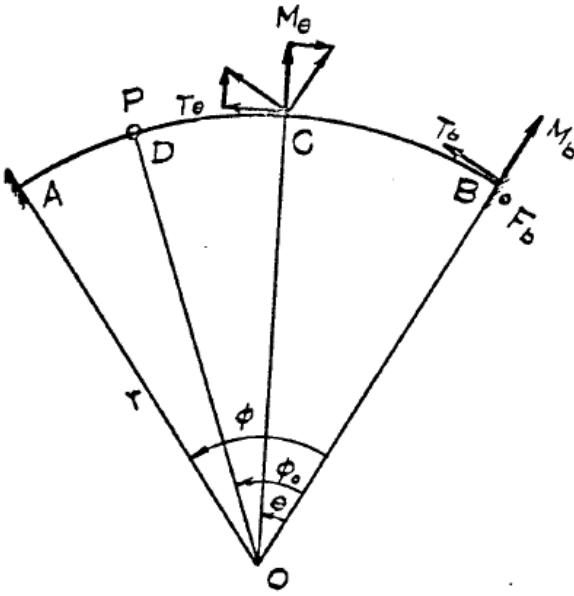


1) Horizontally curved beam fixed at both ends and subjected to concentrated load



As shown in Figure, a concentrated load acts at the point D with an angular distance Φ from support B. M_θ and T_θ represent the bending moment and torsional moment at any section C with an angular distance θ from B.

For portion BD ($0 \leq \theta \leq \Phi_0$)

$$M_\theta = M_b \cos \theta + T_b \sin \theta - F_b r \sin \theta \quad (1)$$

$$T_\theta = -M_b \sin \theta + T_b \cos \theta + F_b r \quad (2)$$

For portion DA ($\Phi_0 \leq \theta \leq \Phi$)

$$M_\theta = M_b \cos \theta + T_b \sin \theta - F_b r \sin \theta + P r \sin(\theta - \Phi_0) \quad (3)$$

$$T_\theta = -M_b \sin \theta + T_b \cos \theta + F_b r \quad (4)$$

Applying Castigiano's theorem with U representing the strain energy

$$U = \int \frac{M_\theta^2}{2EI} rd\theta + \int \frac{T_\theta^2}{2GJ} rd\theta \quad (5)$$

At support B

$$U_b \neq 0 \quad Y_b = \Delta_b = 0$$

$$\frac{\partial U}{\partial M_b} \neq 0 \quad \frac{\partial U}{\partial T_b} = \frac{\partial U}{\partial F_b} = 0 \quad (6)$$

From (5) and (6)

$$\frac{\partial U}{\partial M_b} = \frac{1}{EI} \int \frac{M_\theta \cdot M_\theta}{M_b} r d\theta + \frac{1}{GJ} \int \frac{T_\theta \cdot T_\theta}{M_b} r d\theta = 0 \quad (7)$$

Partially differentiating (1) and (2) by M_b

$$\frac{\partial M_\theta}{\partial M_b} = \cos \theta, \quad \frac{\partial T_\theta}{\partial M_b} = -\sin \theta$$

Let

$$m = \frac{EI}{GJ}$$

Applying above results to (7)

$$\frac{1}{EI} \left[\int M_\theta r \cos \theta d\theta + m \int T_\theta r (-\sin \theta) d\theta \right] = 0 \quad (8)$$

Applying from (1), (2), (3) and (4)

$$\frac{r}{EI} \dot{\varphi}$$

$$\frac{r}{EI} \dot{\varphi} = 0$$

$$\frac{r}{EI} \left[M_b \left(\frac{\varphi}{2} + \frac{\sin 2\varphi}{4} + m \frac{\varphi}{2} - m \frac{\sin 2\varphi}{4} \right) + T_b \left(\frac{-1}{4} (\cos(2\varphi - 1)) + \frac{m}{4} (\cos(2\varphi - 1)) \right) + F_b r \left(\frac{(1-m)}{4} \right. \right.$$

$$\left. \left. M_b [\varphi(m+1) - \sin \varphi \cos \varphi (m-1)] - T_b \sin^2 \varphi (m-1) + F_b r [\sin^2 \varphi (m-1) + 2m(\cos \varphi - 1)] \right) = Pr \right] \quad (9)$$

