

# NorthWoods Software

Program Name: Weld-Group\_W

Project Name: -

Project Number: -

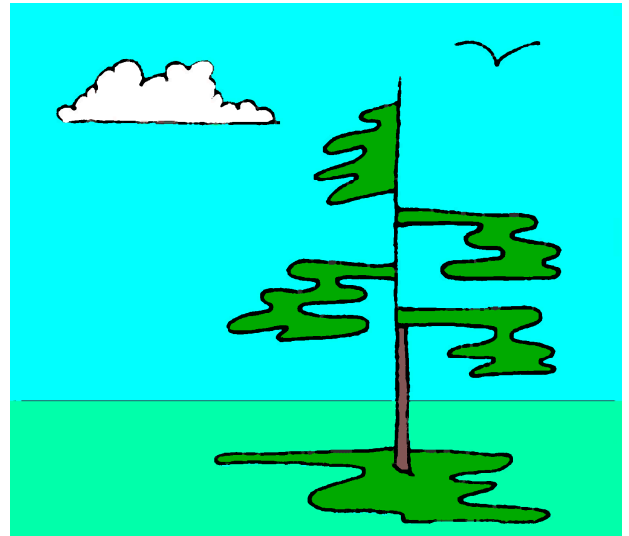
Project Description: -

Project Designer: Dik

Last Revised (yy-mm-dd): 21-02-25

Reference: NBCC, CSA S16,

Created using SMath Studio, a MathCAD workalike from <https://en.smath.info/view/SMathStudio>. The User is responsible to verify data using an alternative method



## Menu:

	Input Data		Important Output		Logical Constructs		Units
	Sum / For		Important Note				

## Defined Units:

$K := \text{kip}$						Force
$K_{ft} := K \text{ ft}$	$kN_m := kN \text{ m}$	$K_{in} := K \text{ in}$	$kN_{mm} := kN \text{ mm}$	$lb_{in} := lbf \text{ in}$		Moment
$pcf := \frac{lbf}{ft^3}$	$kN_{pcm} := \frac{kN}{m^3}$	$kg_{pcm} := \frac{kg}{m^3}$				Density
$K_{lf} := \frac{K}{ft}$	$plf := \frac{lbf}{ft}$	$kN_{pm} := \frac{kN}{m}$	$K_{pi} := \frac{K}{in}$	$kN_{pmm} := \frac{kN}{mm}$		Force/Unit Length
$pli := \frac{lbf}{in}$						Pressure
$psf := \frac{lbf}{ft^2}$	$K_{sf} := \frac{K}{ft^2}$	$K_{si} := \frac{K}{in^2}$	$kN_{psm} := \frac{kN}{m^2}$	$psi := \frac{lbf}{in^2}$		Subgrade Modulus
$pci := \frac{lbf}{in^3}$						Pressure per Depth
$psf_{pf} := \frac{psf}{ft}$	$kPa_{pm} := \frac{kPa}{m}$					Force
$pmcf := \frac{lb}{ft^3}$	$lb := lbf$					Velocity
$mph := \frac{mi}{hr}$	$kph := \frac{km}{hr}$					

## User Defined Functions:

```

Check (arg) := if arg = 1
                Check := "...OK"
            else
                Check := "...NG"

```

```

Check (2 = 3) = "...NG"
Check (2 ≠ 3) = "...OK"

```

```

Check (2 ≤ 3) = "...OK"
Check (3 ≥ 2) = "...OK"

