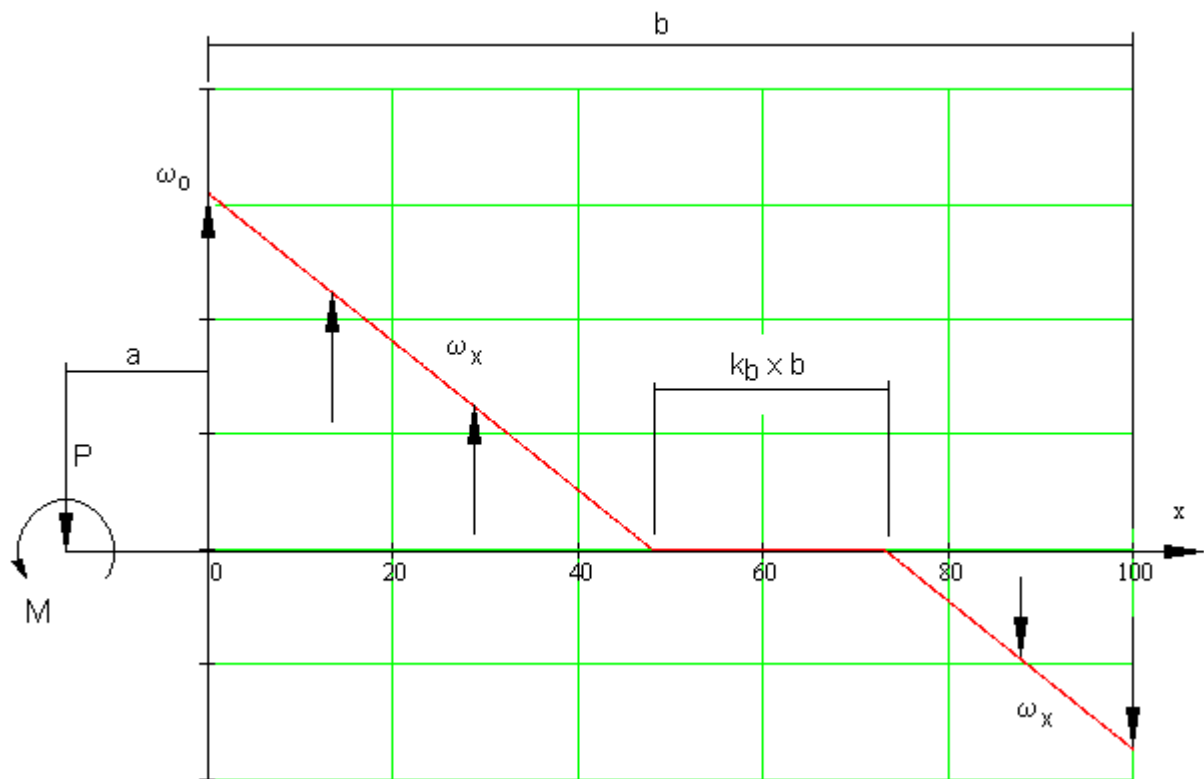


Pin Loaded Socket Analysis



$a := 20 \cdot \text{mm}$... point of load application on pin from mouth of socket

$b := 100 \cdot \text{mm}$... length of socket

$P := 20 \cdot \text{kN}$... applied pin loading

$M := 100 \cdot \text{N} \cdot \text{m}$... applied moment at free end of pin

$k_b := 0.67$... factor defining unloaded section length
inside socket (unloaded length = $b \times k_b$)

Distributed socket loading

$$\omega(x, \omega_0, \omega_x) := \omega_0 + \omega_x \cdot x - \omega_x \cdot \left(x - \frac{-\omega_0}{\omega_x} \right) \cdot \left(x > \frac{-\omega_0}{\omega_x} \right) \dots$$

$$+ \omega_x \cdot \left[x - \left(-\frac{\omega_0}{\omega_x} + k_b \cdot b \right) \right] \cdot \left[x \geq \left(-\frac{\omega_0}{\omega_x} + k_b \cdot b \right) \right]$$

Where ω_0 is the distributed load at $x = 0$ and ω_x is the rate of change in distributed loading.

