

Finite Element Floating Roof Structure Calculation for Light Oil Tanks (TK-2050 A~D)

Rev	Status	Prepared	Checked	Approved	Date

Tabulation of Revised Pages

REV PAGE	REV				REV PAGE	REV				REV PAGE	REV			
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12	X	X	X		54		X	X						
13	X	X			55			X						
14	X	X			56			X						
15	X	X	X		57			X						
16		X			58			X						
17		X			59			X						
18		X	X		60			X						
19		X	X		61			X						
20		X	X		62			X						
21		X	X		63			X						
22		X	X		64			X						
23		X	X		65			X						
24		X	X		66			X						
25		X	X		67			X						
26		X	X		68			X						
27		X	X		69			X						
28		X	X		70			X						
29		X	X		71			X						
30		X	X		72			X						
31		X	X		73			X						
32		X	X		74			X						
33		X	X											
34		X	X											
35		X	X											
36		X	X											
37		X	X											
38		X	X											
39		X	X											
40		X	X											
41		X	X											
42		X	X											

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All Changes are marked by a revision mark and are underlined, **Bolded**, and *italicized*

Revision 0 → ***Revision 1*** 

1. Scope

In this document, mechanical strength of the floating roof structure is analyzed for the following cases using SAP2000:

- Maintenance case (Roof is seated on the bottom of the vessel)
- Floating case (Roof is seated on fluid)

2. Reference Documents

	Document No.	Document Title
1	A238-PV-00-DWG-251	General Arrangement Drawing for TK-2050
2	A238-PV-00-CSH-201	Mechanical Calculation Sheet for Light Oil Storage Tanks (TK-2050 A~D)
3	A238-PV-00-CSH-209	Buoyancy and Floating Structure Calculation for Light Oil Storage Tanks (TK-2050 A~D)

3. Applicable Codes and Standards

- API 650 - 2018 Edition

4. Design Data

4.1. Tank Description

Location	Asaluyeh
Service	Light Oil Storage
Tag	TK-2050 A~D
Roof Type	Internal Floating - Single Deck
Structure Position	Internal

4.2. Geometry

The floating roof type is selected ring pontoon roof with central deck. The pontoon roof is divided to watertight compartments. Within the ring pontoon some beams is welded for stiffening. The deck plate has been stiffened also by welded beams. The roof design criteria and calculation is based on API-650, App. "H". General view of the floating roof is shown in following figure :

Inside Diameter of Tank	ID = 27500 mm
Shell Height	H_SH = 19700 mm
Rim Gap	G_R = 200 mm

Maximum Pontoon Height	H_P1 = 900 mm
Minimum Pontoon Height	H_P2 = 700 mm
Pontoon Width	W_P = 3950 mm
Inside Radius of Inner Rim	R_IR = 9600 mm
Outside Radius of Outer Rim	R_OR = 13550 mm
Corrosion Allowance of wetted surface	CA = 1.5 mm
Pontoon Top Plate Thickness	THK_PTP = 5 mm
Pontoon Bottom Plate Thickness	THK_PBP = 7 mm
Pontoon Inner Rim Plate Thickness	THK_PIR = 20 mm
Pontoon Outer Rim Plate Thickness	THK_POR = 7 mm
Pontoon Compartment Plate Thickness	THK_PCP = 5 mm

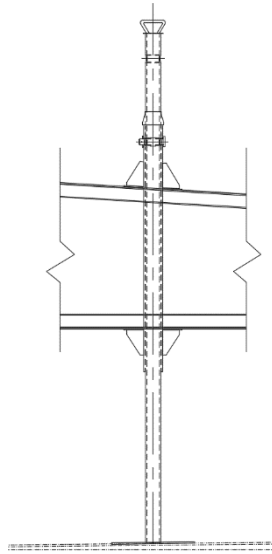


Figure 1: Floating Roof Support at Pontoons
 Table 1: Number of Supports and Their Location

Leg Row	Nos.	Radius mm
1 st	3	2000
2 nd	6	5000
3 rd	9	8000
4 th	12	11000
5 th	12	13250

4.3. Materials

Floating Roof Plate Material	Mat_R = SA-283 C
Roof Plate Density	$\rho_R = 7861$ kg/m ³
Minimum Yield Stress of Roof Plate @ T_d (85°C)	Fy_R = 2.109E+07 kg/m ²
Roof Structure Material	Mat_SR = SA-36 / ST37
Minimum Yield Stress of Roof Structure @ T_d (85°C)	Fy_SR = 2.531E+07 kg/m ²

4.4. Design Conditions

Design External Pressure	Pe_d = 0.24 kPa
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5. Design Considerations

5.1. Load Case Calculation

Following load cases are considered in the roof structure strength calculations based on API-650-Annex H:

5.1.1. Dead Loads

Roof plates has been modeled, and 10% of roof plates weight is considered as dead loads of attachments and distributed on central deck and peripheral pontoons.

5.1.2. Live Loads

Live load on the roof is as follows:

Live Load on the Roof	Lf1 = 0.24 kPa
Point Load of at least Two Men	Lf2 = 22 kN per point

5.1.3. Buoyancy Loads

In this analysis buoyancy loads are calculated using the liquid level height over the parts and applied to the model as hydrostatic pressures.

Standard acceleration of Gravity	= g = 9.8 m/s ²
Liquid Level Over Pontoon Bottom - Intact	(From buoyancy Calculation) = Hp = 0.274 m
Liquid Level Over Deck Bottom - Intact	(From buoyancy Calculation) = Hd = 0.127 m
Liquid Level Over Pontoon Bottom - Punctured	(From buoyancy Calculation) = Hp_pun = 0.403 m
Density of the Product	(From buoyancy Calculation) = $\rho = 700$ kg/m ³
Hydrostatic Pressure on Pontoon - Intact	= $\rho * g * Hp = Pp = 1880$ N/m ²
Hydrostatic Pressure on Deck - Intact	= $\rho * g * Hd = Pd = 871$ N/m ²
Hydrostatic Pressure on Pontoon - Punctured	= $\rho * g * Hp_pun = Pp_pun = 2765$ N/m ²
Hydrostatic Pressure on Deck - Punctured	= Pd_pun = 0 N/m ²

6. SAP Model

6.1. Geometry

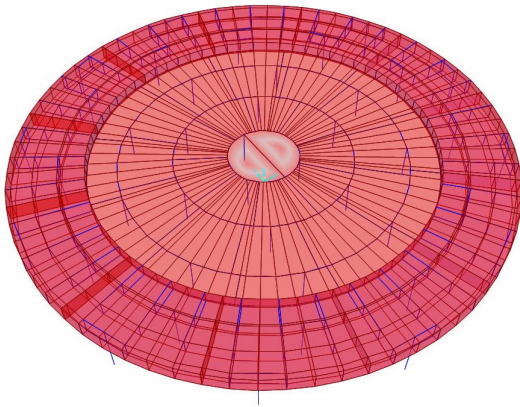


Figure 2: Floating Roof Geometry

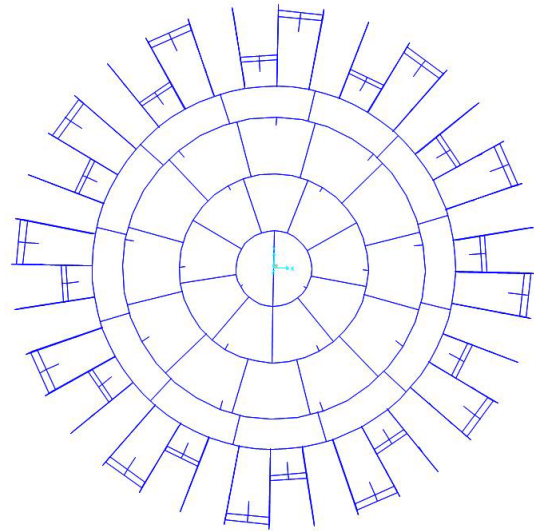


Figure 3: Frames Overview

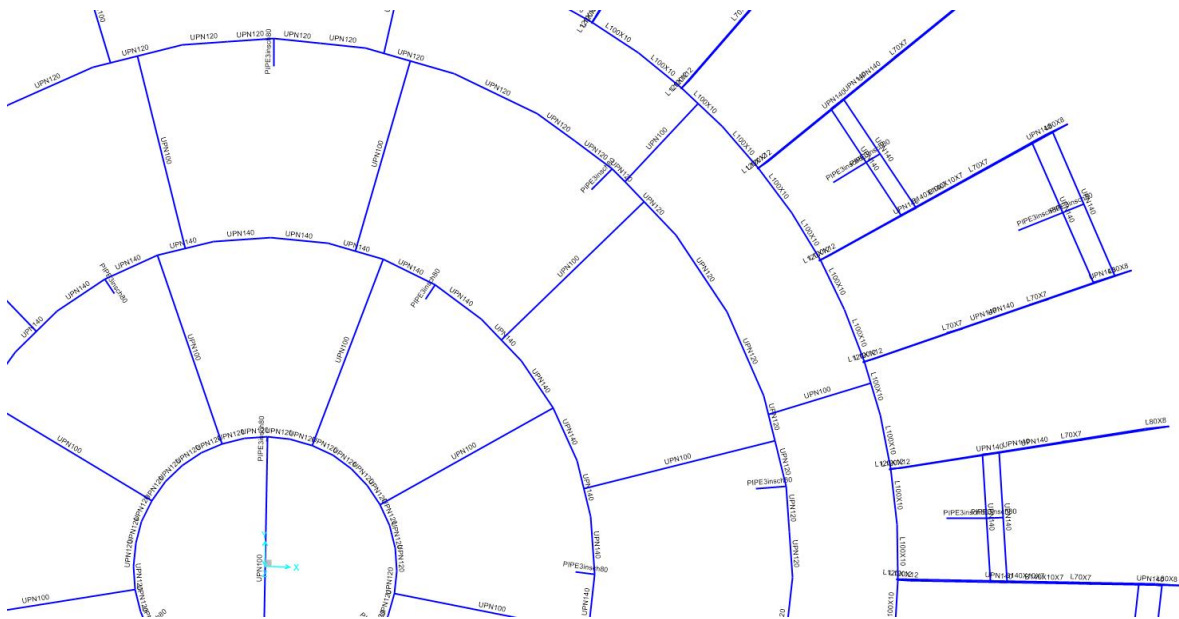
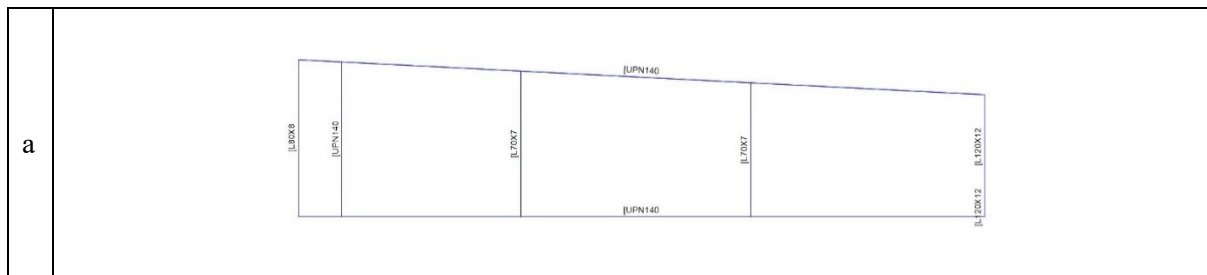


Figure 4: Deck Frame Plan



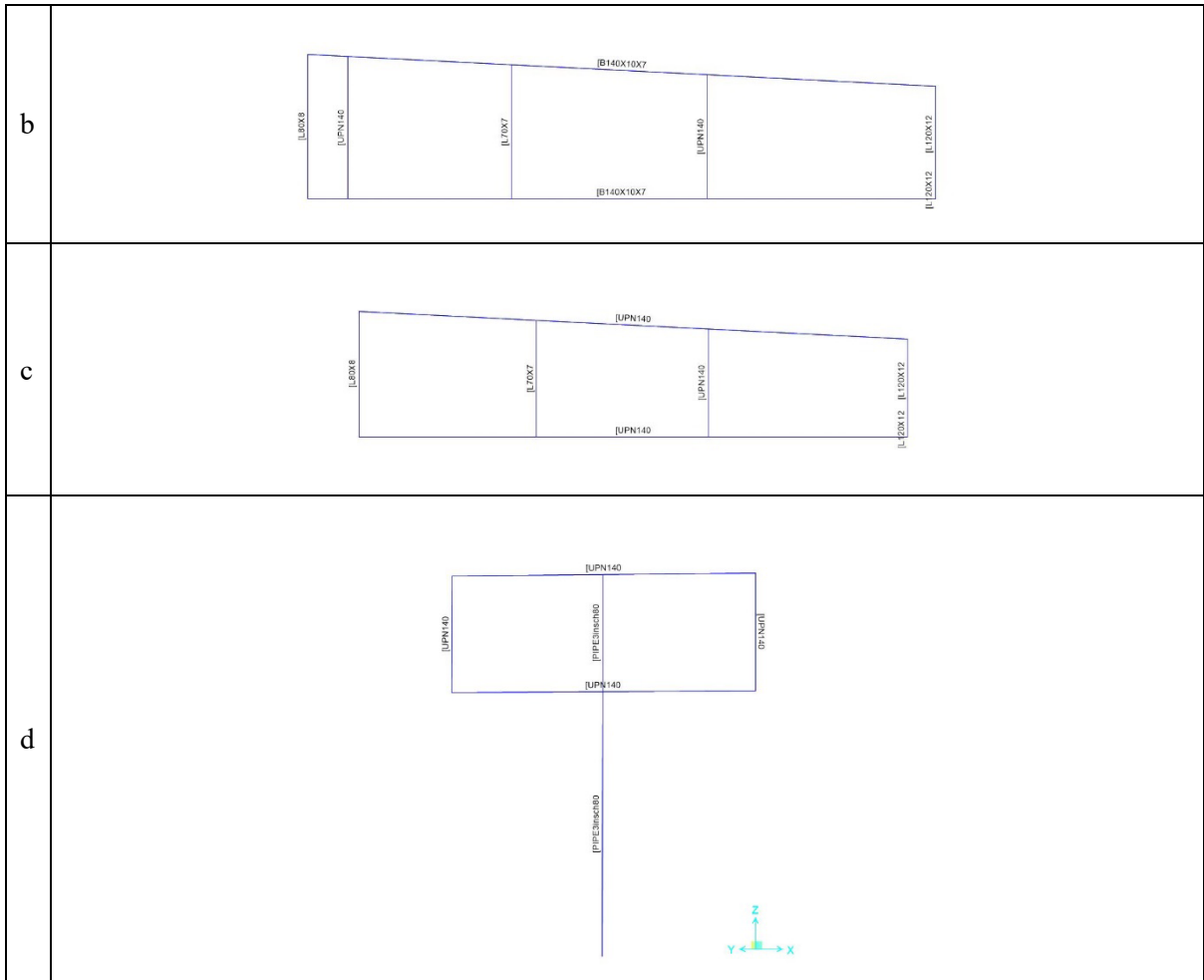


Figure 5: Pontoon Frames a) Type1 b) Type2 c) Type3 d) Support to Pontoon Attachment

Table 2: Profile Section Properties

Section Name	Material	Shape	t3	t2	tf	tw
Text	Text	Text	mm	mm	mm	mm
B140X10X7	A36	Box/Tube	140	140	10	7
L100X10	A36	Angle	100	100	10	10
L120X12	A36	Angle	120	120	12	12
L70X7	A36	Angle	70	70	7	7
L80X8	A36	Angle	80	80	8	8
PIPE-3in-sch80	A53GrB	Pipe	88.9			7.62
UPN100	A36	Channel	100	50	8.5	6
UPN140	A36	Channel	140	60	10	7
<u>DELETD</u>						

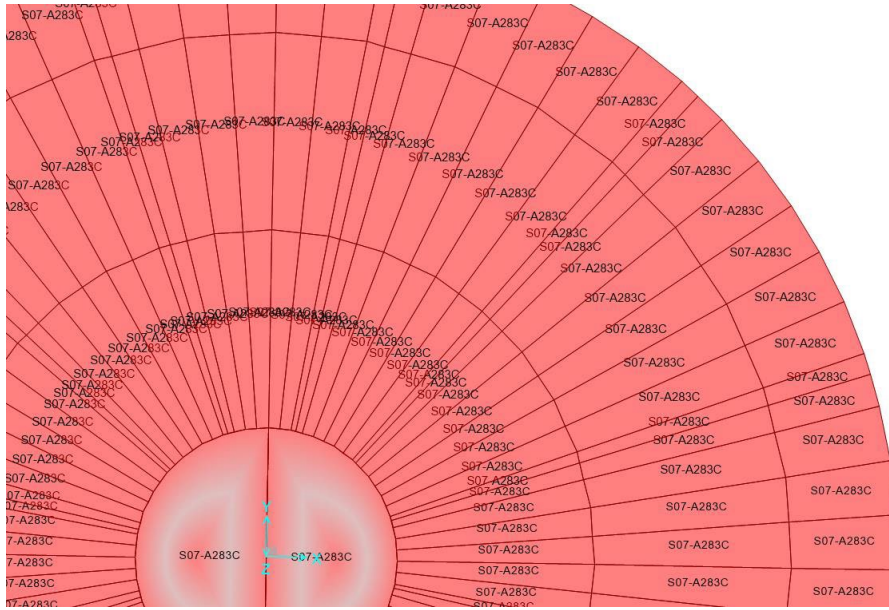


Figure 6: Deck Plate Plan

a	20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C		
	20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C	S20-A283C		
b	A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C
	A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C	S07-A283C