```

**Input Data****Material Property Factors:**

$$\varphi_s := 0.90$$

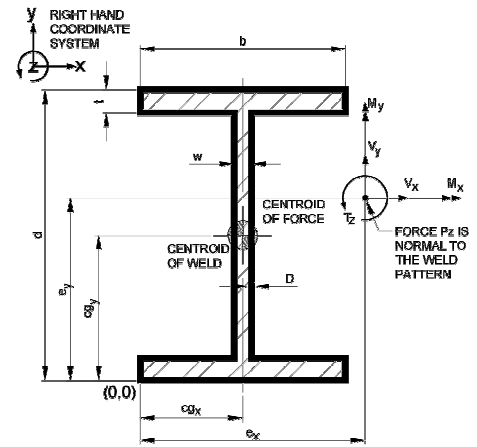
$$\varphi_w := 0.67$$

**Load Factors:**

$$\alpha_L := 1.50$$

$$\alpha_D := 1.25$$

**Weld interface is taken at the face of the attached member rather than the centreline of the weld.**

**Applied Factored Loads:**

$$P_{fz} := 0 \text{ K}$$

$$V_{fx} := 0 \text{ K}$$

$$V_{fy} := 292 \text{ K}$$

$$M_{fx} := 593 \text{ K\_ft}$$

$$M_{fy} := 0 \text{ K\_ft}$$

$$T_{fz} := 0 \text{ K\_ft}$$

**Load Eccentricity:**

$$e_x := 6.375 \text{ in}$$

$$e_y := 12.03 \text{ in}$$

$$e_z := 0 \text{ in}$$

$$P_{fz} = 0.00 \text{ kN} \quad \text{Axial Load}$$

$$V_{fx} = 0.00 \text{ kN} \quad \text{Shear (X-Axis)}$$

$$V_{fy} = 1298.88 \text{ kN} \quad \text{Shear (Y-Axis)}$$

$$M_{fx} = 804 \text{ kN\_m} \quad \text{Moment (X-Axis)}$$

$$M_{fy} = 0.00 \text{ kN\_m} \quad \text{Moment (Y-Axis)}$$

$$T_{fz} = 0.00 \text{ kN\_m} \quad \text{Torsion (Z-Axis)}$$

$$e_x = 161.9 \text{ mm} \quad \text{X-Axis Direction}$$

$$e_y = 305.6 \text{ mm} \quad \text{Y-Axis Direction}$$

$$e_z = 0.0 \text{ mm} \quad \text{Z-Axis Direction}$$

**W Shape Input Data:**

$$d := 24.06 \text{ in}$$

$$b := 12.75 \text{ in}$$

$$t := 0.75 \text{ in}$$

$$w := 0.50 \text{ in}$$

$$d' := d - 2 \cdot t$$

$$d' = 22.56 \text{ in}$$

$$d = 611.1 \text{ mm}$$

$$b = 323.8 \text{ mm}$$

$$t = 19 \text{ mm}$$

$$w = 12.7 \text{ mm}$$

$$d' = 573.02 \text{ mm}$$

$$b' := 0.5 \cdot (b - w)$$

$$b' = 6.125 \text{ in}$$

$$b' = 155.575 \text{ mm}$$

$$pts := \begin{bmatrix} s & x_i & y_i & x_j & y_j \\ 1 & 0 \text{ in} & 0 \text{ in} & 0 \text{ in} & t \\ 2 & 0 \text{ in} & t & b' & t \\ 3 & b' & t & b' & t + d' \\ 4 & b' & t + d' & 0 \text{ in} & t + d' \\ 5 & 0 \text{ in} & t + d' & 0 \text{ in} & d \\ 6 & 0 \text{ in} & d & b & d \\ 7 & b & d & b & t + d' \\ 8 & b & t + d' & b' + w & t + d' \\ 9 & b' + w & t + d' & b' + w & t \\ 10 & b' + w & t & b & t \\ 11 & b & t & b & 0 \text{ in} \\ 12 & b & 0 \text{ in} & 0 \text{ in} & 0 \text{ in} \end{bmatrix}$$

$$pts' := \text{submatrix}(pts, 1, \text{rows}(pts), 2, 5)$$

Used for Summary and Plotting Shape

```

for c ∈ [1..rows(pts')]
  ptsnc 1 := pts'c 1 ·  $\frac{1}{in}$ 
  ptsnc 2 := pts'c 2 ·  $\frac{1}{in}$ 
  ptsnc 3 := pts'c 3 ·  $\frac{1}{in}$ 
  ptsnc 4 := pts'c 4 ·  $\frac{1}{in}$ 

```

```
c := 0
```

```

for c ∈ [1..rows(ptsn)]
  weldc 1 := ptsnc 1
  weldc 2 := ptsnc 2

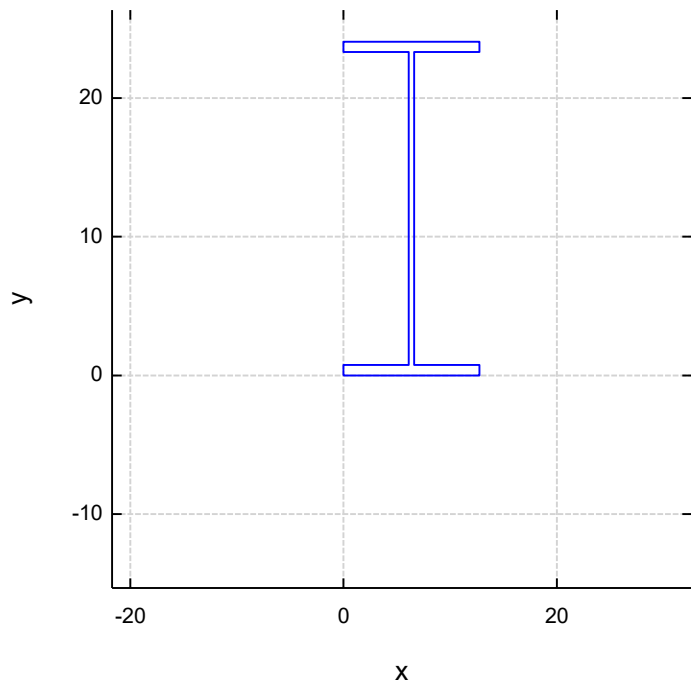
```

```
c := c + 1
```

```
weldc 1 := ptsn1 1
```

```
weldc 2 := ptsn1 2
```