$$\Sigma P(\omega_0, \omega_x) := \omega_0 \cdot b + \frac{1}{2} \cdot \omega_x \cdot b^2 - \frac{1}{2} \cdot \omega_x \cdot \left(b - \frac{-\omega_0}{\omega_x} \right)^2 \dots \dots \text{... summing distributed loading over socket length}$$

$$+ \frac{1}{2} \cdot \omega_x \cdot \left[b - \left(-\frac{\omega_0}{\omega_x} + k_b \cdot b \right) \right]^2$$

$$\Sigma M(\omega_0, \omega_x) := \frac{1}{2} \cdot \omega_0 \cdot b^2 + \frac{1}{6} \cdot \omega_x \cdot b^3 - \frac{1}{6} \cdot \omega_x \cdot \left(b - \frac{-\omega_0}{\omega_x} \right)^3 \dots \dots \text{... BM at end of socket length}$$

$$+ \frac{1}{6} \cdot \omega_x \cdot \left[b - \left(-\frac{\omega_0}{\omega_x} + k_b \cdot b \right) \right]^3$$

Given $\Sigma P(\omega_0, \omega_x) = P$... equ. 1, equating forces

$$M + P \cdot (a + b) - \Sigma M(\omega_0, \omega_x) = 0 \cdot \text{N} \cdot \text{mm} \dots \text{... equ. 2, moment at end of pin}$$

Solving ... $\omega_0 = 2503.21 \frac{\text{N}}{\text{mm}}$... and ... $\omega_x = -114.98 \frac{\text{N}}{\text{mm}^2}$

$$\omega_b(x) := \left[\omega_0 + \omega_x \cdot x - \omega_x \cdot \left(x - \frac{-\omega_0}{\omega_x} \right) \cdot \left(x > \frac{-\omega_0}{\omega_x} \right) \right] \dots \dots \text{distributed loading}$$

$$+ \omega_x \cdot \left[x - \left(\frac{\omega_0}{\omega_x} + k_b \cdot b \right) \right] \cdot \left[x \geq \left(\frac{\omega_0}{\omega_x} + k_b \cdot b \right) \right]$$

$$P_\omega(x) := P - \left[\omega_0 \cdot x + \frac{1}{2} \cdot \omega_x \cdot x^2 - \frac{1}{2} \cdot \omega_x \cdot \left(x - \frac{-\omega_0}{\omega_x} \right)^2 \cdot \left(x > \frac{-\omega_0}{\omega_x} \right) \dots \dots \text{Pin shear} \right.$$

$$\left. + \frac{1}{2} \cdot \omega_x \cdot \left[x - \left(\frac{\omega_0}{\omega_x} + k_b \cdot b \right) \right]^2 \cdot \left[x \geq \left(\frac{\omega_0}{\omega_x} + k_b \cdot b \right) \right] \right]$$

$$M_\omega(x) := M + P \cdot (a + x) - \left[\frac{1}{2} \cdot \omega_0 \cdot x^2 + \frac{1}{6} \cdot \omega_x \cdot x^3 - \frac{1}{6} \cdot \omega_x \cdot \left(x - \frac{-\omega_0}{\omega_x} \right)^3 \cdot \left(x > \frac{-\omega_0}{\omega_x} \right) \dots \dots \text{Pin BM} \right.$$

$$\left. + \frac{1}{6} \cdot \omega_x \cdot \left[x - \left(\frac{\omega_0}{\omega_x} + k_b \cdot b \right) \right]^3 \cdot \left[x \geq \left(\frac{\omega_0}{\omega_x} + k_b \cdot b \right) \right] \right]$$

$$x_p := - \left[\frac{\omega_0}{\omega_x} + \sqrt{2 \cdot \frac{P}{\omega_x} + \left(\frac{\omega_0}{\omega_x} \right)^2} \right] \quad x_p = 10.542 \text{ mm} \quad \dots \text{location of max. BM}$$

$$M_{\max} := M_\omega(x_p) \quad M_{\max} = 594.2 \text{ N} \cdot \text{m} \quad \dots \text{max. BM}$$

$$x_{\text{fwd}} := - \frac{\omega_0}{\omega_x} \quad x_{\text{fwd}} = 21.77 \text{ mm} \quad \dots \text{and} \dots \quad x_{\text{aft}} := x_{\text{fwd}} + k_b \cdot b \quad x_{\text{aft}} = 88.77 \text{ mm}$$

$$\text{Checks} \dots \quad P_\omega(b) = 0.00 \text{ N} \quad \dots \text{and} \dots \quad M_\omega(b) = -0.00 \text{ N} \cdot \text{m}$$