Z
↑

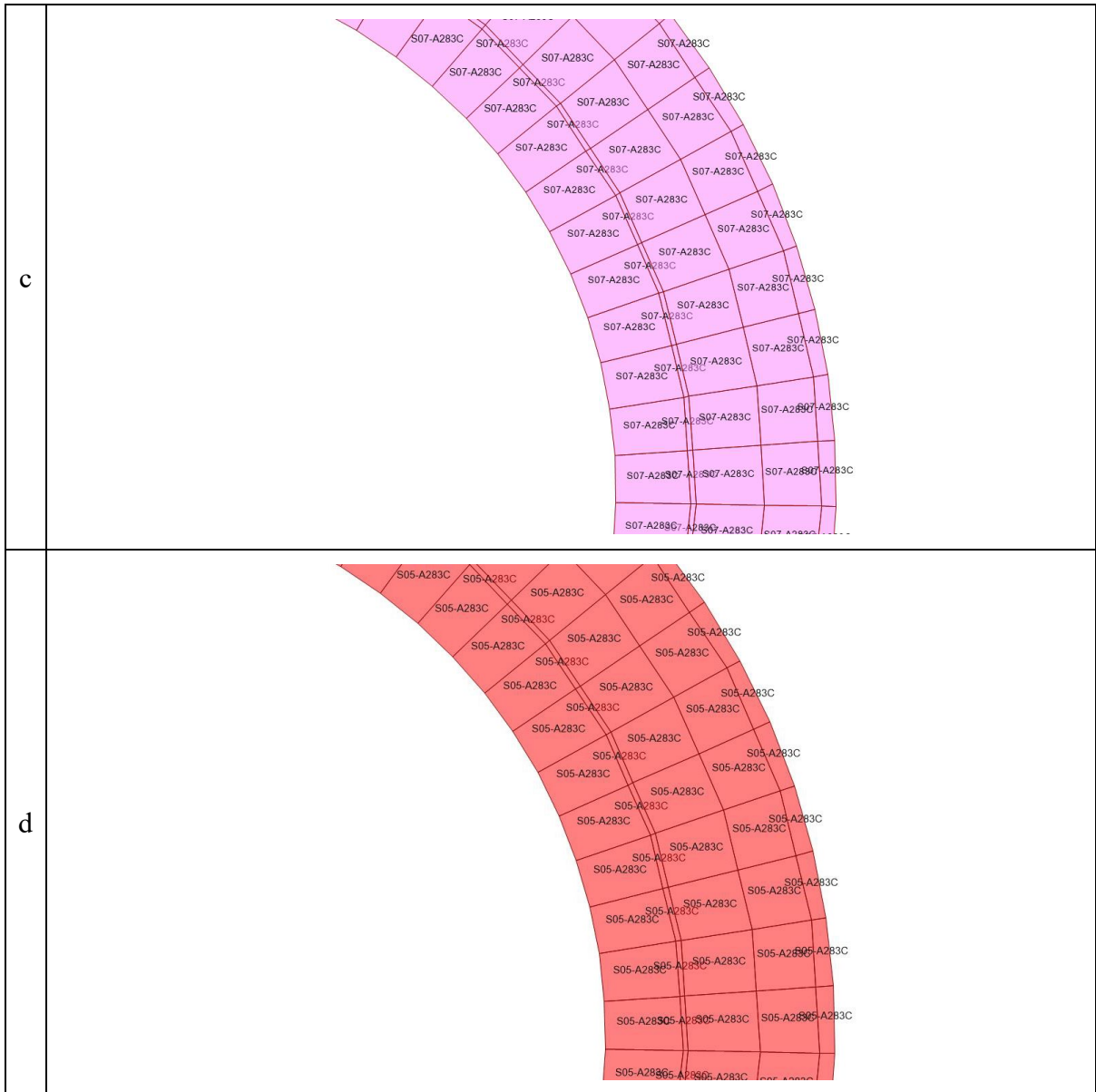


Figure 7: Pontoon Plate a) Inner Rim b) Outer Rim c) Bottom Plate d) Top Plate

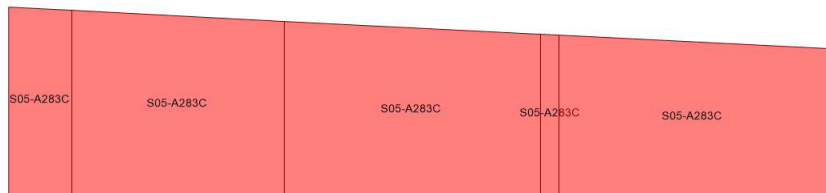


Figure 8: Compartment Plates

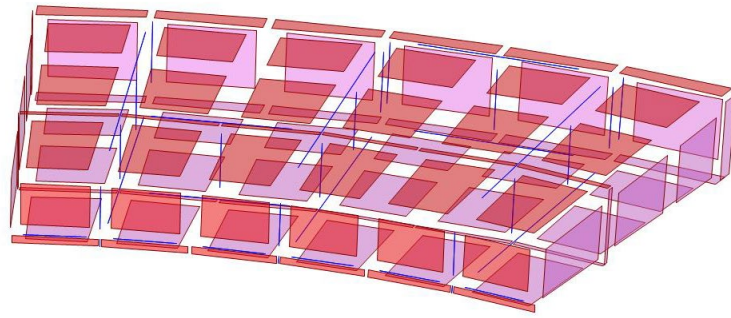


Figure 9: Exploded Parts of a Pontoon Compartment

Table 3: Properties of Plates

Section	Material	Area Type	Thickness	Bend Thick
Text	Text	Text	mm	mm
S05-A283	A283C	Shell	5	5
S07-A283C	A283C	Shell	7	7
S20-A283C	A283C	Shell	20	20

6.2. Boundary Conditions

Boundary conditions of roof structure are as follows:

6.2.1. Maintenance Case

Table 4: Roof Structure Boundary Conditions

Part	Considered?	Boundary Condition
Leg	Yes	Simply supported at the tank bottom

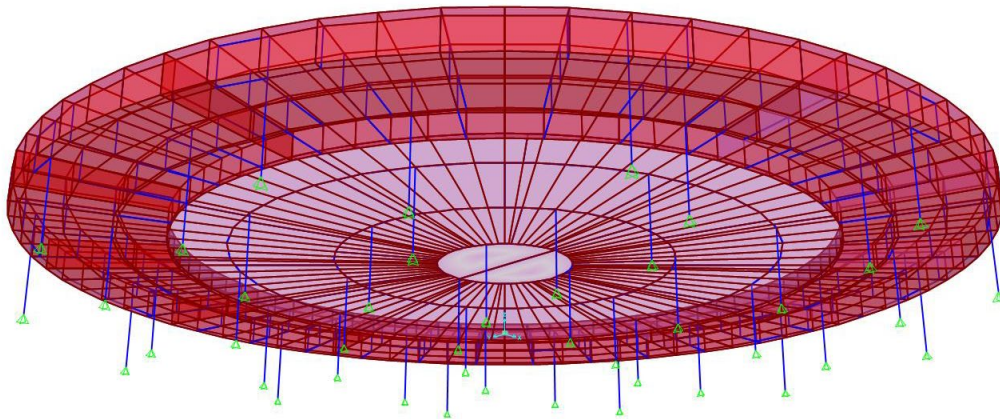


Figure 10: Roof Structure Boundary Conditions-Maintenance Case

6.3. Floating Case

When the roof is floating on the process fluid, the deck stays level with respect to the XY plane. Based on that, in order to bound the model in the Z direction, displacement of the deck

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nodes are fixed in Z direction. On the other hand, since the outer rim of the pontoons is constrained by the roof seal to the shell, displacement of nodes on the outer rim are fixed in the X and Y directions

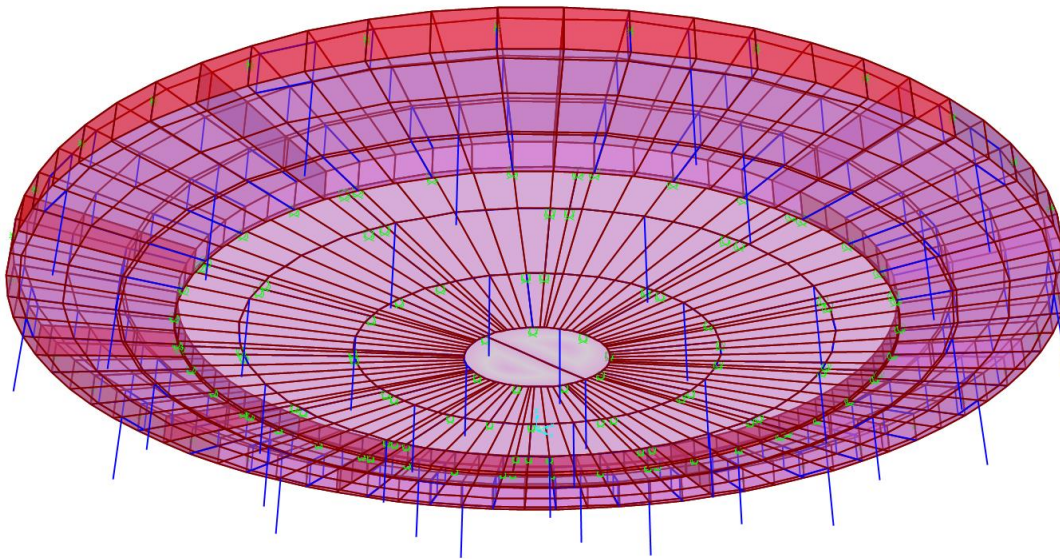


Figure 11: Roof Structure Boundary Conditions-Floating Case

6.4. Loads

6.4.1. Load Combinations for Analyzing the Supports

Following load combinations are considered in the calculation for floating roof support as per API-650-Annex H:

$$D_f + (\text{the greater of}) P_{fe} \text{ or } L_{f1} \text{ or } L_{f2}$$

D_f is the dead load of internal floating roof, including the weight of the flotation compartments, seal and all other floating roof and attached components;

L_{f1} is the internal floating roof uniform live load (0.6 kPa [12.5 lbf/ft²] if not automatic drains are provided, 0.24 kPa [5 lbf/ft²] if automatic drains are provided);

L_{f2} is the internal floating roof point load of at least two men walking anywhere on the roof. One applied load of 2.2 kN [500 lbf] over 0.1 m² [1 ft²] applied anywhere on the roof addresses two men walking;

P_{fe} is the internal floating roof design external pressure (0.24 kPa [5 lbf/ft²] minimum).

Therefore, following load combinations are considered in the SAP model:

#	Load Combination
1	$D_f + L_{f1}$
2	$D_f + L_{f2}$
3	$D_f + P_{fe}$

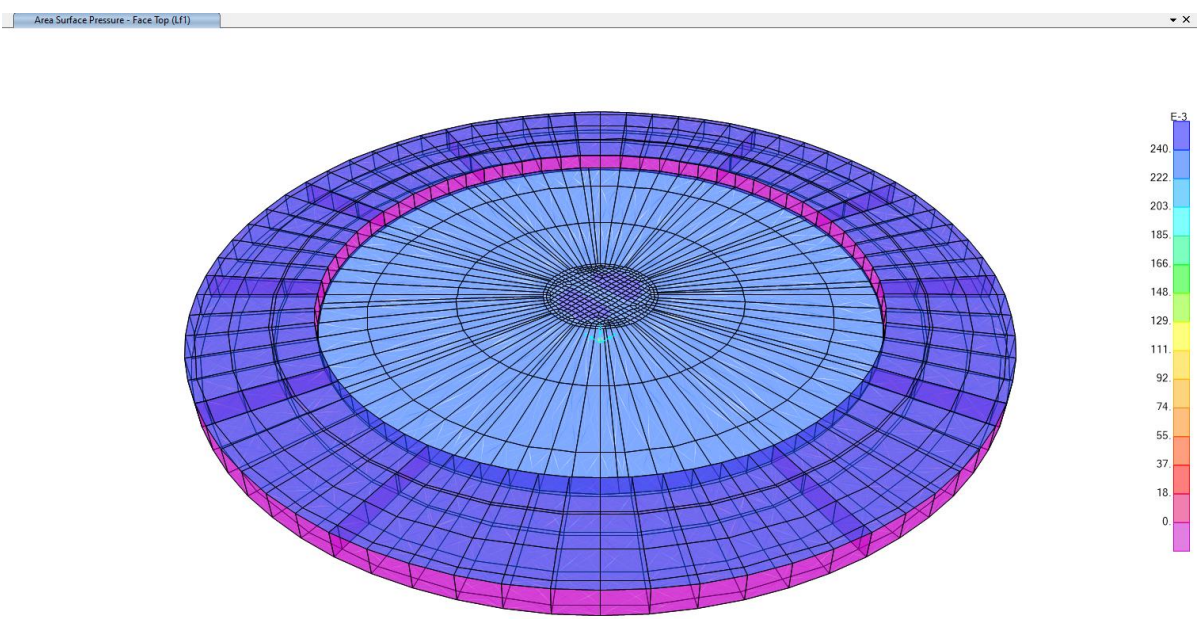


Figure 12: LF1 Load (kN/m2)

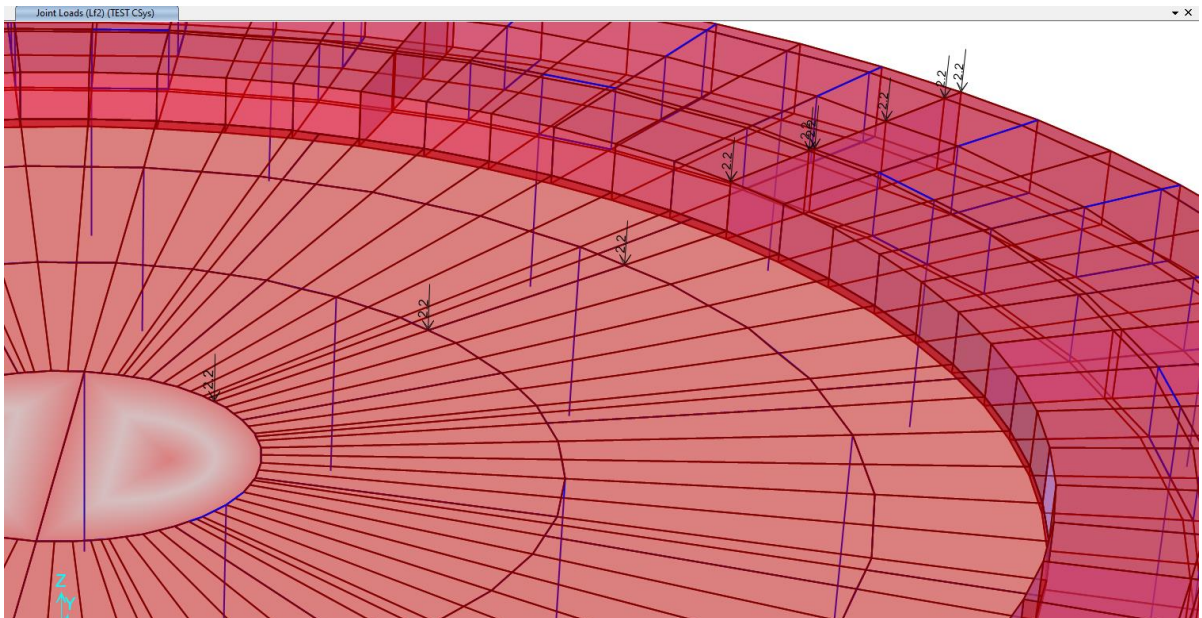


Figure 13: LF2 Load (kN)

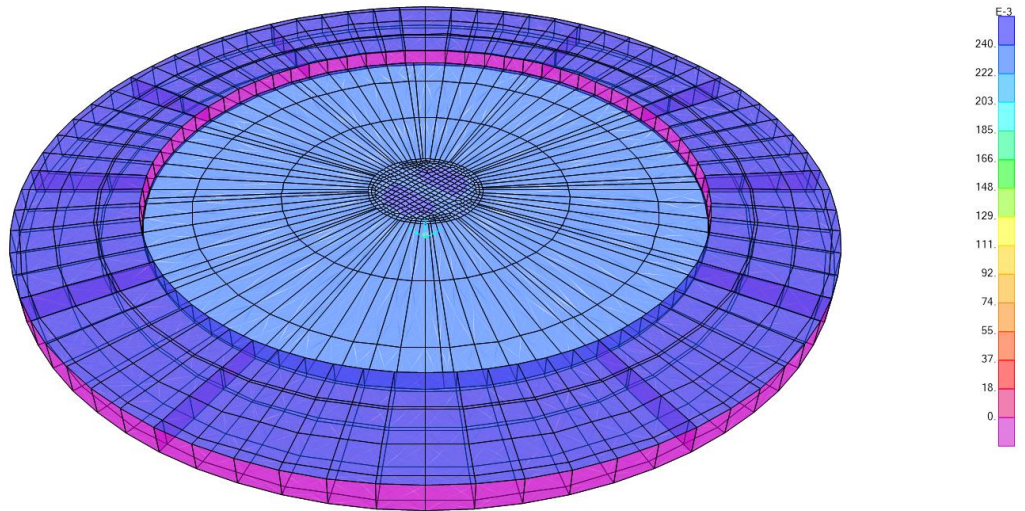


Figure 14: PE Load (kN/m2)

6.4.2. Load Combinations for the Floating Case

For the floating case following load case is considered:

#	Load Combination
1	$D_f + BUO$

D_f is the dead load of internal floating roof, including the weight of the flotation compartments, seal and all other floating roof and attached components;

BUO is the hydrostatic pressure of the liquid which are calculated in section 5.1.3

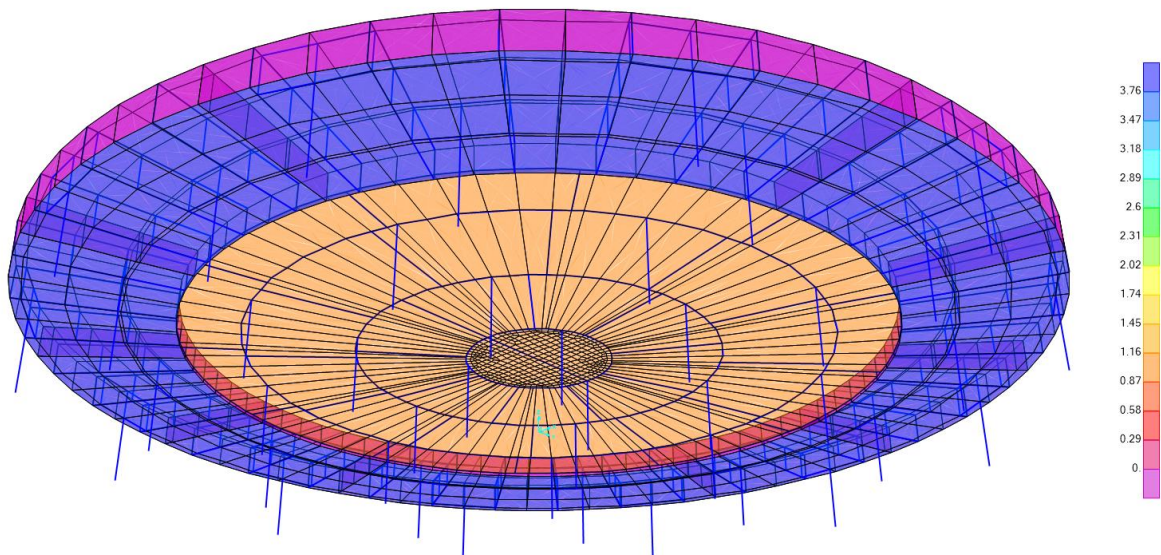


Figure 15: BUO Load - Intact (kN/m2)