### Weld Pattern



```
weld
```

### Base Metal Steel Properties:

```
stlNDX := 3
```

NDX	des	fy	Fu
1	"G40.21-350W"	50 Ksi	65 Ksi
2	"G40.21-300W"	44 Ksi	65 Ksi
3	"A36"	36 Ksi	58 Ksi

$desI_1 := stl_{NDX} 2$      $f_{y1} := stl_{NDX} 3$   
 $F_{u1} := stl_{NDX} 4$   
 $E_s := 29000 \text{ Ksi}$      $G_s := 10.9 \text{ Ksi}$      $\gamma_s := 489 \text{ pcf}$

### Welding Electrodes:

```
weNDX := 2
```

NDX	DesI	DesM	UTS
1	"E60xx"	"E410xx"	60 ksi
2	"E70xx"	"E480xx"	70 ksi
3	"E80xx"	"E550xx"	80 ksi
4	"E90xx"	"E620xx"	90 ksi

$desI_w := we_{NDX} 2$      $X_u := we_{NDX} 4$   
 $desM_w := we_{NDX} 3$

**Weld Sizes:**

$$ws_{NDX} := 14$$

	NDX	desl	desM	D
$ws :=$	1	""	"3mm"	0.11811 in
	2	"1/8"	""	0.125 in
	3	""	"4mm"	0.15748 in
	4	"3/16"	""	0.1875 in
	5	""	"5mm"	0.19685 in
	6	""	"6mm"	0.23622 in
	7	"1/4"	""	0.25 in
	8	""	"7mm"	0.275591 in
	9	"5/16"	""	0.3125 in
	10	""	"8mm"	0.314961 in
	11	""	"9mm"	0.354331 in
	12	"3/8"	""	0.375 in
	13	"7/16"	""	0.4375 in
	14	"1/2"	""	0.5 in

$$desI_D := ws_{NDX} 2 \quad desM_D := ws_{NDX} 3$$

$$D := ws_{NDX} 4$$

**Weld Strength:**

$$v_{rw} := \phi_w \cdot 0.67 \cdot X_u$$

$$v_{rw} = 31.4 \text{ ksi}$$

$$v_{rw} = 216.7 \text{ MPa}$$

Limit Weld Stress

**Base Strength:**

$$v_{rb} := \phi_s \cdot f_{y1}$$

$$v_{rb} = 32.4 \text{ Ksi}$$

$$v_{rb} = 223.4 \text{ MPa}$$

Limit Base Metal Stress

**Maximum Strength per Unit Length:**

$$v'_{rw} := v_{rw} \cdot D \cdot \frac{1}{\sqrt{2}}$$

$$v'_{rw} = 11.1 \text{ Kpi}$$

$$v'_{rw} = 1.9 \text{ kNpmm}$$

Weld Resist per Unit Len

$$v'_{rb} := v_{rb} \cdot D$$

$$v'_{rb} = 16.2 \text{ Kpi}$$

$$v'_{rb} = 2.8 \text{ kNpmm}$$

Base Resist per Unit Len

$$v_r := \min \left( \left[ v'_{rw} \quad v'_{rb} \right] \right)$$

$$v_r = 11.1 \text{ Kpi}$$

$$v_r = 1.9 \text{ kNpmm}$$

Min Resist per Unit Len

**Weld Properties:**

```

for r ∈ [1..rows(pts)]
  pts_r6 := (pts_r2 + pts_r4) / 2
  pts_r7 := (pts_r3 + pts_r5) / 2
  pts_r8 := pts_r4 - pts_r2
  pts_r9 := pts_r5 - pts_r3
  pts_r10 := sqrt((pts_r8)^2 + (pts_r9)^2)
  pts_r11 := (pts_r10 * (pts_r9)^2) / 12
  pts_r12 := (pts_r10 * (pts_r8)^2) / 12
  pts_r13 := pts_r10 * pts_r6
  pts_r14 := pts_r10 * pts_r7

```

 $c_x$  $c_y$  $m$  $n$  $L$  $I_{xx}$  $I_{yy}$  $L_{cx}$  $L_{cy}$

```

for r ∈ [1..rows(pts)]
  pts_r15 := pts_r6 - cg_x
  pts_r16 := pts_r7 - cg_y
  pts_r17 := pts_r11 + pts_r10 · pts_r162
  pts_r18 := pts_r12 + pts_r10 · (pts_r15)2
  pts_r19 := pts_r10 · pts_r15 · pts_r16
  pts_r20 := pts_r2 - cg_x
  pts_r21 := pts_r3 - cg_y
  pts_r22 := pts_r4 - cg_x
  pts_r23 := pts_r5 - cg_y

```

$d_x$   
 $d_y$   
 $I'_{xx}$   
 $I'_{yy}$   
 $I'_{xy}$   
 $d_{xi}$   
 $d_{yi}$   
 $d_{xj}$   
 $d_{yj}$

