Wb / (\pi * d * L))$ bearing pressure (average at bolt circle)	$((48 * 6959) / (\pi * 58^2 * 4)) + (11946.3 / (\pi * 58 * 4)) =$	16.5564
13	tb [in] = $L * \text{SQRT}((3 * f'c) / S)$ minimum base thickness	$4 * \text{SQRT}((3 * 16.556) / 16600) =$	0.2188
14	ckt = $t \geq tb$	$0.5 \geq 0.219 =$	Ok
16	fc [psi] = $Pmax / f'c$	$5644.63 / 16.556 =$	340.9338
17	wb [in] = $L * \text{SQRT}((3 * fc) / S)$ minimum base width ('L')	$4 * \text{SQRT}((3 * 340.934) / 16600) =$	0.9929
18	ckt = $L \geq wb$	$4 \geq 0.993 =$	Ok

Skirt:

19	FLT [lb/in] = $((48 * Mb) / (\pi * D^2)) + (Wb / (\pi * D))$ axial load, tension	$((48 * 6959) / (\pi * 54^2)) + (11946.3 / (\pi * 54)) =$	106.8818447
20			
21	FLC [lb/in] = $-((48 * Mb) / (\pi * D^2)) + (Wb / (\pi * D))$ axial load, tension	$-((48 * 6959) / (\pi * 54^2)) + (11946.3 / (\pi * 54)) =$	33.9561
22			

23	tsk [in] = MAX(fLT/FT,fLC/FC)	min. skirt thickness	MAX(106.882/22078,33.956/22078) =	0.0048
24	cktsk = ts>=tsk		0.375>=0.005 =	Ok
Weld Check:				
25	wl [in] = (H+H+W+(leg*2))	weld length	(4+4+4+(0.5*2)) =	13.0000
26	WeldArea [in ²] = wl*leg		13*0.5 =	6.5000
27	SSw [psi] = S*0.49	UW-15(c) max weld shear	16600*0.49 =	8,134.00
28	CheckSSW = Ss/WeldArea<=SSw		1156/6.5<=8134 =	Ok