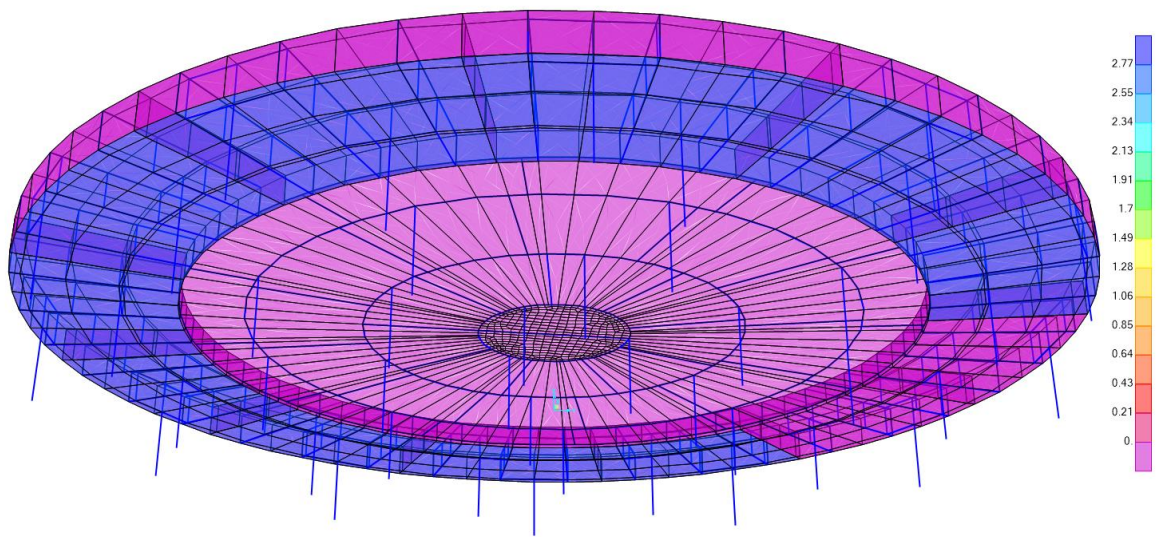


Figure 16: BUO Load - Punctured (kN/m²)

6.5. Section Design

Roof structure layout and sections design are done for optimum strength of the structure considering loads which are specified in section 6.4. In this regard sections are from commonly available profiles and following considerations are followed:

Item	Value
1 Design Code	AISC 360-10
2 Multi-Response Case Design	Envelopes
3 Framing Type	OMF
4 Seismic Design Category	D
5 Importance Factor	1.25
6 Design System Rho	1.
7 Design System Sds	0.5
8 Design System R	8.
9 Design System Omega0	3.
10 Design System Cd	5.5
11 Design Provision	ASD
12 Analysis Method	Direct Analysis
13 Second Order Method	General 2nd Order
14 Stiffness Reduction Method	Tau-b Fixed
15 Omega(Bending)	1.67
16 Omega(Compression)	1.67
17 Omega(Tension-Yielding)	1.67
18 Omega(Tension-Fracture)	2.
19 Omega(Shear)	1.67
20 Omega(Shear-Short Webed Rolled I)	1.5
21 Omega(Torsion)	1.67
22 Ignore Seismic Code?	No
23 Ignore Special Seismic Load?	No

24	Is Doubler Plate Plug-Welded?	Yes
25	HSS Welding Type	ERW
26	Reduce HSS Thickness?	No
27	Consider Deflection?	Yes
28	DL Limit, L/	200.
29	Super DL+LL Limit, L/	200.
30	Live Load Limit, L/	200.
31	Total Limit, L/	200.
32	Total-Camber Limit, L/	200.
33	Pattern Live Load Factor	0.75
34	Demand/Capacity Ratio Limit	0.95

7. Results

7.1. Maintenance case

7.1.1. Overall View

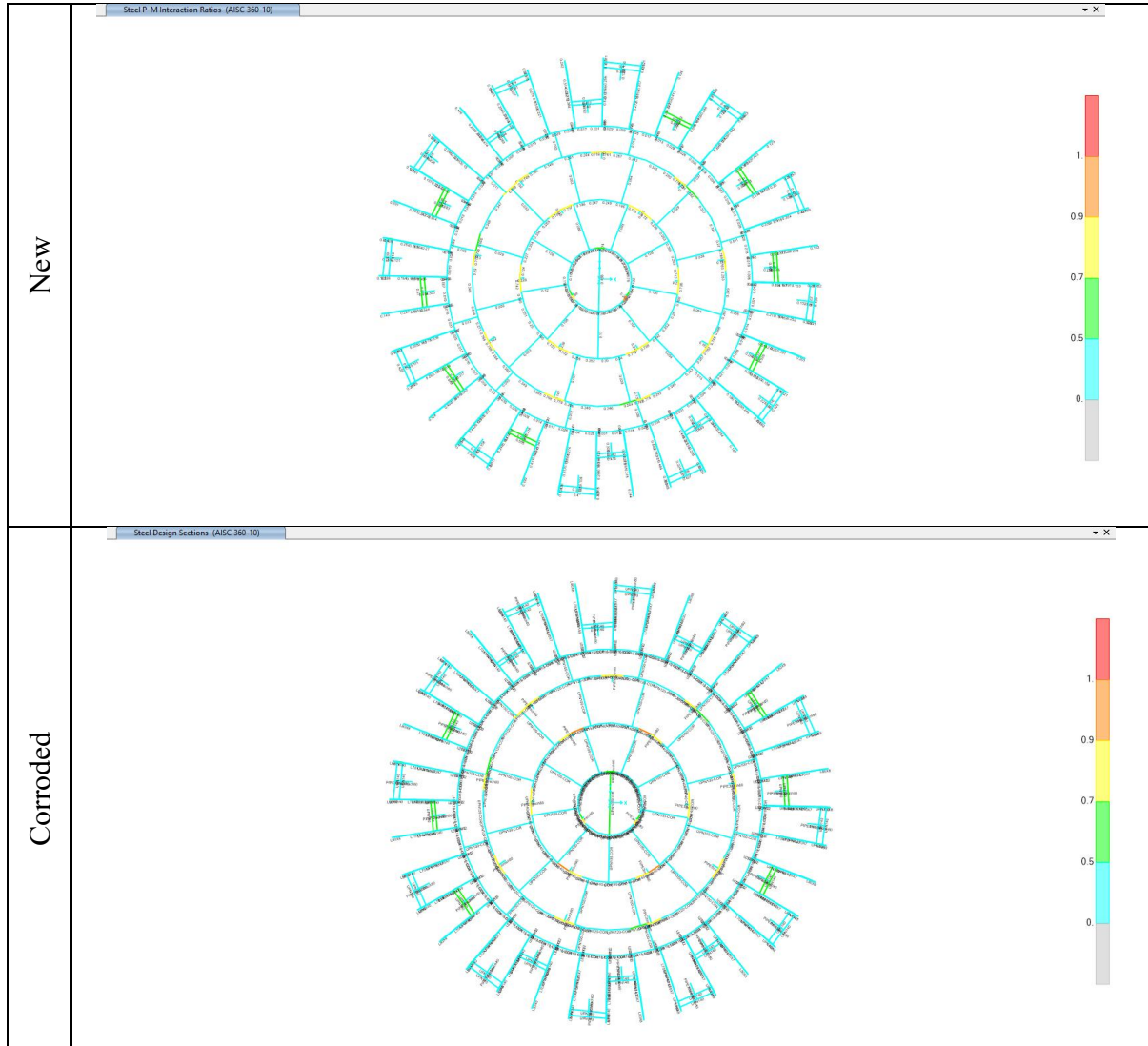


Figure 17: P-M Ratio of the Roof Structure – Maintenance case

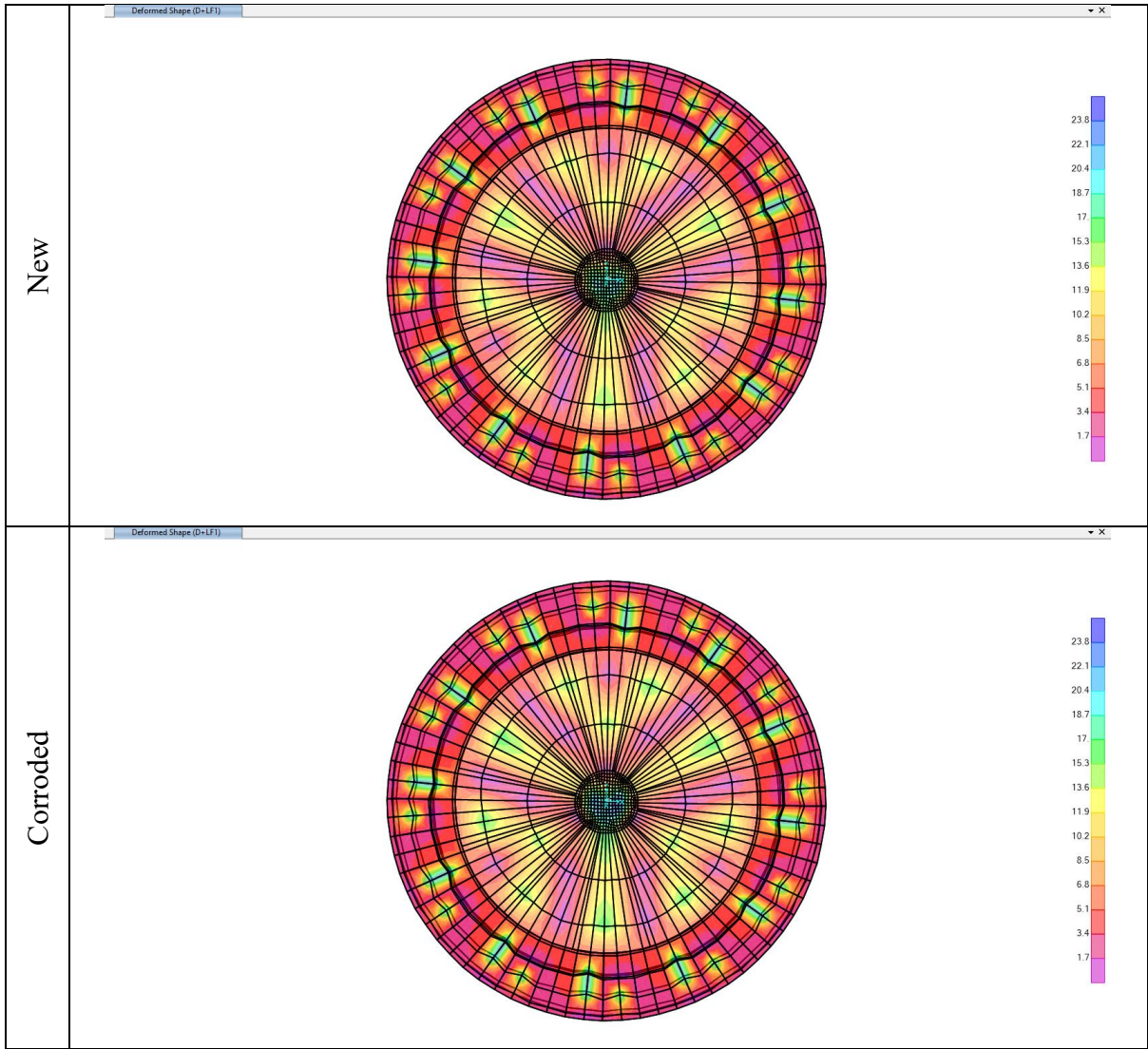
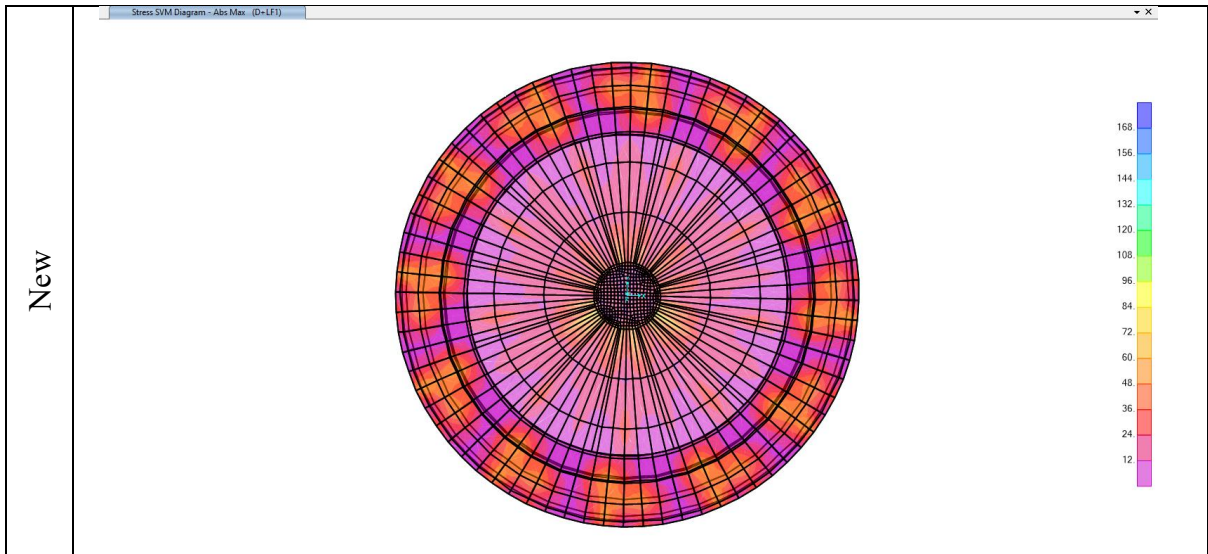


Figure 18: Deflection of Plates (mm) – Maintenance case



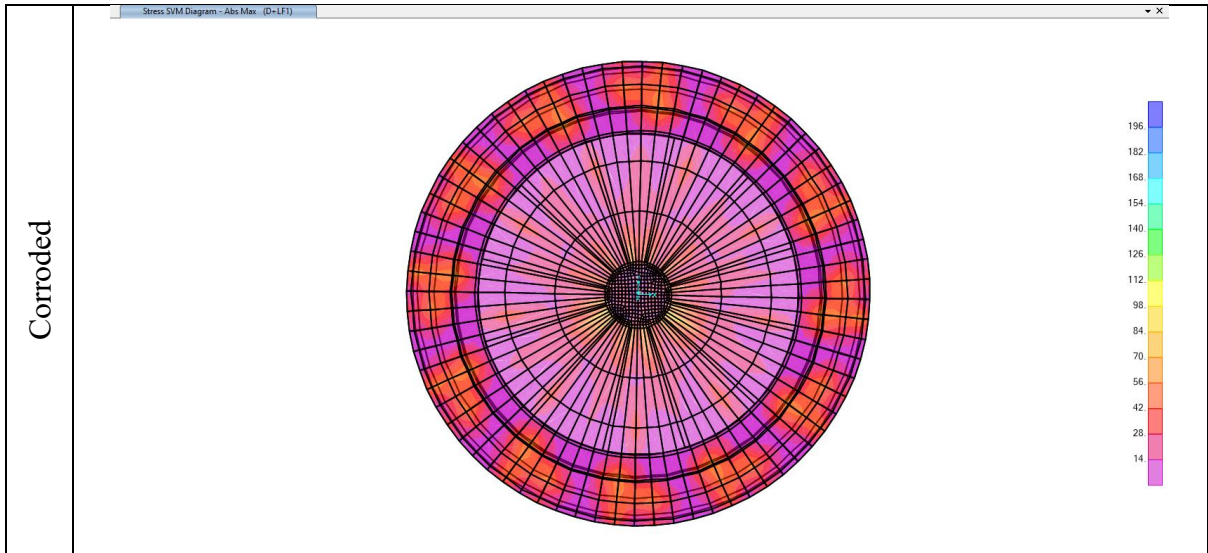
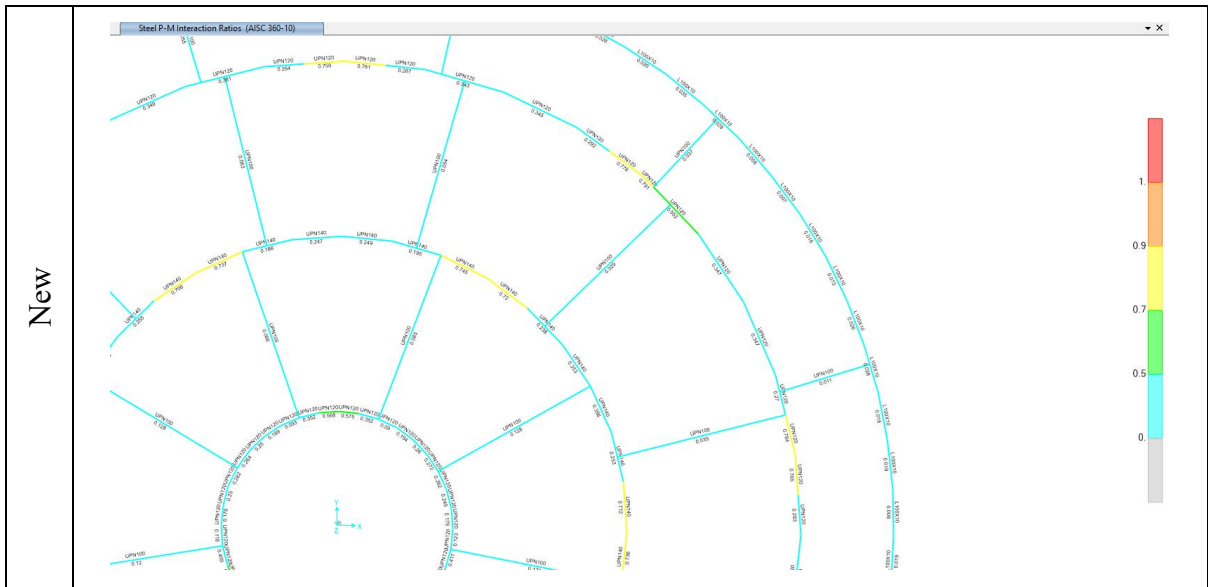