$A := \sum \text{col}(pts, 10)$	$A = 98.12 \text{ in}$	$A = 2492.2 \text{ mm}$	Total Length of Weld
$cg_x := \sum \left( \frac{\text{col}(pts, 13)}{A} \right)$	$cg_x = 6.38 \text{ in}$	$cg_x = 161.9 \text{ mm}$	Centroid of Weld X-Axis
$cg_y := \sum \left( \frac{\text{col}(pts, 14)}{A} \right)$	$cg_y = 12.03 \text{ in}$	$cg_y = 305.6 \text{ mm}$	Centroid of Weld Y-Axis
$I'_{xx} := \sum \text{col}(pts, 17)$	$I'_{xx} = 9129.0 \text{ in}^3$	$I'_{xx} = 1.50 \cdot 10^8 \text{ mm}^3$	Moment of Inertia (X-Axis)
$I'_{yy} := \sum \text{col}(pts, 18)$	$I'_{yy} = 815.6 \text{ in}^3$	$I'_{yy} = 1.34 \cdot 10^7 \text{ mm}^3$	Moment of Inertia (Y-Axis)
$I'_{xy} := \sum \text{col}(pts, 19)$	$I'_{xy} = -1.1 \cdot 10^{-12} \text{ in}^3$	$I'_{xy} = -1.80 \cdot 10^{-8} \text{ mm}^3$	Product of Inertia
$I'_p := I'_{xx} + I'_{yy}$	$I'_p = 9944.7 \text{ in}^3$	$I'_p = 1.63 \cdot 10^8 \text{ mm}^3$	Polar Moment of Inertia
$I'_{prod} := I'_{xx} \cdot I'_{yy} - I'_{xy}^2$	$I'_{prod} = 7.4 \cdot 10^6 \text{ in}^6$	$I'_{prod} = 2.00 \cdot 10^{15} \text{ mm}^6$	Product of Inertia

**Load Distance from Centroid:**

$e'_x := e_x - cg_x$	$e'_x = 0.00 \text{ in}$	$e'_x = 0 \text{ mm}$	X-Axis Direction
$e'_y := e_y - cg_y$	$e'_y = 1.50 \cdot 10^{-14} \text{ in}$	$e'_y = 3.8211 \cdot 10^{-13} \text{ mm}$	Y-Axis Direction
$e'_z := e_z$	$e'_z = 0.00 \text{ in}$	$e'_z = 0 \text{ mm}$	Z-Axis Direction

**Stress from Applied Factored Loads:**

$\sigma_{fx} := \frac{V_{fx}}{A}$	$\sigma_{fx} = 0.00 \text{ Kpi}$	$\sigma_{fx} = 0 \text{ kNpmm}$	X-Axis Direction
$\sigma_{fy} := \frac{V_{fy}}{A}$	$\sigma_{fy} = 2.9759 \text{ Kpi}$	$\sigma_{fy} = 0.5212 \text{ kNpmm}$	Y-Axis Direction
$\sigma_{fz} := \frac{P_{fz}}{A}$	$\sigma_{fz} = 0 \text{ Kpi}$	$\sigma_{fz} = 0 \text{ kNpmm}$	Z-Axis Direction

**Load at Weld Group Centroid:**

$d_x := e_x - cg_x$	$d_x = 0.00 \text{ in}$	$d_x = 0.00 \text{ mm}$
$d_y := e_y - cg_y$	$d_y = 1.5044 \cdot 10^{-14} \text{ in}$	$d_y = 3.8211 \cdot 10^{-13} \text{ mm}$
$d_z := e_z$	$d_z = 0 \text{ in}$	$d_z = 0 \text{ mm}$
$M'_{fx} := M_{fx} - V_{fy} \cdot d_z + P_{fz} \cdot d_y$	$M'_{fx} = 593.00 \text{ K\_ft}$	$M'_{fx} = 804 \text{ kN\_m}$
$M'_{fy} := M_{fy} + V_{fx} \cdot d_z - P_{fz} \cdot d_x$	$M'_{fy} = 0 \text{ K\_ft}$	$M'_{fy} = 0 \text{ kN\_m}$
$T'_{fz} := T_{fz} - V_{fx} \cdot d_y + V_{fy} \cdot d_x$	$T'_{fz} = 0 \text{ K\_ft}$	$T'_{fz} = 0 \text{ kN\_m}$

```

for r ∈ [1..rows(pts)]
  if pts_r 10 == 0 in
    pts_r 24 := 0 pli
    pts_r 25 := 0 pli
    pts_r 26 := 0 pli
    pts_r 27 := 0 pli
    pts_r 28 := pts_r 24 + pts_r 25 + pts_r 26 + pts_r 27
    pts_r 29 := pts_r 28 + σfz
    pts_r 30 := 0 pli
    pts_r 31 := pts_r 30 + σfx
    pts_r 32 := 0 pli
    pts_r 33 := pts_r 32 + σfy
    pts_r 34 := √(pts_r 292 + pts_r 312 + pts_r 332)
    pts_r 35 := 0 pli
  else
    pts_r 24 :=  $\frac{pts_{r 21} \cdot M'_{fx} \cdot I'_{yy}}{I'_{prod}}$ 
    pts_r 25 :=  $\frac{pts_{r 21} \cdot M'_{fy} \cdot I'_{xy}}{I'_{prod}}$ 
    pts_r 26 :=  $\frac{(-1 \cdot pts_{r 20}) \cdot M'_{fx} \cdot I'_{xy}}{I'_{prod}}$ 
    pts_r 27 :=  $\frac{(-1 \cdot pts_{r 20}) \cdot M'_{fy} \cdot I'_{xx}}{I'_{prod}}$ 
    pts_r 28 := pts_r 24 + pts_r 25 + pts_r 26 + pts_r 27
    pts_r 29 := pts_r 28 + σfz
    pts_r 30 :=  $\frac{(-1 \cdot pts_{r 21}) \cdot T'_{fz}}{I'_p}$ 
    pts_r 31 := pts_r 30 + σfx
    pts_r 32 :=  $\frac{pts_{r 20} \cdot T'_{fz}}{I'_p}$ 
    pts_r 33 := pts_r 32 + σfy
    pts_r 34 := √((pts_r 29)2 + (pts_r 31)2 + (pts_r 33)2)
    pts_r 35 :=  $\frac{pts_{r 23} \cdot M'_{fx} \cdot I'_{yy}}{I'_{prod}}$ 

