

Thermal performance calculator according to the ISO 13786

$$kJ := 10^3 \cdot J$$

Assembly characteristics:

	Layer1 - Clay based plaster	Layer2 - Hempcrete
Width	$d1 := 0.01 \cdot m$	$d2 := 0.01 \cdot m$
Specific heat capacity	$c1 := 880 \cdot \frac{J}{kg \cdot K}$	$c2 := 1600 \cdot \frac{J}{kg \cdot K}$
Density	$\rho1 := 1800 \cdot \frac{kg}{m^3}$	$\rho2 := 300 \cdot \frac{kg}{m^3}$
Thermal conductivity	$\lambda1 := 0.8 \cdot \frac{W}{m \cdot K}$	$\lambda2 := 0.07 \cdot \frac{W}{m \cdot K}$

Interior layer thermal resistance

$$R_{si} := \frac{1}{8.7} \cdot \frac{m^2 \cdot K}{W}$$

Exterior layer thermal resistance

$$R_{se} := \frac{1}{23} \cdot \frac{m^2 \cdot K}{W}$$

Temperature oscillation time

$$Time := 24 \cdot 60 \cdot 60 \cdot sec$$

$$u_value := \frac{1}{R_{si} + \frac{d1}{\lambda1} + \frac{d2}{\lambda2} + R_{se}} = 3.187 \frac{W}{m^2 \cdot K}$$

Penetration depth

$$\delta1 := \sqrt{\frac{\lambda1 \cdot Time}{\pi \cdot \rho1 \cdot c1}} = 0.118 \ m$$

$$\delta2 := \sqrt{\frac{\lambda2 \cdot Time}{\pi \cdot \rho2 \cdot c2}} = 0.063 \ m$$

Dimensionless penetration depth

$$\xi_1 := \frac{d_1}{\delta_1} = 0.085$$

$$\xi_2 := \frac{d_2}{\delta_2} = 0.158$$

Thermal transmittance matrix component

Layer1

$$z_{11} := \cosh(\xi_1) \cdot \cos(\xi_1) + \sqrt{-1} \cdot \sinh(\xi_1) \cdot \sin(\xi_1) = 1 + 0.007i$$

$$z_{22} := z_{11} = 1 + 0.007i$$

$$z_{12} := \frac{-\delta_1}{2 \cdot \lambda_1} \cdot \left(\sinh(\xi_1) \cdot \cos(\xi_1) + \cosh(\xi_1) \cdot \sin(\xi_1) + \sqrt{-1} \cdot (\cosh(\xi_1) \cdot \sin(\xi_1) - \sinh(\xi_1) \cdot \cos(\xi_1)) \right) = (-0.012 - 3i \cdot 10^{-5}) \frac{m^2 \cdot K}{W}$$

$$z_{21} := \frac{-\lambda_1}{\delta_1} \cdot \left(\sinh(\xi_1) \cdot \cos(\xi_1) - \cosh(\xi_1) \cdot \sin(\xi_1) + \sqrt{-1} \cdot (\cosh(\xi_1) \cdot \sin(\xi_1) + \sinh(\xi_1) \cdot \cos(\xi_1)) \right) = (0.003 - 1.152i) \frac{W}{m^2 \cdot K}$$

Layer2

$$z_{11_2} := \cosh(\xi_2) \cdot \cos(\xi_2) + \sqrt{-1} \cdot \sinh(\xi_2) \cdot \sin(\xi_2) = 1 + 0.025i$$

$$z_{22_2} := z_{11_2} = 1 + 0.025i$$

$$z_{12_2} := \frac{-\delta_2}{2 \cdot \lambda_2} \cdot \left(\sinh(\xi_2) \cdot \cos(\xi_2) + \cosh(\xi_2) \cdot \sin(\xi_2) + \sqrt{-1} \cdot (\cosh(\xi_2) \cdot \sin(\xi_2) - \sinh(\xi_2) \cdot \cos(\xi_2)) \right) = (-0.143 - 0.001i) \frac{m^2 \cdot K}{W}$$

$$z_{21_2} := \frac{-\lambda_2}{\delta_2} \cdot \left(\sinh(\xi_2) \cdot \cos(\xi_2) - \cosh(\xi_2) \cdot \sin(\xi_2) + \sqrt{-1} \cdot (\cosh(\xi_2) \cdot \sin(\xi_2) + \sinh(\xi_2) \cdot \cos(\xi_2)) \right) = (0.003 - 0.349i) \frac{W}{m^2 \cdot K}$$

Construction thermal transmittance matrix

Layer1

$$Z1 := \begin{bmatrix} z11 & z12 \cdot \frac{W}{m^2 \cdot K} \\ \frac{m^2 \cdot K}{W} \cdot z21 & z22 \end{bmatrix}$$