Figure 19: Shell SVM Stress (MPa) – Maintenance case

7.1.2. Deck Structure



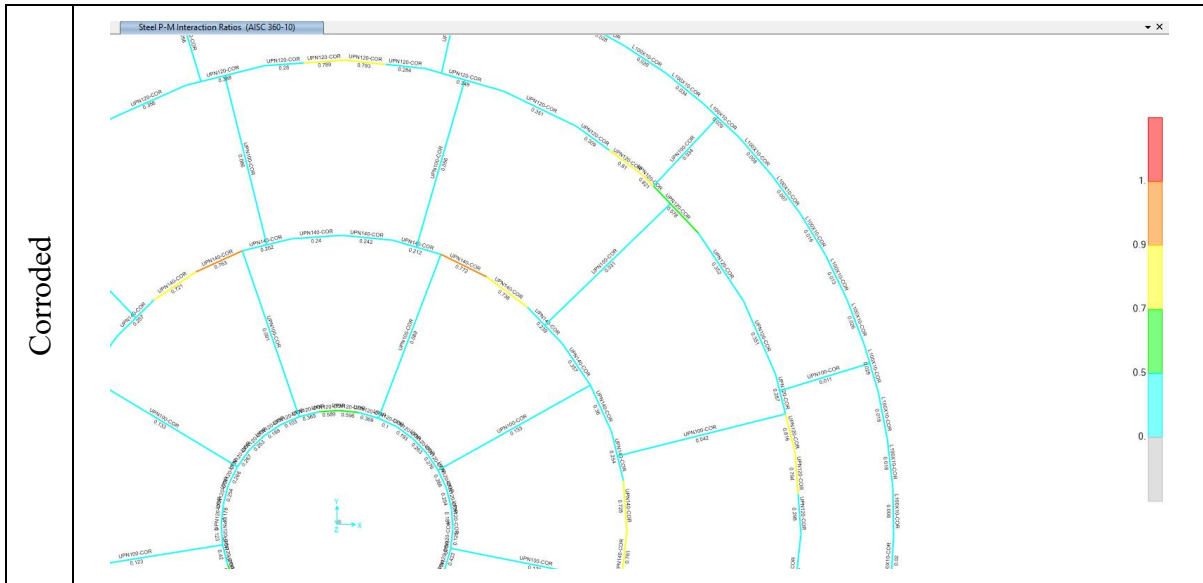


Figure 20: P-M Ratio of the Roof Structure– Maintenance case

P-M Ratio for the worst case - NEW

AISC 360-10 STEEL SECTION CHECK (Summary for Combo and Station)
 Units : N, mm, C

Frame : 617 X Mid: -7840.212 Combo: ENV Design Type: Beam
 Length: 277.873 Y Mid: 1524.558 Shape: UPN120 Frame Type: OMF
 Loc : 277.873 Z Mid: 2100. Class: Compact Princpl Rot: 0. degrees

Provision: ASD Analysis: Direct Analysis
 D/C Limit=0.95 2nd Order: General 2nd Order Reduction: Tau-b Fixed
 AlphaPr/Py=0.002 AlphaPr/Pe=7E-05 Tau_b=1. EA factor=0.8 EI factor=0.8

OmegaB=1.67 OmegaC=1.67 OmegaTY=1.67 OmegaTF=2.
 OmegaV=1.67 OmegaV-RI=1.5 OmegaVT=1.67

A=1704. I33=3675168. r33=46.441 S33=61252.8 Av3=990.
 J=35132.17 I22=491416.592 r22=16.982 S22=13084.785 Av2=840.
 E=199947.979 Fy=248.211 Ry=1.5 z33=73152. Cw=1053471116.3
 RLLF=1. Fu=399.896 z22=23668.

STRESS CHECK FORCES & MOMENTS (Combo ENV)

Location	Pr	Mr33	Mr22	Vr2	Vr3	Tr
277.873	540.315	-8656405.8	4283.484	10101.974	-30.212	-18231.683

PMM DEMAND/CAPACITY RATIO (H1.2,H1-1b)
 D/C Ratio: 0.799 = 0.001 + 0.796 + 0.001
 = (1/2)(Pr/Pc) + (Mr33/Mc33) + (Mr22/Mc22)

AXIAL FORCE & BIAxIAL MOMENT DESIGN (H1.2,H1-1b)

Factor	L	K1	K2	B1	B2	Cm
Major Bending	1.	1.	1.	1.	1.	1.
Minor Bending	1.	1.	1.	1.	1.	1.

Ltb	Ltb	Ktb	Cb
LTB	1.	1.	1.148

Pr	Pnc/Omega	Pnt/Omega	
Force	Capacity	Capacity	
Axial	540.315	247721.312	253264.687

Mr	Mn/Omega	Mn/Omega	Mn/Omega
Moment	Capacity	No LTB	Cb=1
Major Moment	-8656405.8	10872546.02	10872546.02
Minor Moment	4283.484	3111656.215	

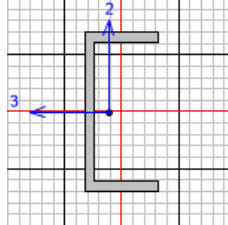
SHEAR CHECK

	Vr	Vn/Omega	Stress	Status
	Force	Capacity	Ratio	Check
Major Shear	10101.974	74909.274	0.135	OK
Minor Shear	30.212	88285.93	0.	OK

CONNECTION SHEAR FORCES FOR BEAMS

	VMajor	VMajor
	Left	Right
Major (V2)	10025.437	10101.974

P-M Ratio for the worst case - CORRODED



AISC 360-10 STEEL SECTION CHECK (Summary for Combo and Station)
Units : N, mm, C

Frame : 617 X Mid: -7840.212 Combo: ENV Design Type: Beam
 Length: 277.873 Y Mid: 1524.558 Shape: UPN120-COR Frame Type: OMF
 Loc : 277.873 Z Mid: 2100. Class: Compact Princpl Rot: 0. degrees

Provision: ASD Analysis: Direct Analysis
 D/C Limit=0.95 2nd Order: General 2nd Order Reduction: Tau-b Fixed
 AlphaPr/Py=0.002 AlphaPr/Pe=8E-05 Tau_b=1. EA factor=0.8 EI factor=0.8

OmegaB=1.67 OmegaC=1.67 OmegaTY=1.67 OmegaTF=2.
 OmegaV=1.67 OmegaV-RI=1.5 OmegaVT=1.67

A=1520.25 I33=3240189.703 r33=46.167 S33=54686.746 Av3=882.75
 J=26062.086 I22=419237.177 r22=16.606 S22=11436.793 Av2=740.625
 E=199947.979 Fy=248.211 Ry=1.5 z33=64917.844 Cw=887457854.8
 RLLF=1. Fu=399.896 z22=20710.048

STRESS CHECK FORCES & MOMENTS (Combo ENV)

Location	Pr	Mr33	Mr22	Vr2	Vr3	Tr
277.873	563.836	-7973103.6	4071.128	9049.732	-27.581	-13086.075

PMM DEMAND/CAPACITY RATIO (H1.2,H1-1b)

D/C Ratio: 0.829 = 0.001 + 0.826 + 0.001
 = (1/2)(Pr/Pc) + (Mr33/Mc33) + (Mr22/Mc22)

AXIAL FORCE & BIAXIAL MOMENT DESIGN (H1.2,H1-1b)

Factor	L	K1	K2	B1	B2	Cm
Major Bending	1.	1.	1.	1.	1.	1.
Minor Bending	1.	1.	1.	1.	1.	1.

	Ltb	Kltb	Cb
LTB	1.	1.	1.144

	Pr	Pnc/Omega	Pnt/Omega
	Force	Capacity	Capacity
Axial	563.836	220783.559	225954.015

	Mr	Mn/Omega	Mn/Omega	Mn/Omega
	Moment	Capacity	No LTB	Cb=1
Major Moment	-7973103.6	9648707.397	9648707.397	9648707.397
Minor Moment	4071.128	2719751.96		

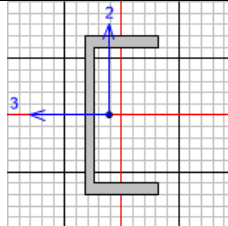
SHEAR CHECK

	Vr	Vn/Omega	Stress	Status
	Force	Capacity	Ratio	Check
Major Shear	9049.732	66047.239	0.137	OK
Minor Shear	27.581	78721.621	0.	OK

CONNECTION SHEAR FORCES FOR BEAMS

	VMajor	VMajor
	Left	Right
Major (V2)	8981.447	9049.732

Deflection for the worst case - NEW



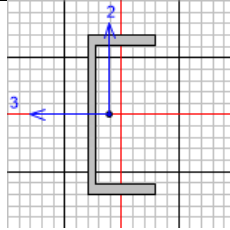
AISC 360-10 STEEL SECTION CHECK (Deflection Details)
 Units : N, mm, C

Frame : 394 X Mid: 1632.224 Combo: def(D+LF2) Design Type: Beam
 Length: 348.144 Y Mid: -1142.603 Shape: UPN120 Frame Type: OMF
 Loc : 0. Z Mid: 2100. Class: Slender Princpl Rot: 0. degrees

DEFLECTION CHECK (Combodef(D+LF))

Type	Consider	Deflection	Limit	Ratio	Status
Dead Load	Yes	0.542	1.741	0.312	OK
Super DL+LL	Yes	1.107	1.741	0.636	OK
Live Load	Yes	1.107	1.741	0.636	OK
Total Load	Yes	1.65	1.741	0.948	OK
Total-Camber	Yes	1.65	1.741	0.948	OK

Deflection for the worst case - CORRODED



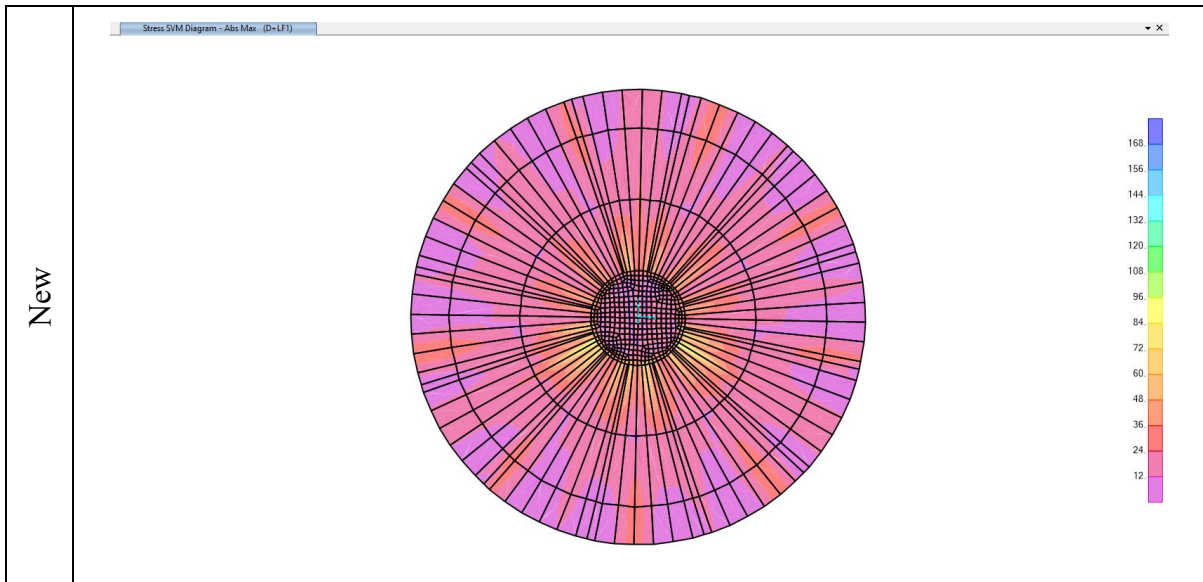
AISC 360-10 STEEL SECTION CHECK (Deflection Details)
 Units : N, mm, C

Frame : 332 X Mid: -2105.732 Combo: def(D+PE) Design Type: Beam
 Length: 870.57 Y Mid: 4514.089 Shape: UPN140-COR Frame Type: OMF
 Loc : 0. Z Mid: 2100. Class: Slender Princpl Rot: 0. degrees

DEFLECTION CHECK (Combodef(D+PE))

Type	Consider	Deflection	Limit	Ratio	Status
Dead Load	Yes	1.83	4.353	0.42	OK
Super DL+LL	Yes	0.	4.353	0.	OK
Live Load	Yes	0.	4.353	0.	OK
Total Load	Yes	4.21	4.353	0.967	OK
Total-Camber	Yes	4.21	4.353	0.967	OK

7.1.3. Deck Plates



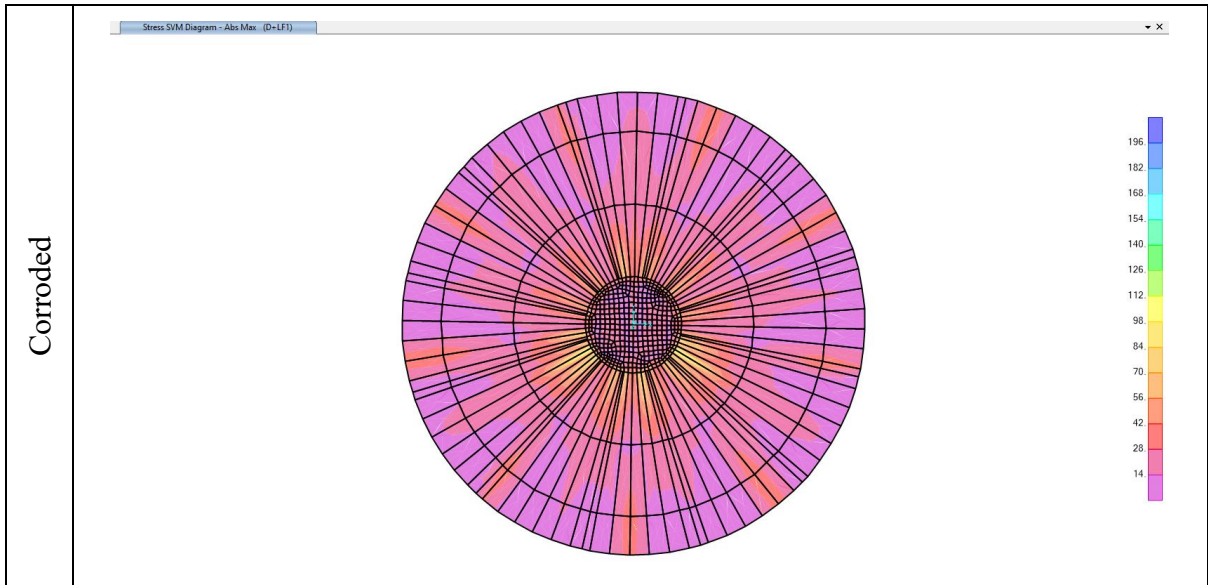
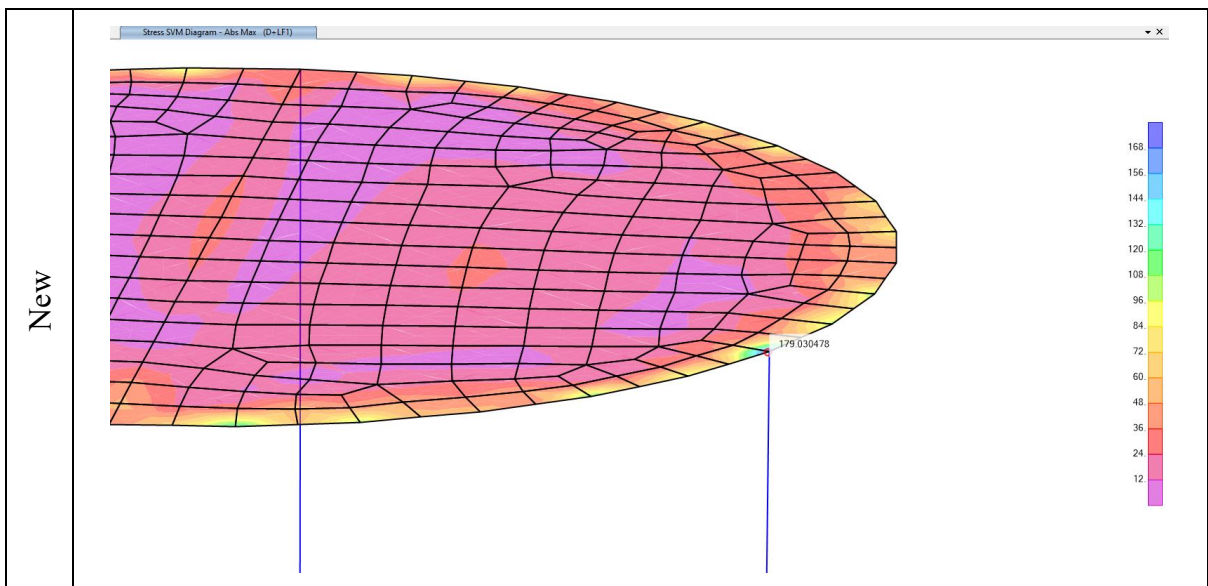


Figure 21: Deck Plate Stress (MPa) – Maintenance case

Based on above results SVM of most of plates are in the allowable range (under 120 MPa). The highest stresses in the results (179 MPa for new and 202 MPa for corroded) are due to stress concentration at the location of supports. These points will be reinforced by an additional pad. For more information, see below figures:



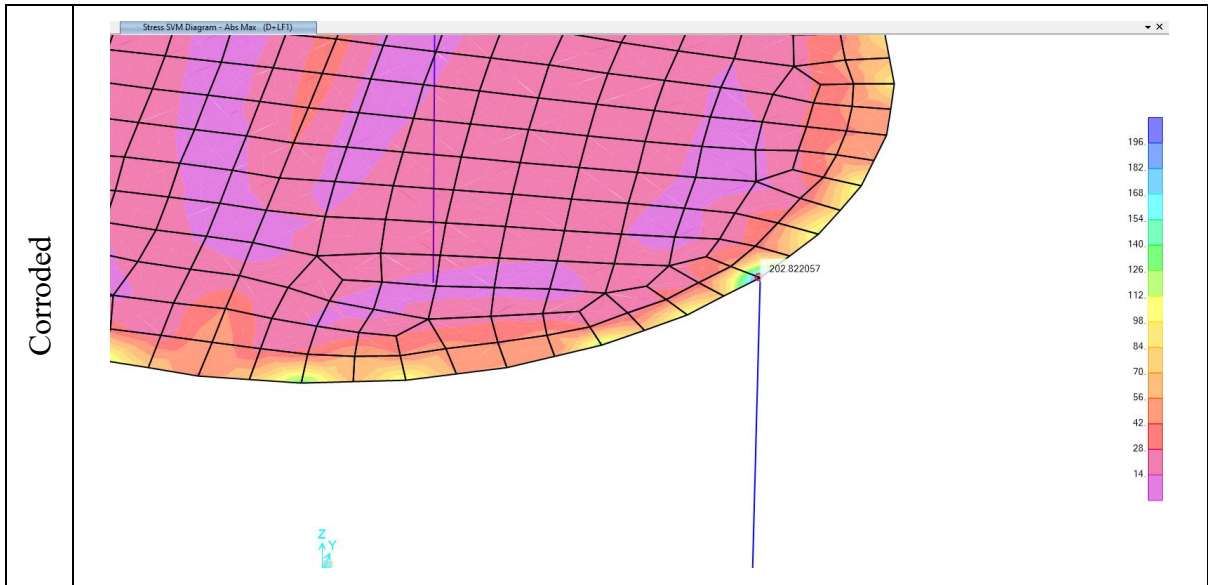
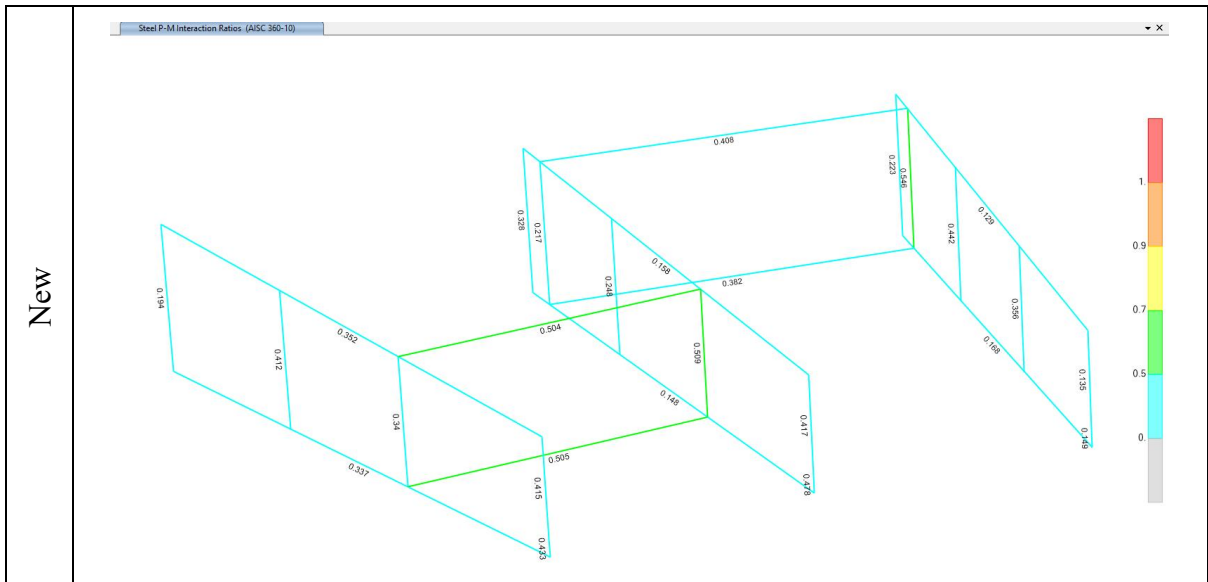


Figure 22: Stress Concentration at the Deck Plate (MPa) -Maintenance Case

7.1.4. Pontoon Structure



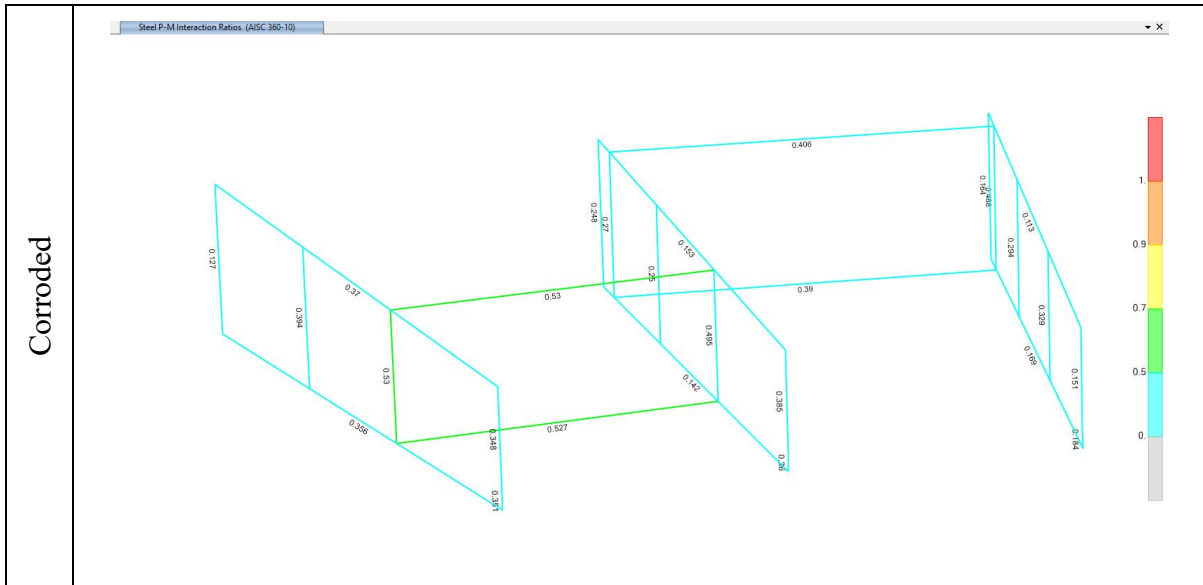


Figure 23: P-M Ratio for Frames in a Pontoon Compartment – Maintenance case

P-M Ratio for the worst case - NEW

AISC 360-10 STEEL SECTION CHECK (Summary for Combo and Station)
 Units : N, mm, C

Frame : 598 X Mid: 3746.815 Combo: ENV Design Type: Column
 Length: 768.108 Y Mid: -10289.981 Shape: L70X7 Frame Type: OMF
 Loc : 768.108 Z Mid: 2384.054 Class: Compact Princpl Rot: 45. degrees

Provision: ASD Analysis: Direct Analysis
 D/C Limit=0.95 2nd Order: General 2nd Order Reduction: Tau-b Fixed
 AlphaPr/Py=0.009 AlphaPr/Pe=0.003 Tau_b=1. EA factor=0.8 EI factor=0.8

OmegaB=1.67 OmegaC=1.67 OmegaTY=1.67 OmegaTF=2.
 OmegaV=1.67 OmegaV-Rl=1.5 OmegaVT=1.67

A=931. I33=432190.531 r33=21.546 S33=8657.48 Av3=490.
 J=14618.088 I22=432190.531 r22=21.546 S22=8657.48 Av2=490.
 Ixy=-255896.053 Imax=688086.583 rmax=27.186 Smax=14633.103
 Rot= 45. deg lmin=176294.478 rmin=13.761 Smin=6208.444
 E=199947.979 Fy=248.211 Ry=1.5 z33=15597.925
 RLLF=1. Fu=399.896 z22=15597.925

STRESS CHECK FORCES & MOMENTS (Combo ENV)

Location	Pr	Mr33	Mr22	Vr2	Vr3	Tr
768.108	-1279.55	899042.651	78242.076	-1677.976	-226.392	-250.814

PMM DEMAND/CAPACITY RATIO (H2-1)
 D/C Ratio: 0.642 = 0.011 + 0.212 + 0.419
 = fa/Fa + fbw/Fbw + fbz/Fbz

AXIAL FORCE & BIAXIAL MOMENT DESIGN (H2-1)

Factor	L	K1	K2	B1	B2	Cm
Major Bending	1.	1.	1.	1.	1.	0.454
Minor Bending	1.	1.	1.	1.	1.	0.615

Ltb Kltb Cb
 LTB 1. 1. 1.

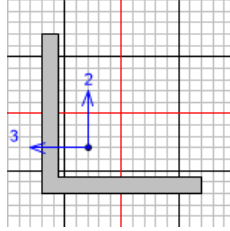
Pr Pnc/Omega Pnt/Omega
 Force Capacity Capacity
 Axial -1279.55 117441.028 138374.075

Mr Mn/Omega Mn/Omega Mn/Omega
 Moment Capacity No LTB Cb=1
 Major Moment 691044.657 3262366.52 3262366.52 3262366.52
 Minor Moment -580393.653 1384137.004

SHEAR CHECK

	Vr	Vn/Omega	Stress	Status
	Force	Capacity	Ratio	Check
Major Shear	1677.976	43697.076	0.038	OK
Minor Shear	1037.558	43697.076	0.024	OK

P-M Ratio for the worst case - CORRODED



AISC 360-10 STEEL SECTION CHECK (Summary for Combo and Station)
Units : N, mm, C

Frame : 598 X Mid: 3746.815 Combo: ENV Design Type: Column
 Length: 768.108 Y Mid: -10289.981 Shape: L70X7 Frame Type: OMF
 Loc : 768.108 Z Mid: 2384.054 Class: Compact Princpl Rot: 45. degrees

Provision: ASD Analysis: Direct Analysis
 D/C Limit=0.95 2nd Order: General 2nd Order Reduction: Tau-b Fixed
 AlphaPr/Py=0.009 AlphaPr/Pe=0.004 Tau_b=1. EA factor=0.8 EI factor=0.8

OmegaB=1.67 OmegaC=1.67 OmegaTY=1.67 OmegaTF=2.
 OmegaV=1.67 OmegaV-RI=1.5 OmegaVT=1.67

A=931. I33=432190.531 r33=21.546 S33=8657.48 Av3=490.
 J=14618.088 I22=432190.531 r22=21.546 S22=8657.48 Av2=490.
 Ixy=-255896.053 Imax=688086.583 rmax=27.186 Smax=14633.103
 Rot= 45. deg Imin=176294.478 rmin=13.761 Smin=6208.444
 E=199947.979 Fy=248.211 Ry=1.5 z33=15597.925
 RLLF=1. Fu=399.896 z22=15597.925

STRESS CHECK FORCES & MOMENTS (Combo ENV)

Location	Pr	Mr33	Mr22	Vr2	Vr3	Tr
768.108	-1362.221	894009.971	77804.378	-1638.573	-218.754	-252.468

PMM DEMAND/CAPACITY RATIO (H2-1)

D/C Ratio: 0.639 = 0.012 + 0.211 + 0.417
 = fa/Fa + fbw/Fbw + fbz/Fbz

AXIAL FORCE & BIAXIAL MOMENT DESIGN (H2-1)

Factor	L	K1	K2	B1	B2	Cm
Major Bending	1.	1.	1.	1.	1.	0.464
Minor Bending	1.	1.	1.	1.	1.	0.611

	Lt/b	Kt/b	Cb
LTB	1.	1.	1.

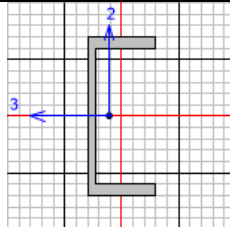
	Pr	Pnc/Omega	Pnt/Omega
	Force	Capacity	Capacity
Axial	-1362.221	117441.028	138374.075

	Mr	Mn/Omega	Mn/Omega	Mn/Omega
	Moment	Capacity	No LTB	Cb=1
Major Moment	687176.516	3262366.52	3262366.52	3262366.52
Minor Moment	-577144.51	1384137.004		

SHEAR CHECK

	Vr	Vn/Omega	Stress	Status
	Force	Capacity	Ratio	Check
Major Shear	1638.573	43697.076	0.037	OK
Minor Shear	1015.879	43697.076	0.023	OK

Deflection for the worst case - NEW



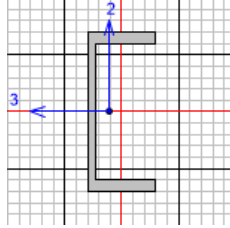
AISC 360-10 STEEL SECTION CHECK (Deflection Details)
Units : N, mm, C

Frame : 219 X Mid: -10957.662 Combo: def(D+PE) Design Type: Beam
 Length: 1924.688 Y Mid: -960.103 Shape: UPN140 Frame Type: OMF
 Loc : 0. Z Mid: 2000. Class: Slender Princpl Rot: 0. degrees

DEFLECTION CHECK (Combodef(D+PE))

Type	Consider	Deflection	Limit	Ratio	Status
Dead Load	Yes	0.767	9.623	0.08	OK
Super DL+LL	Yes	0.	9.623	0.	OK
Live Load	Yes	0.	9.623	0.	OK
Total Load	Yes	1.581	9.623	0.164	OK
Total-Camber	Yes	1.581	9.623	0.164	OK

Deflection for the worst case - CORRODED



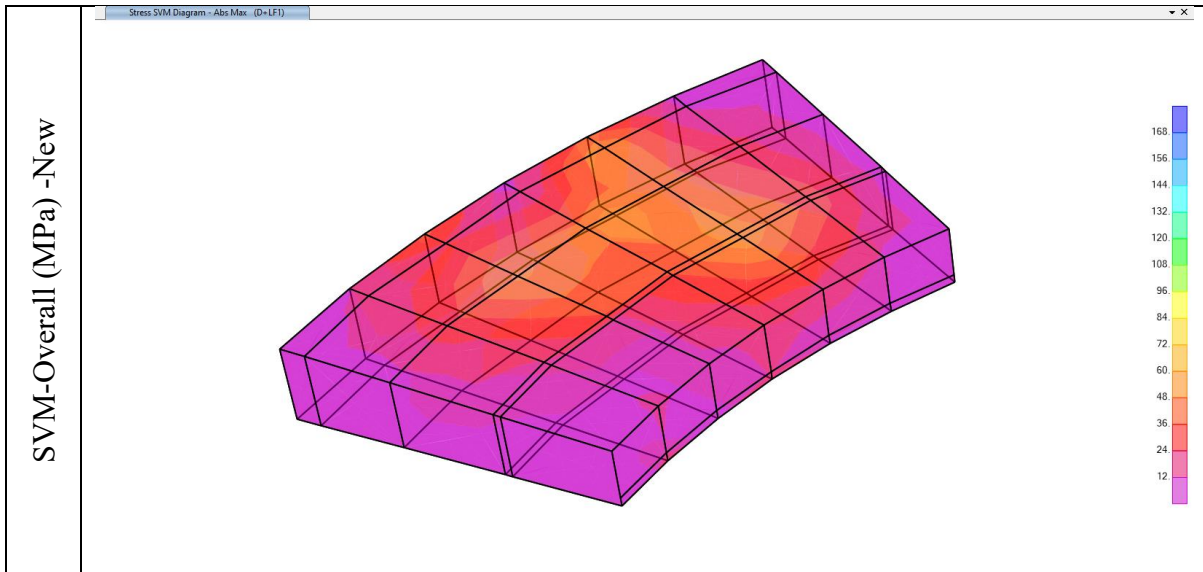
AISC 360-10 STEEL SECTION CHECK (Deflection Details)
Units : N, mm, C

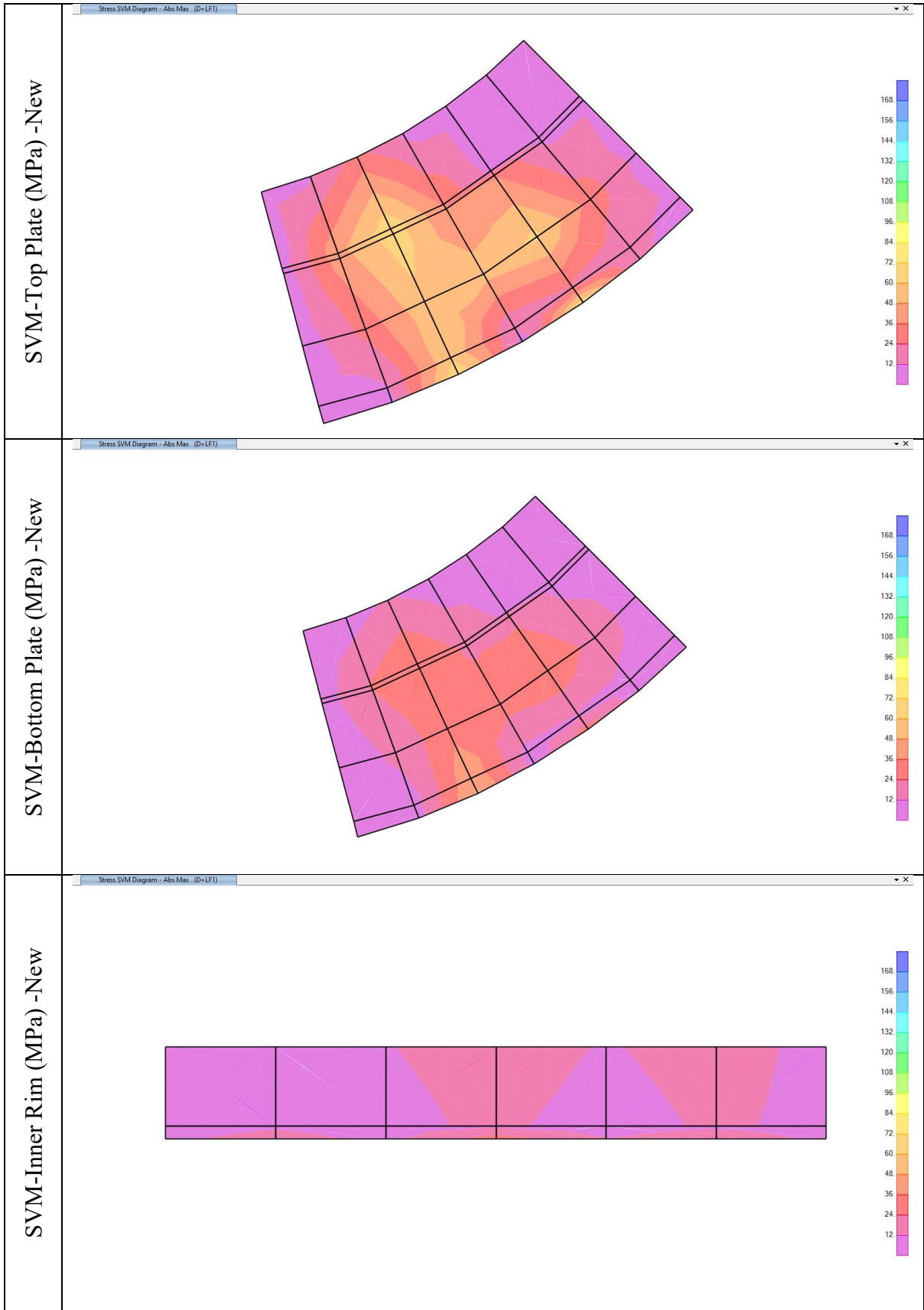
Frame : 219 X Mid: -10957.662 Combo: def(D+PE) Design Type: Beam
Length: 1924.688 Y Mid: -960.103 Shape: UPN140 Frame Type: OMF
Loc : 0. Z Mid: 2000. Class: Slender Princpl Rot: 0. degrees