```

σ<sub>z</sub> y from M<sub>x</sub> Stress at Start of Segmentσ<sub>z</sub> y from M<sub>y</sub>σ<sub>z</sub> x from M<sub>x</sub>σ<sub>z</sub> x from M<sub>y</sub>Σσ<sub>z</sub> from MΣσ<sub>z</sub>σ<sub>x</sub> from TΣσ<sub>x</sub>σ<sub>y</sub> from TΣσ<sub>y</sub>σ<sub>y</sub> combinedσ<sub>z</sub> y from M<sub>x</sub>σ<sub>z</sub> y from M<sub>y</sub>σ<sub>z</sub> x from M<sub>x</sub>σ<sub>z</sub> x from M<sub>y</sub>Σσ<sub>z</sub> from MΣσ<sub>z</sub>σ<sub>x</sub> from TΣσ<sub>x</sub>σ<sub>y</sub> from TΣσ<sub>y</sub>σ<sub>y</sub> combinedΣσ<sub>y</sub>

Stress at Start of Segment

σ<sub>z</sub> y from M<sub>x</sub>

Stress at End of Segment

```
for r ∈ [1..rows(pts)]
```

```
  if ptsr 10 = 0 in
```

```
    ptsr 36 := 0 pli
```

```
    ptsr 37 := 0 pli
```

```
    ptsr 38 := 0 pli
```

```
    ptsr 39 := ptsr 35 + ptsr 36 + ptsr 37 + ptsr 38
```

```
    ptsr 40 := (ptsr 39 + σfz)
```

```
    ptsr 41 := 0 pli
```

```
    ptsr 42 := ptsr 41 + σfx
```

```
    ptsr 43 := 0 pli
```

```
    ptsr 44 := ptsr 43 + σfy
```

```
    ptsr 45 := √((ptsr 40)2 + (ptsr 42)2 + (ptsr 44)2)
```

```
    ptsr 46 := 0 pli
```

```
    ptsr 47 := 0 pli
```

```
    ptsr 48 := 0 pli
```

```
  else
```

```
    ptsr 36 :=  $\frac{pts_{r 23} \cdot M'_{fy} \cdot I'_{xy}}{I'_{prod}}$ 
```

```
    ptsr 37 :=  $\frac{(-1 \cdot pts_{r 22}) \cdot M'_{fx} \cdot I'_{xy}}{I'_{prod}}$ 
```

```
    ptsr 38 :=  $\frac{(-1 \cdot pts_{r 22}) \cdot M'_{fy} \cdot I'_{xx}}{I'_{prod}}$ 
```

```
    ptsr 39 := ptsr 35 + ptsr 36 + ptsr 37 + ptsr 38
```

```
    ptsr 40 := (ptsr 39 + σfz)
```

```
    ptsr 41 :=  $\left( - \frac{1 \cdot pts_{r 23} \cdot T'_{fz}}{I'_p} \right)$ 
```

```
    ptsr 42 := ptsr 41 + σfx
```

```
    ptsr 43 :=  $\frac{pts_{r 22} \cdot T'_{fz}}{I'_p}$ 
```

```
    ptsr 44 := ptsr 43 + σfy
```

```
    ptsr 45 := √((ptsr 40)2 + (ptsr 42)2 + (ptsr 44)2)
```

```
    ptsr 46 :=  $\frac{pts_{r 16} \cdot M'_{fx} \cdot I'_{yy}}{I'_{prod}}$ 
```

```
    ptsr 47 :=  $\frac{pts_{r 16} \cdot M'_{fy} \cdot I'_{xy}}{I'_{prod}}$ 
```

```
    ptsr 48 :=  $\frac{(-1 \cdot pts_{r 15} \cdot M'_{fx} \cdot I'_{xy})}{I'_{prod}}$ 
```