Layer2

$$Z2 := \begin{bmatrix} z11_2 & z12_2 \cdot \frac{W}{m^2 \cdot K} \\ \frac{m^2 \cdot K}{W} \cdot z21_2 & z22_2 \end{bmatrix}$$

$$Z := Z1 \cdot Z2 = \begin{bmatrix} 1 + 0.036i & -0.155 - 0.003i \\ 0.037 - 1.501i & 0.998 + 0.197i \end{bmatrix}$$

Boundary layer thermal transmittance matrix

$$Zs2 := \begin{bmatrix} 1 & -Rsi \cdot \frac{W}{m^2 \cdot K} \\ 0 & 1 \end{bmatrix}$$

$$Zs1 := \begin{bmatrix} 1 & -Rse \cdot \frac{W}{m^2 \cdot K} \\ 0 & 1 \end{bmatrix}$$

Construction thermal transmittance matrix from environment to environment

$$Zee := Zs2 \cdot Z \cdot Zs1 = \begin{bmatrix} 0.995 + 0.209i & -0.313 - 0.034i \\ 0.037 - 1.501i & 0.996 + 0.262i \end{bmatrix}$$

Decrement factor

$$f := \frac{\left| \operatorname{Im} \left(\frac{1}{Zee_{0,1}} \right) \right| \cdot \frac{W}{m^2 \cdot K}}{u_value} = 0.108$$

Internal area heat capacity, $\text{kJ/m}^2\text{K}$

$$k1 := \left| \frac{Zee_{1,1} - 1}{Zee_{0,1}} \right| \cdot \frac{24 \cdot \text{hr} \cdot W}{2 \cdot \pi \cdot m^2 \cdot K} = (11.43 \cdot 10^3) \frac{J}{m^2 \cdot K}$$

External area heat capacity, $\text{kJ/m}^2\text{K}$

$$k2 := \left| \frac{Zee_{0,0} - 1}{Zee_{0,1}} \right| \cdot \frac{24 \cdot \text{hr} \cdot W}{2 \cdot \pi \cdot m^2 \cdot K} = (9.12 \cdot 10^3) \frac{J}{m^2 \cdot K}$$

Periodic thermal transmittance, $\text{W/m}^2\text{K}$:

$$Y12 := \left| \text{Im} \left(\frac{1}{Zee_{0,1}} \right) \right| \cdot \frac{W}{m^2 \cdot K} = 0.345 \frac{W}{m^2 \cdot K}$$

Time shift periodic thermal transmittance, hr :

$$\Delta t_f := \frac{\text{atan2} \left(\text{Re} \left(\frac{1}{Zee_{0,1}} \right), \text{Im} \left(\frac{1}{Zee_{0,1}} \right) \right) \cdot 24 \cdot \text{hr}}{2 \cdot \pi} - 12 \cdot \text{hr} = -0.416 \text{ hr}$$

Time shift internal side, hr :

$$\Delta int := \frac{\text{atan2} \left(\text{Re} \left(-1 \cdot \frac{Zee_{1,1}}{Zee_{0,1}} \right), \text{Im} \left(-1 \cdot \frac{Zee_{1,1}}{Zee_{0,1}} \right) \right) \cdot 24 \cdot \text{hr}}{2 \cdot \pi} = 0.566 \text{ hr}$$

Internal thermal admittance, W/m^2K :

$$Y_{22} := \left| -1 \cdot \frac{Z_{ee_{1,1}}}{Z_{ee_{0,1}}} \right| \cdot \frac{W}{m^2 \cdot K} = 3.268 \frac{W}{m^2 \cdot K}$$

External thermal admittance, W/m^2K :

$$Y_{11} := \left| -1 \cdot \frac{Z_{ee_{0,0}}}{Z_{ee_{0,1}}} \right| \cdot \frac{W}{m^2 \cdot K} = 3.227 \frac{W}{m^2 \cdot K}$$

Timeshift external side, hr :

$$\Delta_{ext} := \frac{\text{atan2} \left(\text{Re} \left(-1 \cdot \frac{Z_{ee_{0,0}}}{Z_{ee_{0,1}}} \right), \text{Im} \left(-1 \cdot \frac{Z_{ee_{0,0}}}{Z_{ee_{0,1}}} \right) \right) \cdot 24 \cdot hr}{2 \cdot \pi} = 0.375 \text{ hr}$$