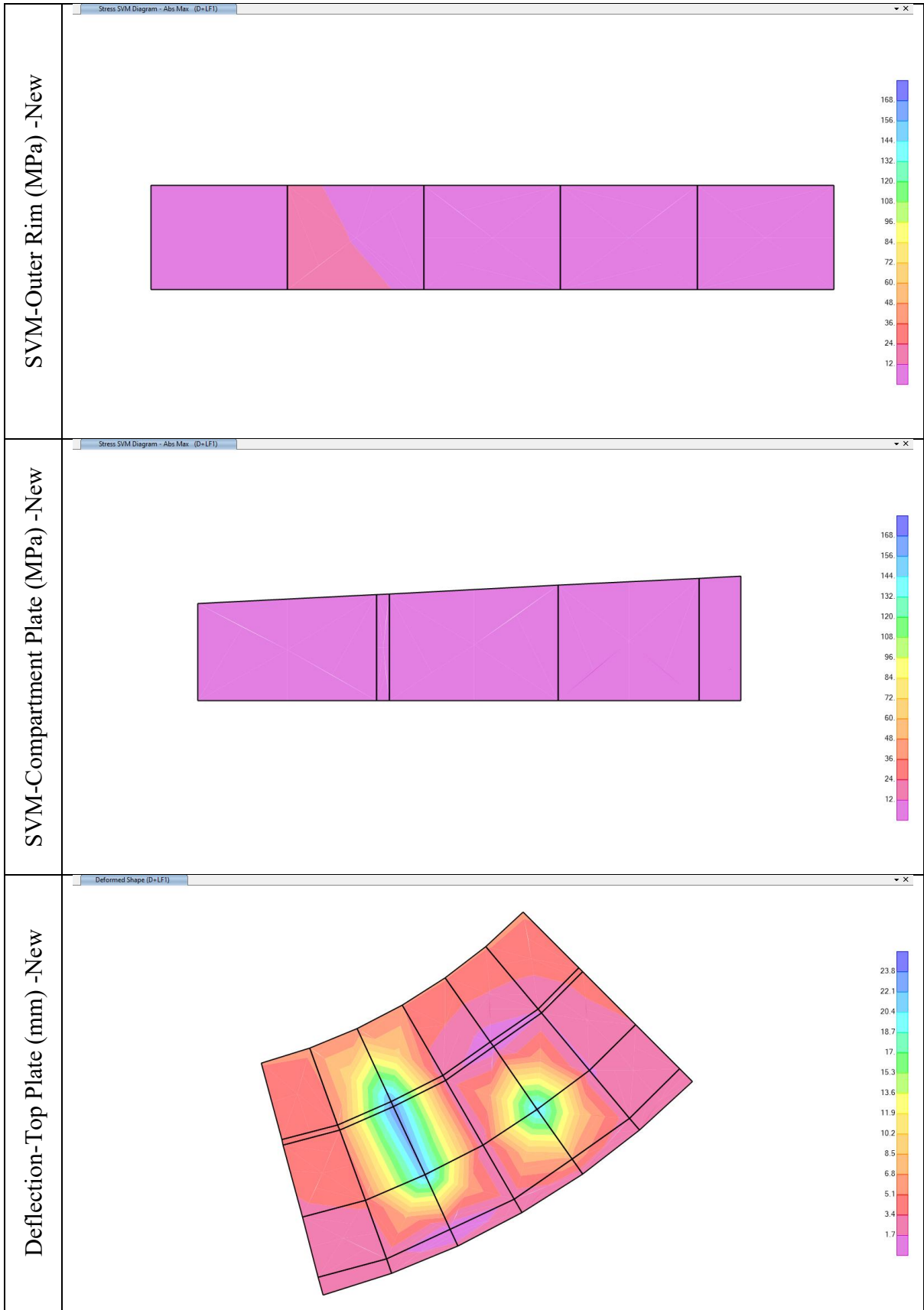
DEFLECTION CHECK (Combodef(D+PE))

Type	Consider	Deflection	Limit	Ratio	Status
Dead Load	Yes	0.737	9.623	0.077	OK
Super DL+LL	Yes	0.	9.623	0.	OK
Live Load	Yes	0.	9.623	0.	OK
Total Load	Yes	1.523	9.623	0.158	OK
Total-Camber	Yes	1.523	9.623	0.158	OK

7.1.5. Pontoon and Compartment Plates







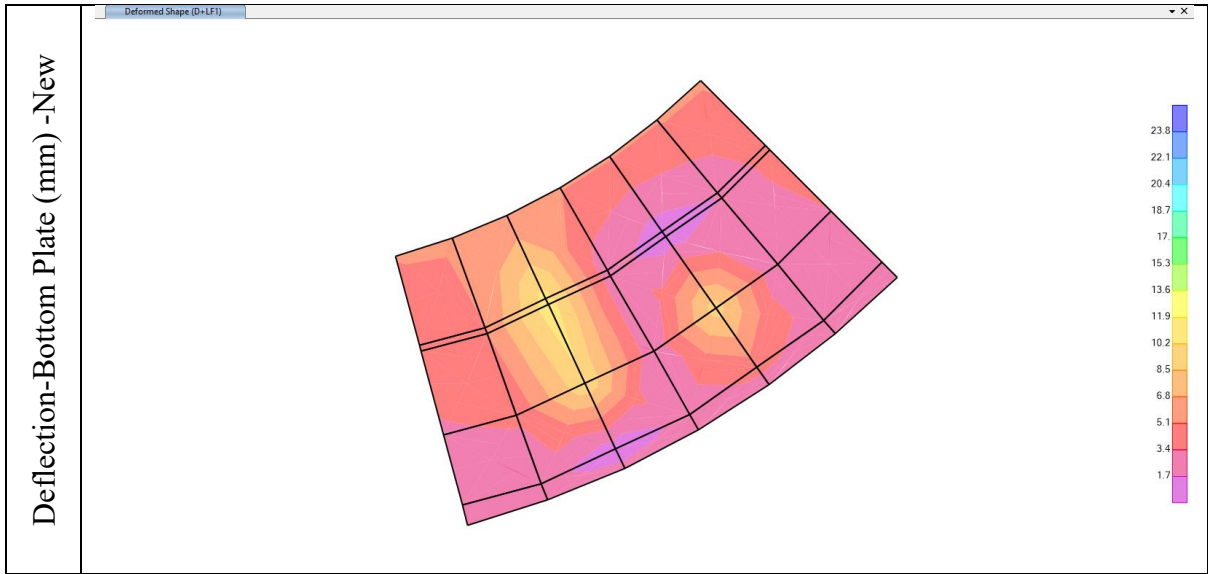
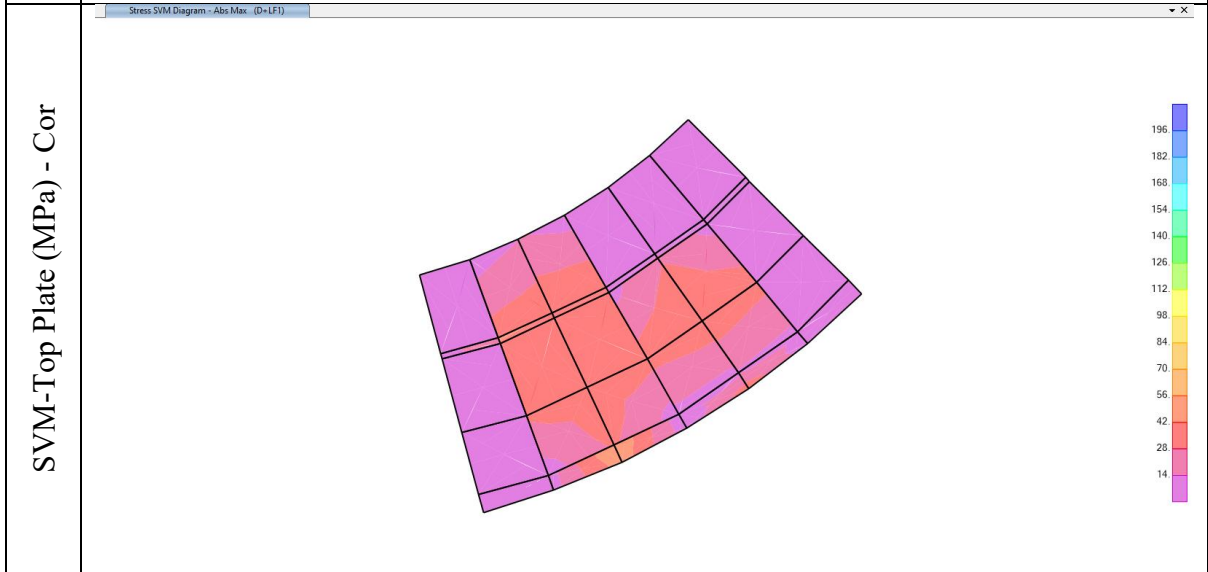
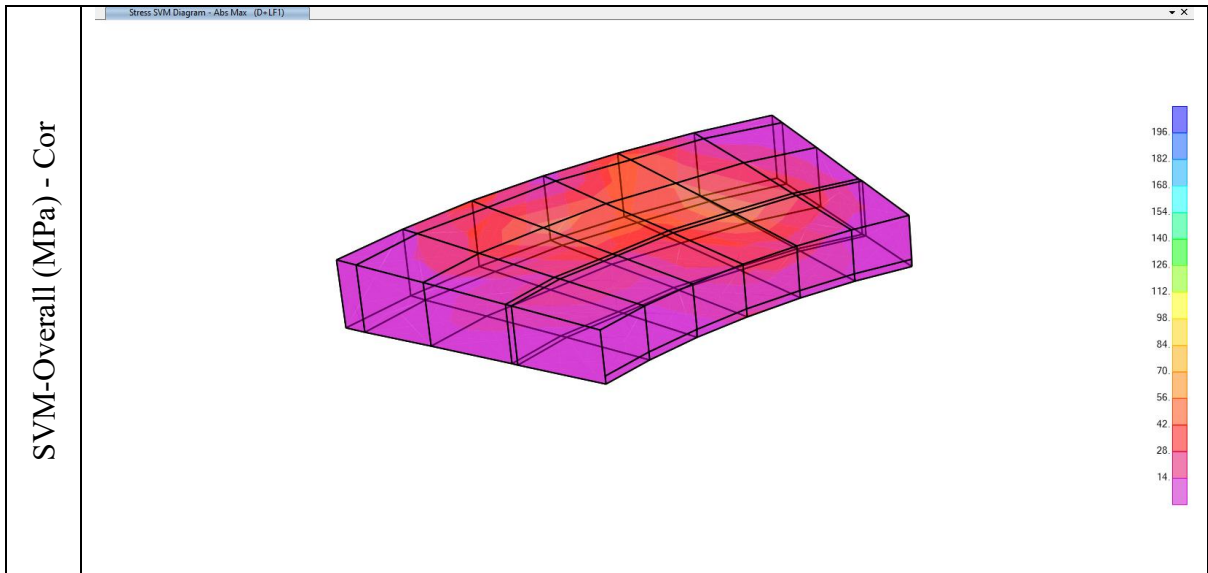
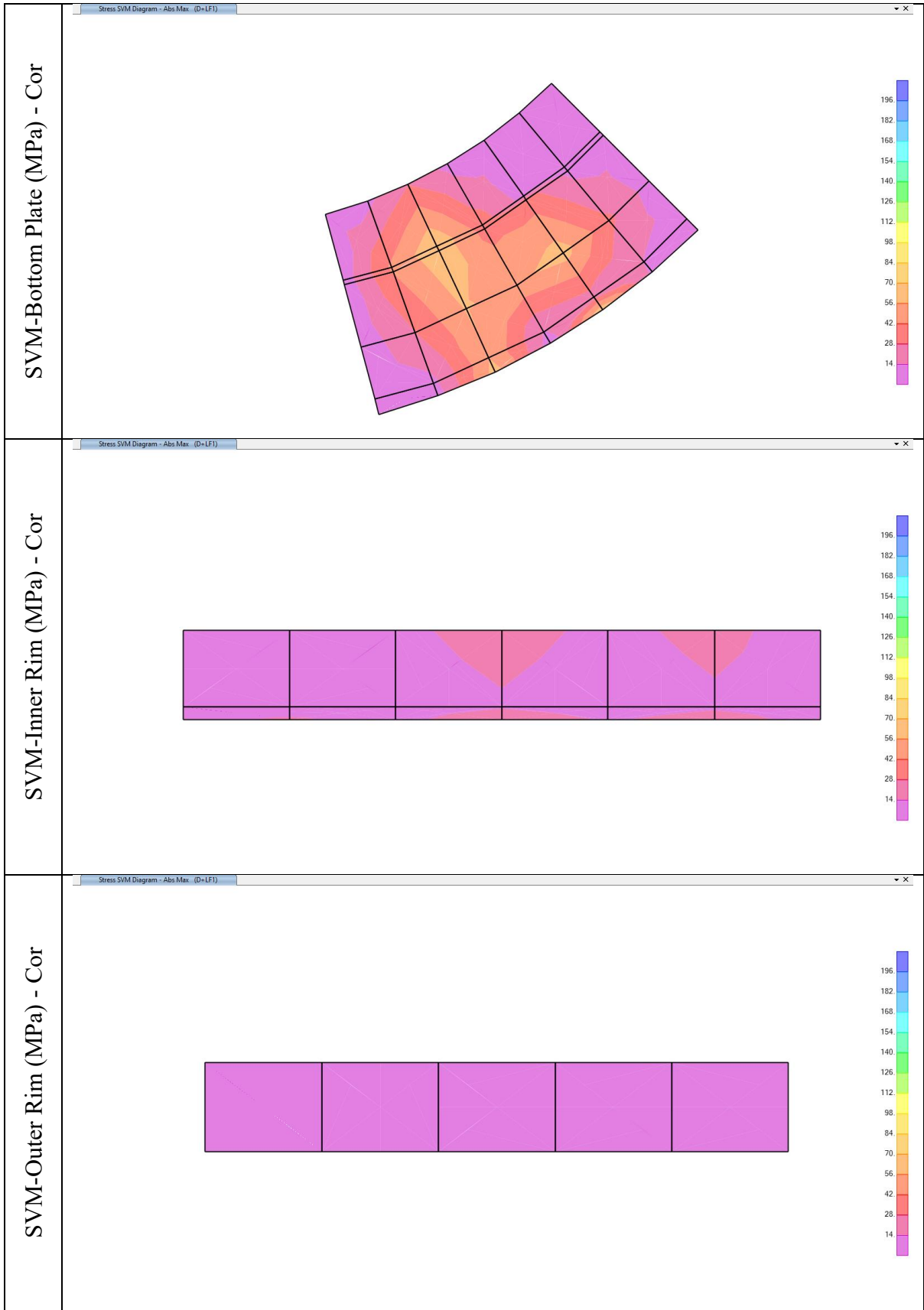