σz y from My

σz x from Mx

σz x from My

Σσz from M

Σσz

σx from T

Σσx

σy from T

Σσy

σy combined

σz y from Mx

σz y from My

σz x from Mx

σz y from My

σz x from Mx

σz x from My

Σσz from M

Σσz

σx from T

Σσx

σy from T

Σσy

σy combined

Stress at End of Segment

σz y from Mx

Stress at Midpoint of Segment

σz y from My

```

for r ∈ [1..rows(pts)]
  if pts_r 10 = 0 in
    pts_r 49 := 0 pli
    pts_r 50 := pts_r 46 + pts_r 47 + pts_r 48 + pts_r 49
    pts_r 51 := pts_r 50 + σfz
    pts_r 52 := 0 pli
    pts_r 53 := pts_r 52 · σfx
    pts_r 54 := 0 pli
    pts_r 55 := pts_r 54 + σfy
    pts_r 56 := √((pts_r 51)2 + (pts_r 53)2 + (pts_r 55)2)
  else
    pts_r 49 :=  $\frac{(-1 \cdot pts_r 15) \cdot M'_{fy} \cdot I'_{xx}}{I'_{prod}}$ 
    pts_r 50 := pts_r 46 + pts_r 47 + pts_r 48 + pts_r 49
    pts_r 51 := pts_r 50 + σfz
    pts_r 52 :=  $\frac{(-1 \cdot pts_r 16) \cdot T'_{fz}}{I'_p}$ 
    pts_r 53 := (pts_r 52 + σfx)
    pts_r 54 :=  $\frac{pts_r 15 \cdot T'_{fz}}{I'_p}$ 
    pts_r 55 := pts_r 54 + σfy
    pts_r 56 := √((pts_r 51)2 + (pts_r 53)2 + (pts_r 55)2)

```

σ<sub>z</sub> x from M<sub>x</sub>σ<sub>z</sub> x from M<sub>y</sub>σ<sub>z</sub> frin Mσ<sub>z</sub> Totalσ<sub>x</sub> from Tσ<sub>x</sub> Combinedσ<sub>y</sub> from Tσ<sub>y</sub> Combined

Total σ

σ<sub>z</sub> x from M<sub>y</sub>σ<sub>z</sub> frin Mσ<sub>z</sub> Totalσ<sub>x</sub> from Tσ<sub>x</sub> Combinedσ<sub>y</sub> from Tσ<sub>y</sub> Combined

Total σ

Stress at Midpoint of Segment

**Max and Min Stress in Segment:**

$\sigma'_z := \max(\text{col}(\text{pts}, 34))$	$\sigma'_z = 9.84 \text{ Kpi}$	$\sigma'_z = 1.72 \text{ kNpmm}$	Max Stress at Start of Segment
$op'_1 := \min(\text{col}(\text{pts}, 34))$	$op'_1 = 9 \text{ Kpi}$	$op'_1 = 2 \text{ kNpmm}$	Min Stress at Start of Segment
$\sigma'_x := \max(\text{col}(\text{pts}, 45))$	$\sigma'_x = 9.84 \text{ Kpi}$	$\sigma'_x = 1.72 \text{ kNpmm}$	Max Stress at End of Segment
$op'_2 := \min(\text{col}(\text{pts}, 45))$	$op'_2 = 9.2826 \text{ Kpi}$	$op'_2 = 1.6256 \text{ kNpmm}$	Min Stress at End of Segment
$\sigma'_y := \max(\text{col}(\text{pts}, 56))$	$\sigma'_y = 9.84 \text{ Kpi}$	$\sigma'_y = 1.72 \text{ kNpmm}$	Max Stress at Middle of Segment
$op'_3 := \min(\text{col}(\text{pts}, 56))$	$op'_3 = 2.9759 \text{ Kpi}$	$op'_3 = 0.5212 \text{ kNpmm}$	Min Stress at Middle of Segment

**Max and Min Stress in Welds:**

$op_{max} := \max\left(\left[\begin{array}{ccc} \sigma'_x & \sigma'_y & \sigma'_z \end{array}\right]\right)$	$op_{max} = 9.84 \text{ Kpi}$	$op_{max} = 1.72 \text{ kNpmm}$	Maximum Stress in Segment
$op'_{min} := \min\left(\left[\begin{array}{ccc} op'_1 & op'_2 & op'_3 \end{array}\right]\right)$	$op'_{min} = 2.9759 \text{ Kpi}$	$op'_{min} = 0.5212 \text{ kNpmm}$	Minimum Stress in Segment
$v_r = 11.11 \text{ Kpi}$	$v_r = 1.9456 \text{ kNpmm}$		Weld Resistance:



**Summary:****Material Property Factors**

Rolled Sections	$\phi_s = 0.9$
Weld	$\phi_w = 0.67$
Dead Load Factor	$\alpha_D = 1.25$
Live Load Factor	$\alpha_L = 1.5$