Algorithmisation of multilayered assembly calculation

$$d1 = 0.01 \text{ m}$$

$$d2 = 0.01 \text{ m}$$

$$n := 100$$

Internal := for $i \in 1..n$

$$d1_i \leftarrow 0.1 \cdot i \cdot d1$$

$$d2_i \leftarrow 0.5 \cdot i \cdot d2$$

$$u_value_i \leftarrow \frac{1}{Rsi + \frac{d1_i}{\lambda1} + \frac{d2_i}{\lambda2} + Rse}$$

$$\xi1_i \leftarrow \frac{d1_i}{\delta1}$$

$$\xi2_i \leftarrow \frac{d2_i}{\delta2}$$

$$z11_i \leftarrow \cosh(\xi1_i) \cdot \cos(\xi1_i) + \sqrt{-1} \cdot \sinh(\xi1_i) \cdot \sin(\xi1_i)$$

$$z22_i \leftarrow z11_i$$

$$z12_i \leftarrow \frac{-\delta1}{2 \cdot \lambda1} \cdot \left(\sinh(\xi1_i) \cdot \cos(\xi1_i) + \cosh(\xi1_i) \cdot \sin(\xi1_i) + \sqrt{-1} \cdot \left(\cosh(\xi1_i) \cdot \sin(\xi1_i) - \sinh(\xi1_i) \cdot \cos(\xi1_i) \right) \right)$$

$$z21_i \leftarrow \frac{-\lambda1}{\delta1} \cdot \left(\sinh(\xi1_i) \cdot \cos(\xi1_i) - \cosh(\xi1_i) \cdot \sin(\xi1_i) + \sqrt{-1} \cdot \left(\cosh(\xi1_i) \cdot \sin(\xi1_i) + \sinh(\xi1_i) \cdot \cos(\xi1_i) \right) \right)$$

$$z11_2_i \leftarrow \cosh(\xi2_i) \cdot \cos(\xi2_i) + \sqrt{-1} \cdot \sinh(\xi2_i) \cdot \sin(\xi2_i)$$

$$z22_2_i \leftarrow z11_2_i$$

$$z12_2_i \leftarrow \frac{-\delta2}{2 \cdot \lambda2} \cdot \left(\sinh(\xi2_i) \cdot \cos(\xi2_i) + \cosh(\xi2_i) \cdot \sin(\xi2_i) + \sqrt{-1} \cdot \left(\cosh(\xi2_i) \cdot \sin(\xi2_i) - \sinh(\xi2_i) \cdot \cos(\xi2_i) \right) \right)$$

$$-12 \cdot \sqrt{-1} \cdot \left(\cosh(\xi2_i) \cdot \sin(\xi2_i) - \sinh(\xi2_i) \cdot \cos(\xi2_i) \right)$$

$$\begin{aligned}
z1_{-2}_i &\leftarrow \frac{-\sqrt{2}}{\delta 2} \cdot \left(\sinh(\xi 2_i) \cdot \cos(\xi 2_i) - \cosh(\xi 2_i) \cdot \sin(\xi 2_i) + \sqrt{-1} \cdot \left(\cosh(\xi 2_i) \cdot \sin(\xi 2_i) + \sinh(\xi 2_i) \cdot \cos(\xi 2_i) \right) \right) \\
Z1_i &\leftarrow \begin{bmatrix} z11_i & z12_i \cdot \frac{W}{m^2 \cdot K} \\ z21_i \cdot \frac{m^2 \cdot K}{W} & z22_i \end{bmatrix} \\
Z2_i &\leftarrow \begin{bmatrix} z11_{-2}_i & z12_{-2}_i \cdot \frac{W}{m^2 \cdot K} \\ z21_{-2}_i \cdot \frac{m^2 \cdot K}{W} & z22_{-2}_i \end{bmatrix} \\
Z_i &\leftarrow Z1_i \cdot Z2_i \\
Zee_i &\leftarrow Zs2 \cdot Z_i \cdot Zs1 \\
f_i &\leftarrow \begin{cases} \text{if } u_value_i \leq 0.25 \cdot \frac{W}{m^2 \cdot K} \wedge d1_i > 0 \cdot m \wedge d2_i > 0 \cdot m \wedge d1_i + d2_i \leq 0.6 \cdot m \\ \frac{\left| \operatorname{Im} \left(\frac{1}{(Zee_i)_{0,1}} \right) \right|}{u_value_i} \\ \text{else} \\ 0 \end{cases} \\
k1_i &\leftarrow \begin{cases} \text{if } u_value_i \leq 0.25 \cdot \frac{W}{m^2 \cdot K} \wedge d1_i \neq 0 \cdot m \wedge d2_i \neq 0 \cdot m \wedge d1_i + d2_i \leq 0.6 \cdot m \\ \frac{\left| (Zee_i)_{1,1} - 1 \right|}{(Zee_i)_{0,1}} \cdot \frac{24 \cdot 3600}{2 \cdot \pi \cdot 1000} \end{cases}
\end{aligned}$$

Age Group	Male (%)	Female (%)
18-29	85	80
30-49	80	75
50-69	75	70
70+	70	65

Internal = ?