Figure 24: Pontoon Plates Results- Maintenance case -New





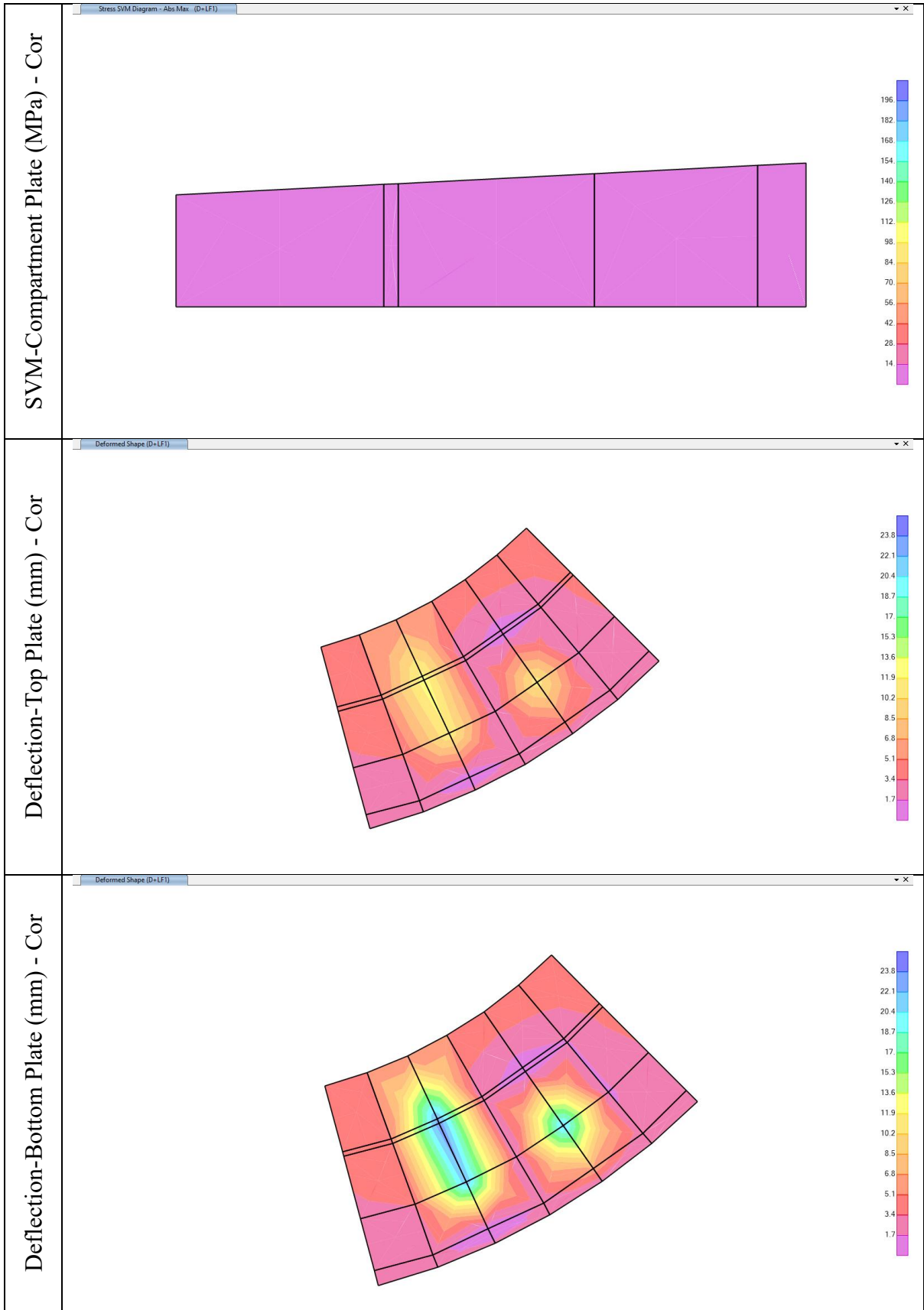


Figure 25: Pontoon Plates Results – Corroded – Maintenance case

7.2. Floating Case

7.2.1. Intact Roof

(1) Overall View

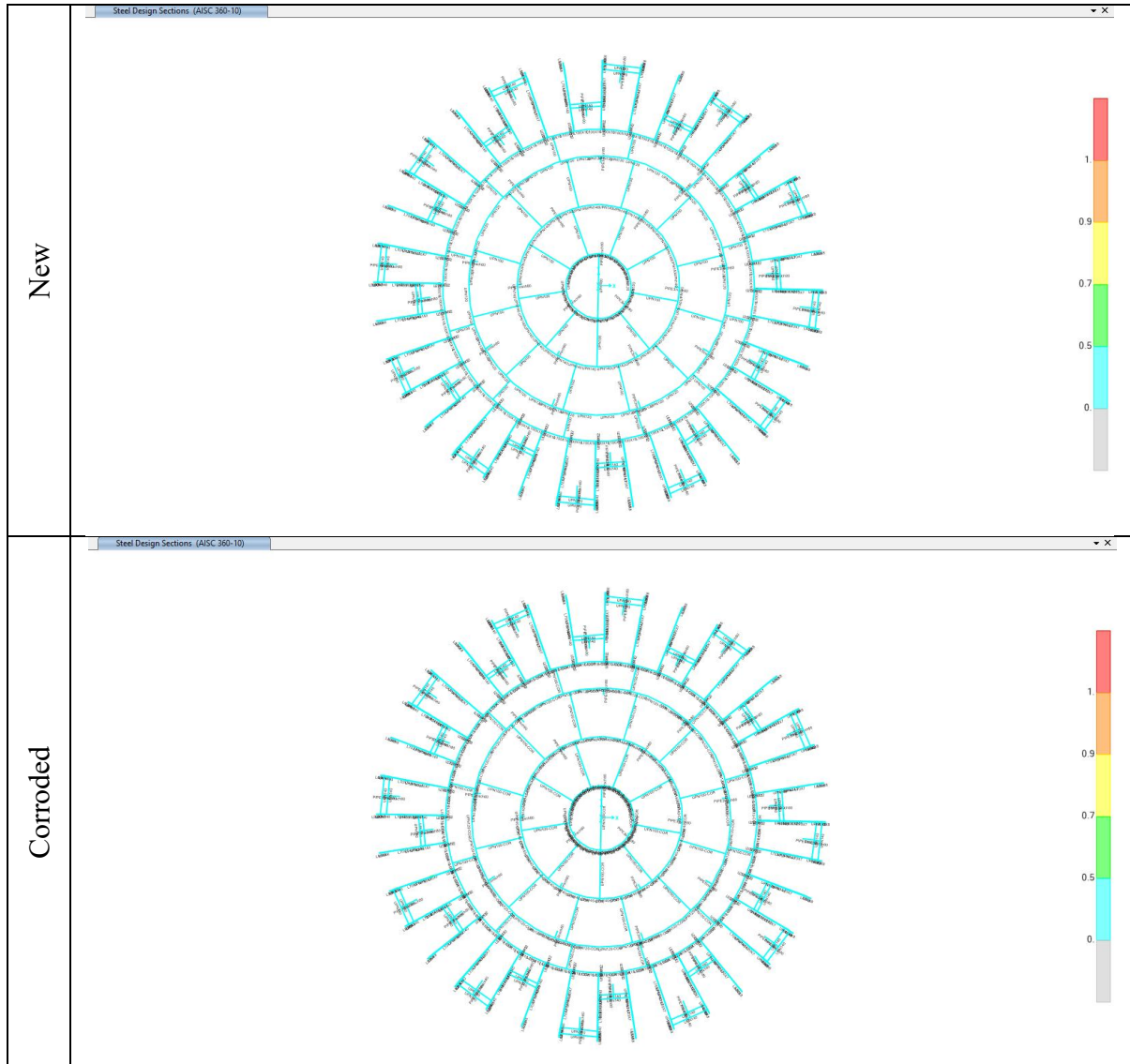


Figure 26: P-M Ratio of the Roof Structure – Floating case - Intact Roof

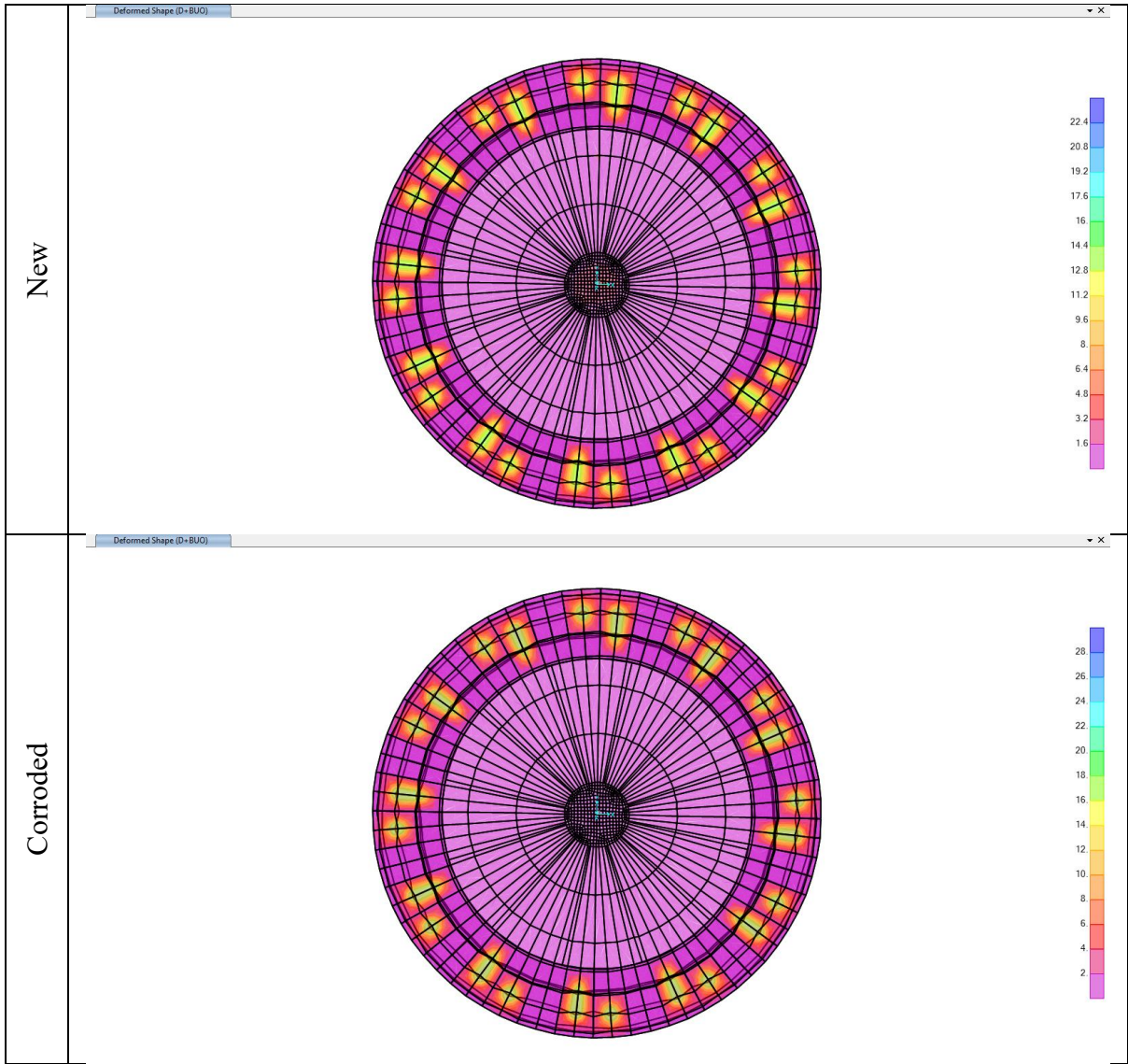
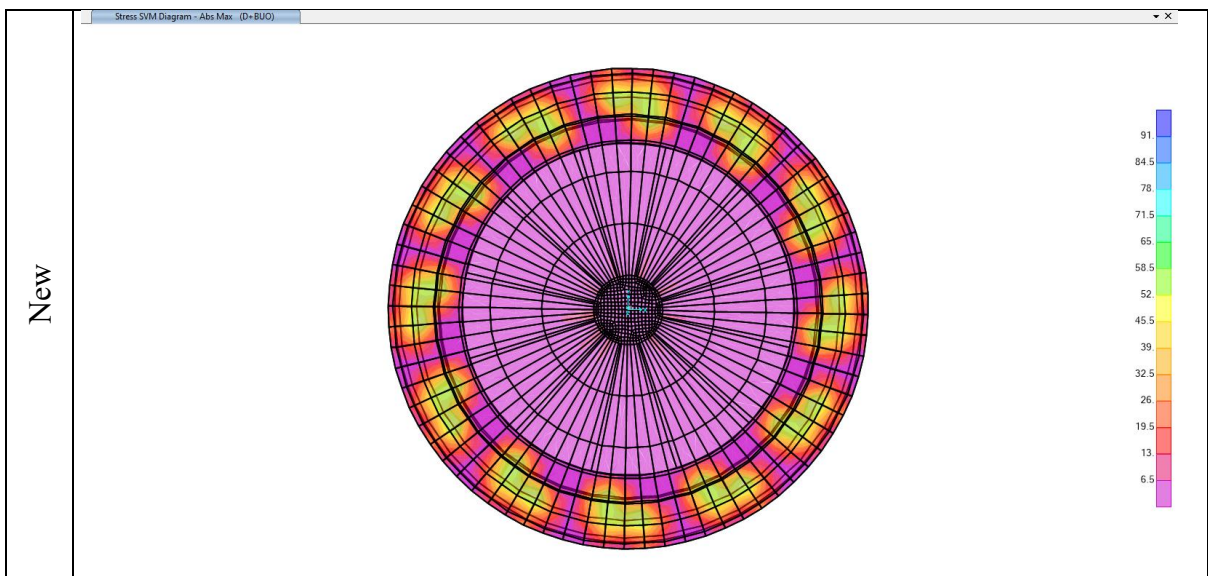


Figure 27: Deflection of Plates (mm) – Floating case - Intact Roof



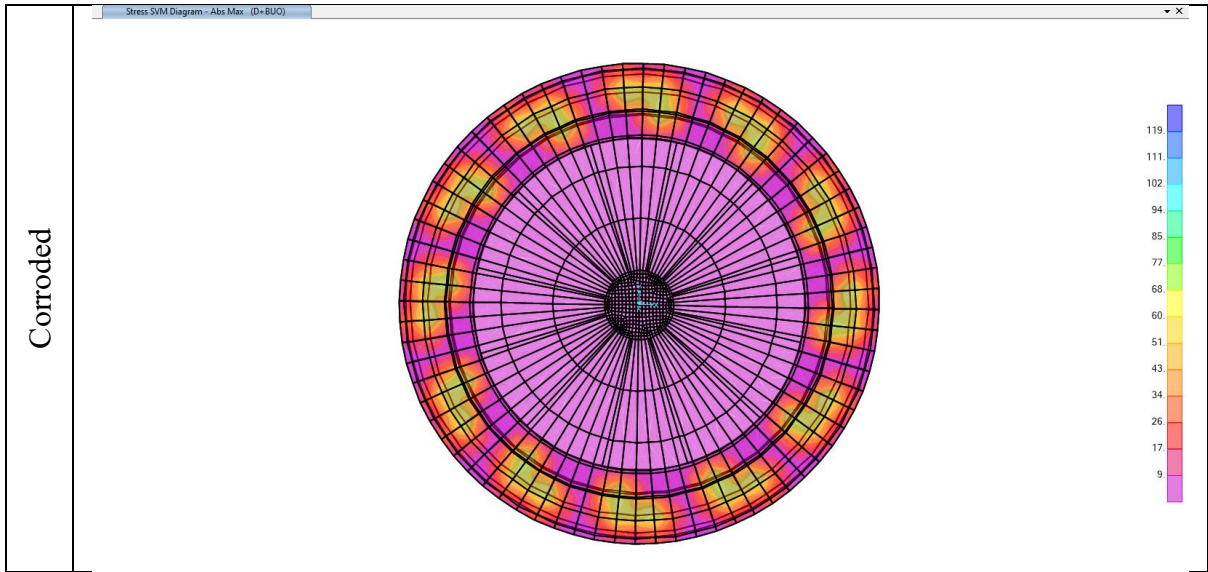
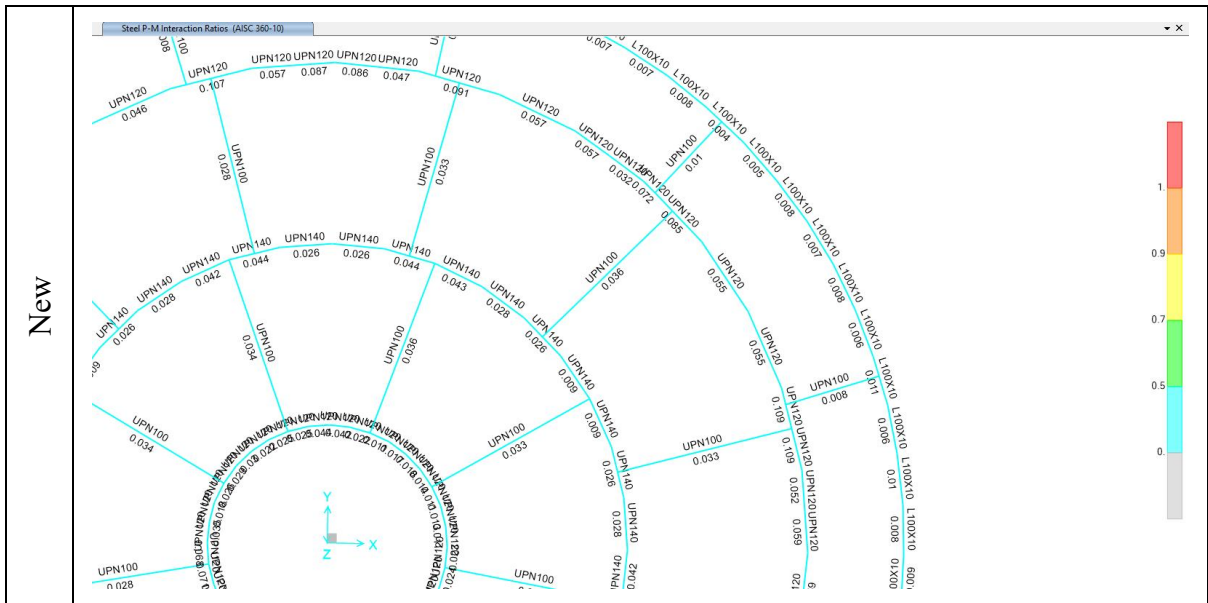


Figure 28: Shell SVM Stress (MPa) – Floating case - Intact Roof

(II) Deck Structure



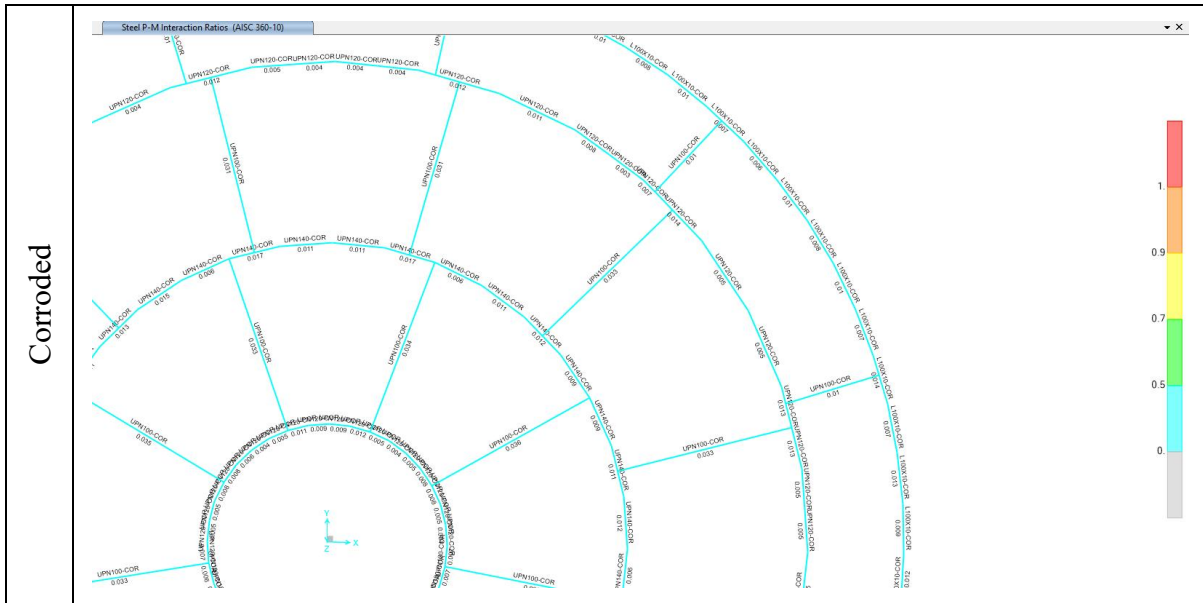


Figure 29: P-M Ratio of the Roof Structure– Floating case - Intact Roof

P-M Ratio for the worst case - NEW

AISC 360-10 STEEL SECTION CHECK (Summary for Combo and Station)
 Units : N, mm, C

Frame : 607 X Mid: -1724.982 Combo: D+BUO Design Type: Beam
 Length: 699.163 Y Mid: -7788.399 Shape: UPN120 Frame Type: OMF
 Loc : 0. Z Mid: 2100. Class: Compact Princpl Rot: 0. degrees

Provision: ASD Analysis: Direct Analysis Reduction: Tau-b Fixed
 D/C Limit=0.95 2nd Order: General 2nd Order EA factor=0.8 EI factor=0.8
 AlphaPr/Py=0.001 AlphaPr/Pe=8E-05 Tau_b=1.

OmegaB=1.67 OmegaC=1.67 OmegaTY=1.67 OmegaTF=2.
 OmegaV=1.67 OmegaV-RI=1.5 OmegaVT=1.67

A=1704. I33=3675168. r33=46.441 S33=61252.8 Av3=990.
 J=35132.17 I22=491416.592 r22=16.982 S22=13084.785 Av2=840.
 E=199947.979 Fy=248.211 Ry=1.5 z33=73152. Cw=1053471116.3
 RLLF=1. Fu=399.896 z22=23668.

STRESS CHECK FORCES & MOMENTS (Combo D+BUO)

Location	Pr	Mr33	Mr22	Vr2	Vr3	Tr
0.	289.914	-1176284.59	-527.26	-1145.366	0.695	1404.426

PMM DEMAND/CAPACITY RATIO (H1.2,H1-1b)
 D/C Ratio: 0.109 = 0. + 0.108 + 0.
 = (1/2) (Pr/Pc) + (Mr33/Mc33) + (Mr22/Mc22)

AXIAL FORCE & BIAXIAL MOMENT DESIGN (H1.2,H1-1b)

Factor	L	K1	K2	B1	B2	Cm
Major Bending	1.	1.	1.	1.	1.	1.
Minor Bending	0.597	1.	1.	1.	1.	1.