Check  $(\alpha_D \geq 1.25) = "...OK"$

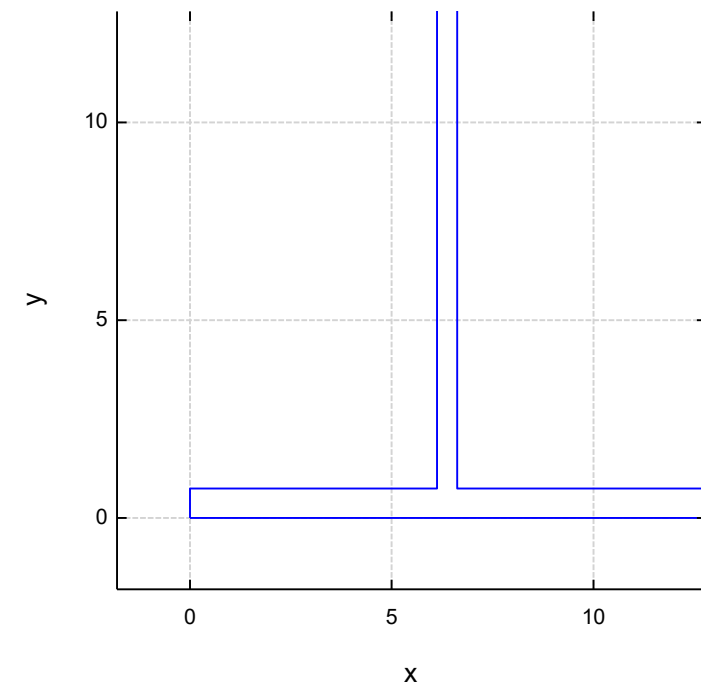
Check  $(\alpha_L \geq 1.5) = "...OK"$

**Applied Factored Loads:**

Axial Load	$P_{fz} = 0 \text{ K}$	$P_{fz} = 0 \text{ kN}$
Shear (X-Axis)	$V_{fx} = 0 \text{ K}$	$V_{fx} = 0 \text{ kN}$
Shear (Y-Axis)	$V_{fy} = 292 \text{ K}$	$V_{fy} = 1298.8807 \text{ kN}$
Moment (X-Axis)	$M_{fx} = 593 \text{ K\_ft}$	$M_{fx} = 804 \text{ kN\_m}$
Moment (Y-Axis)	$M_{fy} = 0 \text{ K\_ft}$	$M_{fy} = 0 \text{ kN\_m}$
Torsion (Z-Axis)	$T_{fz} = 0 \text{ K\_ft}$	$T_{fz} = 0 \text{ kN\_m}$

**Load Eccentricity from Origin:**

X-Axis Direction	$e_x = 6.4 \text{ in}$	$e_x = 161.9 \text{ mm}$
Y-Axis Direction	$e_y = 12 \text{ in}$	$e_y = 305.6 \text{ mm}$
Z-Axis Direction	$e_z = 0 \text{ in}$	$e_z = 0 \text{ mm}$

**Weld Pattern****Segment Input Data:**

Row Represents Segment Number  
Columns represent S(xi, yi, xj, yj)  
coordinates

$pts' =$	0.0	0.0	0.0	0.8
	0.0	0.8	6.1	0.8
	6.1	0.8	6.1	23.3
	6.1	23.3	0.0	23.3
	0.0	23.3	0.0	24.1
	0.0	24.1	12.8	24.1
	12.8	24.1	12.8	23.3
	12.8	23.3	6.6	23.3
	6.6	23.3	6.6	0.8
	6.6	0.8	12.8	0.8
	12.8	0.8	12.8	0.0
	12.8	0.0	0.0	0.0
	0	0	0	19
$pts' =$	0	19	155.6	19
	155.6	19	155.6	592.1
	155.6	592.1	0	592.1
	0	592.1	0	611.1
	0	611.1	323.8	611.1
	323.8	611.1	323.8	592.1
	323.8	592.1	168.3	592.1
	168.3	592.1	168.3	19
	168.3	19	323.8	19
	323.8	19	323.8	0
	323.8	0	0	0
	0	0	0	0
	0	0	0	0

**Steel Base Properties**

Designation	$desI_1 = \text{"A36"}$	
Yield Strength	$f_{y1} = 36 \text{ Ksi}$	$f_{y1} = 248 \text{ MPa}$
Ultimate Strength	$F_{u1} = 58 \text{ Ksi}$	$F_{u1} = 400 \text{ MPa}$
Young's Modulus	$E_s = 29000 \text{ Ksi}$	$E_s = 1.9995 \cdot 10^5 \text{ MPa}$
Shear Modulus	$G_s = 10.9 \text{ Ksi}$	$G_s = 75 \text{ MPa}$
Density	$\gamma_s = 489 \text{ pcf}$	$\gamma_s = 76.8158 \text{ kNpcm}$

**Welding Electrodes**

Imperial Designation	$desI_w = \text{"E70xx"}$	
Metric Designation	$desM_w = \text{"E480xx"}$	
Ultimate Strength	$X_u = 70 \text{ ksi}$	$X_u = 483 \text{ MPa}$