Similarly, for $\frac{\partial U}{\partial T_b} = 0$ we can obtain

$$-M_b [\sin^2 \varphi (m-1)] + T_b [\varphi(m+1) + \sin \varphi \cos \varphi (m-1)] + F_b r [2m \sin \varphi - \varphi(m+1) - \sin \varphi \cos \varphi] = Pr \quad (10)$$

Similarly, for $\frac{\partial U}{\partial F_b} = 0$ we can obtain

$$M_b[\sin^2 \theta_0(m-1) + 2m(\cos \theta - 1)] + T_b[2m \sin \theta - \theta(m+1) - \sin \theta \cos \theta (m-1)] + F_b r[\theta(m-1) - \theta_0(m+1)] = 0 \quad (11)$$

Let

$$a_1 = \theta(m+1) - \sin \theta \cos \theta (m-1) \quad (12)$$

$$b_1 = \sin^2 \theta (m-1) \quad (13)$$

$$c_1 = \sin^2 \theta (m-1) + 2m(\cos \theta - 1) \quad (14)$$

$$d_1 = (m-1) \cos \theta_0 (\sin^2 \theta - \sin^2 \theta_0) + \sin \theta_0 (\theta - \theta_0)(m+1) - \sin \theta_0 \frac{(m-1)}{2} (\sin 2\theta - \sin 2\theta_0) \quad (15)$$

$$a_2 = b_1 \quad (16)$$

$$b_2 = \theta(m+1) + \sin \theta \cos \theta (m-1) \quad (17)$$

$$c_2 = 2m \sin \theta - \theta(m+1) - \sin \theta \cos \theta (m-1) \quad (18)$$

$$d_2 = -\cos \theta_0 (\theta - \theta_0)(m+1) - \frac{1}{2} \cos \theta_0 (m-1) (\sin 2\theta - \sin 2\theta_0) - (m-1) \sin \theta_0 (\sin^2 \theta - \sin^2 \theta_0) \quad (19)$$

$$a_3 = c_1 \quad (20)$$

$$b_3 = c_2 \quad (21)$$

$$c_3 = \theta(m+1) + \sin \theta \cos \theta (m-1) - 4m \sin \theta + 2m \theta \quad (22)$$

$$d_3 = \left[\frac{(m-1)}{2} \cos \theta_0 (\sin 2\theta - \sin 2\theta_0) + (\theta - \theta_0)(\cos \theta_0 (m+1) + 2m) + (m-1) \sin \theta_0 (\sin^2 \theta - \sin^2 \theta_0) \right] \quad (23)$$

Then the equations can be simplified into following simultaneous equations

$$a_1 M_b - b_1 T_b + c_1 F_b r = d_1 Pr \quad (24)$$

$$-b_1 M_b + b_2 T_b + c_2 F_b r = d_2 Pr \quad (25)$$

$$c_1 M_b + c_2 T_b + c_3 F_b r = d_3 Pr \quad (26)$$

Just need to solve above two simultaneous equations now.

Placing above equation system in matrix form and carrying out operations for matrices the following result can be obtained.

$$|A| = \begin{vmatrix} a_1 & -b_1 & c_1 \\ -b_1 & b_2 & c_2 \\ c_1 & c_2 & c_3 \end{vmatrix}$$

$$M_b = \frac{Pr}{|A|} \begin{vmatrix} d_1 & -b_1 & c_1 \\ d_2 & b_2 & c_2 \\ d_3 & c_2 & c_3 \end{vmatrix} \quad (27)$$

$$T_b = \frac{Pr}{|A|} \begin{vmatrix} a_1 & d_1 & c_1 \\ -b_1 & d_2 & c_2 \\ c_1 & d_3 & c_3 \end{vmatrix} \quad (28)$$

$$F_b = \frac{P}{|A|} \begin{vmatrix} a_1 & -b_1 & d_1 \\ -b_1 & b_2 & d_2 \\ c_1 & c_2 & d_3 \end{vmatrix} \quad (29)$$