**Weld Size**

Imperial Designation	$desI_D = \text{"1/2"}$	
Metric Designation	$desM_D = \text{" "}$	
Size	$D = 0.5 \text{ in}$	$D = 12.7 \text{ mm}$
Limit Weld Stress	$v_{rw} = 31.4 \text{ ksi}$	$v_{rw} = 216.7 \text{ MPa}$
Limit Base Metal Stress	$v_{rb} = 32.4 \text{ Ksi}$	$v_{rb} = 223.4 \text{ MPa}$
Weld Resist per Unit Len	$v'_{rw} = 11.1 \text{ Kpi}$	$v'_{rw} = 1.9 \text{ kNpmm}$
Base Resist per Unit Len	$v'_{rb} = 16.2 \text{ Kpi}$	$v'_{rb} = 2.8 \text{ kNpmm}$
Min Resistance per Unit Len	$v_r = 11.1 \text{ Kpi}$	$v_r = 1.9 \text{ kNpmm}$

**Weld Properties**

Total Length of Weld	$A = 98.12 \text{ in}$	$A = 2492.2 \text{ mm}$
Centroid of Weld X-Axis	$cg_x = 6.375 \text{ in}$	$cg_x = 161.9 \text{ mm}$
Centroid of Weld Y-Axis	$cg_y = 12.03 \text{ in}$	$cg_y = 305.6 \text{ mm}$
Moment of Inertia (X-Axis)	$I'_{xx} = 9129 \text{ in}^3$	$I'_{xx} = 1.50 \cdot 10^8 \text{ mm}^3$
Moment of Inertia (Y-Axis)	$I'_{yy} = 815.6 \text{ in}^3$	$I'_{yy} = 1.34 \cdot 10^7 \text{ mm}^3$
Product of Inertia	$I'_{xy} = -1.1 \cdot 10^{-12} \text{ in}^3$	$I'_{xy} = -1.80 \cdot 10^{-8} \text{ mm}^3$
Polar Moment of Inertia	$I'_p = 9944.7 \text{ in}^3$	$I'_p = 1.63 \cdot 10^8 \text{ mm}^3$
Prod of Moment of Inertia	$I'_{prod} = 7.4 \cdot 10^6 \text{ in}^6$	$I'_{prod} = 2.00 \cdot 10^{15} \text{ mm}^6$

**Weld Force from Direct Loads**

X-Axis Direction	$\sigma_{fx} = 0.00 \text{ Kpi}$	$\sigma_{fx} = 0.00 \text{ kNpmm}$
Y-Axis Direction	$\sigma_{fy} = 2.98 \text{ Kpi}$	$\sigma_{fy} = 0.52 \text{ kNpmm}$
Z-Axis Direction	$\sigma_{fz} = 0.00 \text{ Kpi}$	$\sigma_{fz} = 0.00 \text{ kNpmm}$

**Load at Weld Group Centroid:**

Moment (X-Axis)	$M'_{fx} = 593 \text{ K\_ft}$	$M'_{fx} = 804 \text{ kN\_m}$
Moment (Y-Axis)	$M'_{fy} = 0 \text{ K\_ft}$	$M'_{fy} = 0 \text{ kN\_m}$
Torsion (Z-Axis)	$T'_{fz} = 0 \text{ K\_ft}$	$T'_{fz} = 0 \text{ kN\_m}$
Max Weld Force at Start of Segment in Pattern	$\sigma'_x = 9.838 \text{ Kpi}$	$\sigma'_x = 1.72 \text{ kNpmm}$

Min Weld Force at Start of Segment in Pattern	$op'_1 = 9.283 \text{ Kpi}$	$op'_1 = 2 \text{ kNpmm}$
Max Weld Force at End of Segment in Pattern	$\sigma'_y = 9.838 \text{ Kpi}$	$\sigma'_y = 1.72 \text{ kNpmm}$
Min Weld Force at End of Segment in Pattern	$op'_2 = 9.283 \text{ Kpi}$	$op'_2 = 1.63 \text{ kNpmm}$
Max Weld Force at Mid Point of Segment in Pattern	$\sigma'_z = 9.838 \text{ Kpi}$	$\sigma'_z = 1.72 \text{ kNpmm}$
Min Weld Force at Mid Point of Segment in Pattern	$op'_3 = 2.976 \text{ Kpi}$	$op'_3 = 0.52 \text{ kNpmm}$
Maximum Weld Force in Pattern	$op_{max} = 9.838 \text{ Kpi}$	$op_{max} = 1.72 \text{ kNpmm}$
Minimum Weld Force in Pattern	$op'_{min} = 2.976 \text{ Kpi}$	$op'_{min} = 0.52 \text{ kNpmm}$
Weld Resistance:	$v_r = 11.110 \text{ Kpi}$	$v_r = 1.95 \text{ kNpmm}$

Check  $(v_r \geq op_{max}) = "...OK"$

Check  $(v_r \geq 0.95 \cdot op_{max}) = "...OK"$

Check  $(v_r \geq |op'_{min}|) = "...OK"$