LTB

	Lltb	Kltb	Cb
LTB	0.597	1.	1.241

	Pr Force	Pnc/Omega Capacity	Pnt/Omega Capacity
Axial	289.914	241363.931	253264.687

	Mr Moment	Mn/Omega Capacity	Mn/Omega No LTB	Mn/Omega Cb=1
Major Moment	-1176284.59	10872546.02	10872546.02	10872546.02
Minor Moment	-527.26	3111656.215		

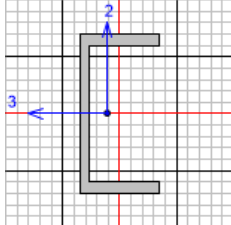
SHEAR CHECK

	Vr	Vn/Omega	Stress	Status
	Force	Capacity	Ratio	Check
Major Shear	1145.366	74909.274	0.015	OK
Minor Shear	0.695	88285.93	7.870E-06	OK

CONNECTION SHEAR FORCES FOR BEAMS

	VMajor	VMajor
	Left	Right
Major (V2)	1145.366	826.358

P-M Ratio for the worst case - CORRODED



AISC 360-10 STEEL SECTION CHECK (Summary for Combo and Station)
 Units : N, mm, C

Frame : 429 X Mid: -3031.51 Combo: D+BUO Design Type: Beam
 Length: 3000. Y Mid: 1749.271 Shape: UPN100-COR Frame Type: OMF
 Loc : 1500. Z Mid: 2100. Class: Compact Princpl Rot: 0. degrees

Provision: ASD Analysis: Direct Analysis
 D/C Limit=0.95 2nd Order: General 2nd Order Reduction: Tau-b Fixed
 AlphaPr/Fy=0.002 AlphaPr/Pe=0.01 Tau_b=1. EA factor=0.8 EI factor=0.8

OmegaB=1.67 OmegaC=1.67 OmegaTY=1.67 OmegaTF=2.
 OmegaV=1.67 OmegaV-RI=1.5 OmegaVT=1.67

A=1187.5 I33=1801690.505 r33=38.951 S33=36582.548 Av3=751.75
 J=17379.428 I22=277359.446 r22=15.283 S22=8617.598 Av2=517.125
 E=199947.979 Fy=248.211 Ry=1.5 z33=43152.469 Cw=401141632.7
 RLLF=1. Fu=399.896 z22=15475.513

STRESS CHECK FORCES & MOMENTS (Combo D+BUO)

Location	Pr	Mr33	Mr22	Vr2	Vr3	Tr
1500.	373.528	192456.318	1.405	-8.991	-0.008	-0.572

PMM DEMAND/CAPACITY RATIO (H1.2,H1-1b)
 D/C Ratio: 0.035 = 0.001 + 0.034 + 0.
 = (1/2) (Pr/Pc) + (Mr33/Mc33) + (Mr22/Mc22)

AXIAL FORCE & BIAXIAL MOMENT DESIGN (H1.2,H1-1b)

Factor	L	K1	K2	B1	B2	Cm
Major Bending	1.	1.	1.	1.	1.	1.
Minor Bending	1.	1.	1.	1.	1.	1.

	Lltb	Kltb	Cb
LTB	1.	1.	1.176

	Pr	Pnc/Omega	Pnt/Omega
	Force	Capacity	Capacity
Axial	373.528	31937.457	176497.545

	Mr	Mn/Omega	Mn/Omega	Mn/Omega
	Moment	Capacity	No LTB	Cb=1
Major Moment	192456.318	5616923.528	6413730.346	4776596.841
Minor Moment	1.405	2049327.11		

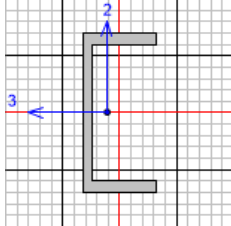
SHEAR CHECK

	Vr	Vn/Omega	Stress	Status
	Force	Capacity	Ratio	Check
Major Shear	8.991	46116.022	0.	OK
Minor Shear	0.008	67039.341	0.	OK

CONNECTION SHEAR FORCES FOR BEAMS

	VMajor	VMajor
	Left	Right
Major (V2)	296.917	278.936

Deflection for the worst case - NEW



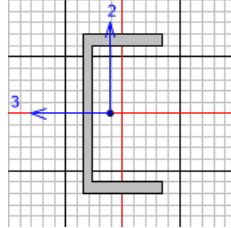
AISC 360-10 STEEL SECTION CHECK (Deflection Details)
 Units : N, mm, C

Frame : 607 X Mid: -1724.982 Combo: def(D+BUO) Design Type: Beam
 Length: 699.163 Y Mid: -7788.399 Shape: UPN120 Frame Type: OMF
 Loc : 0. Z Mid: 2100. Class: Slender Princpl Rot: 0. degrees

DEFLECTION CHECK (Combodef(D+BU))

Type	Consider	Deflection	Limit	Ratio	Status
Dead Load	Yes	0.068	3.496	0.019	OK
Super DL+LL	Yes	0.	3.496	0.	OK
Live Load	Yes	0.	3.496	0.	OK
Total Load	Yes	0.068	3.496	0.019	OK
Total-Camber	Yes	0.068	3.496	0.019	OK

Deflection for the worst case - CORRODED



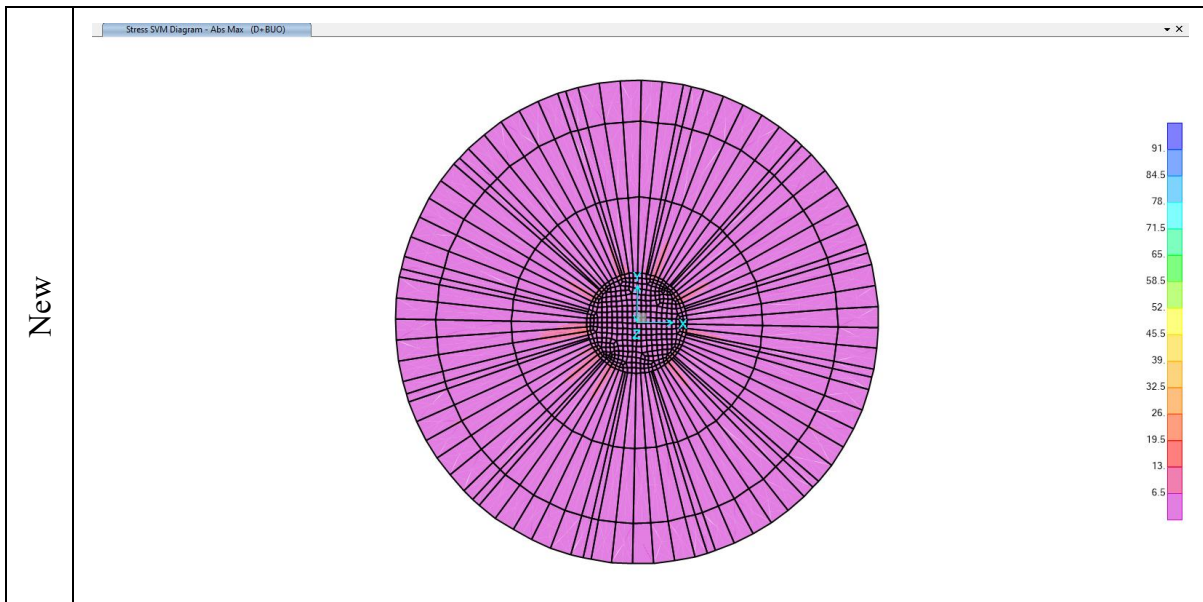
AISC 360-10 STEEL SECTION CHECK (Deflection Details)
 Units : N, mm, C

Frame : 429 X Mid: -3031.51 Combo: def(D+BUO) Design Type: Beam
 Length: 3000. Y Mid: 1749.271 Shape: UPN100-COR Frame Type: OMF
 Loc : 0. Z Mid: 2100. Class: Slender Princpl Rot: 0. degrees

DEFLECTION CHECK (Combodef(D+BU))

Type	Consider	Deflection	Limit	Ratio	Status
Dead Load	Yes	0.476	15.	0.032	OK
Super DL+LL	Yes	0.	15.	0.	OK
Live Load	Yes	0.	15.	0.	OK
Total Load	Yes	0.476	15.	0.032	OK
Total-Camber	Yes	0.476	15.	0.032	OK

(III)Deck Plates



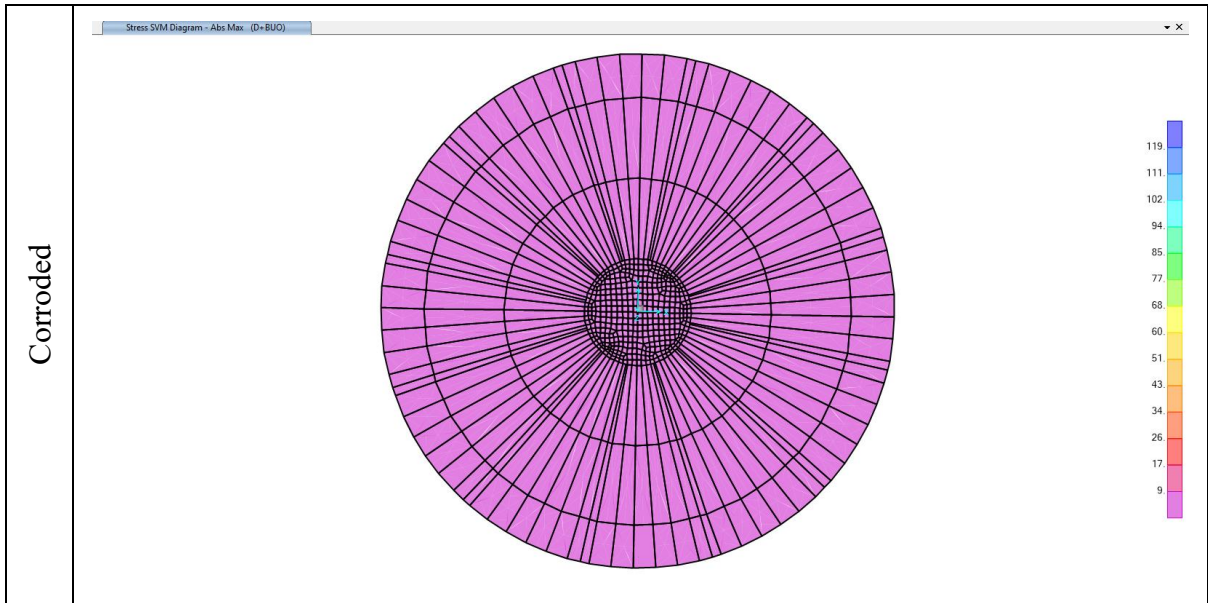
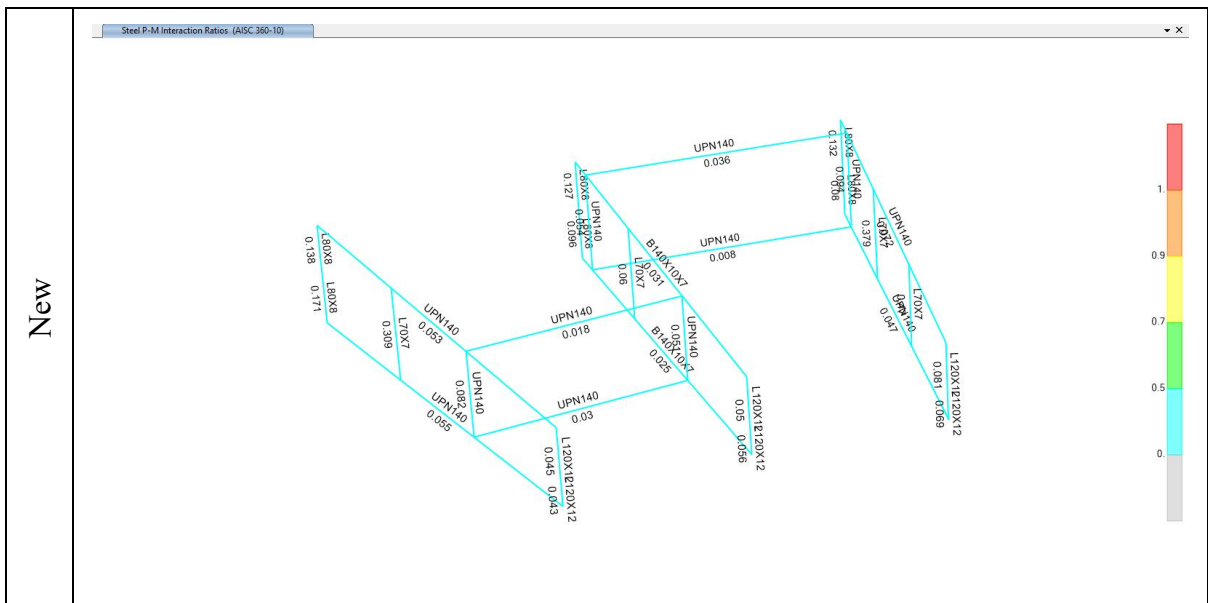


Figure 30: Deck Plate Stress (MPa) – Floating case - Intact Roof

(IV) Pontoon Structure



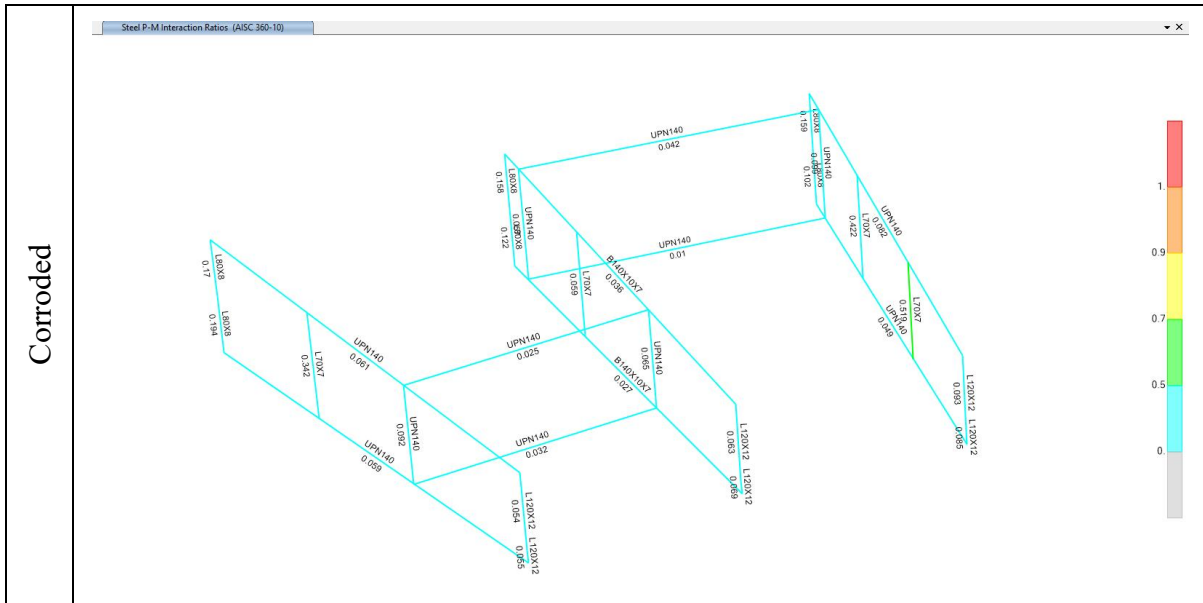


Figure 31: P-M Ratio for Frames in a Pontoon Compartment– Floating case - Intact Roof

P-M Ratio for the worst case - NEW

AISC 360-10 STEEL SECTION CHECK (Summary for Combo and Station)
 Units : N, mm, C

Frame : 601 X Mid: 10289.981 Combo: D+BUO Design Type: Column
 Length: 768.108 Y Mid: 3746.815 Shape: L70X7 Frame Type: OMF
 Loc : 0. Z Mid: 2384.054 Class: Compact Princpl Rot: 45. degrees

Provision: ASD Analysis: Direct Analysis Reduction: Tau-b Fixed
 D/C Limit=0.95 2nd Order: General 2nd Order EA factor=0.8 EI factor=0.8
 AlphaPr/Py=0.027 AlphaPr/Pe=0.01 Tau_b=1.

OmegaB=1.67 OmegaC=1.67 OmegaTY=1.67 OmegaTF=2.
 OmegaV=1.67 OmegaV-RI=1.5 OmegaVT=1.67

A=931. I33=432190.531 r33=21.546 S33=8657.48 Av3=490.
 J=14618.088 I22=432190.531 r22=21.546 S22=8657.48 Av2=490.
 Ixy=-255896.053 Imax=688086.583 rmax=27.186 Smax=14633.103
 Rot= 45. deg Imin=176294.478 rmin=13.761 Smin=6208.444
 E=199947.979 Fy=248.211 Ry=1.5 z33=15597.925
 RLLF=1. Fu=399.896 z22=15597.925

STRESS CHECK FORCES & MOMENTS (Combo D+BUO)

Location	Pr	Mr33	Mr22	Vr2	Vr3	Tr
0.	-3837.806	308244.185	725272.984	535.211	862.036	-187.341

PMM DEMAND/CAPACITY RATIO (H2-1)
 D/C Ratio: 0.47 = 0.033 + 0.224 + 0.213
 = fa/Fa + fbw/Fbw + fbz/Fbz

AXIAL FORCE & BIAXIAL MOMENT DESIGN (H2-1)

Factor	L	K1	K2	B1	B2	Cm
Major Bending	1.	1.	1.	1.	1.	0.585
Minor Bending	1.	1.	1.	1.	1.	0.759

	Litb	Kltb	Cb
LTB	1.	1.	1.

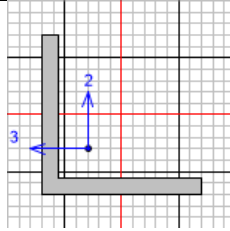
	Pr Force	Pnc/Omega Capacity	Pnt/Omega Capacity
Axial	-3837.806	117441.028	138374.075

	Mr Moment	Mn/Omega Capacity	Mn/Omega Capacity No LTB	Mn/Omega Capacity Cb=1
Major Moment	730806.998	3262366.52	3262366.52	3262366.52
Minor Moment	294883.892	1384137.004		

SHEAR CHECK

			Force	Vr	Vn/Omega	Stress	Status
				Capacity	Ratio	Check	
Major Shear	535.211	43697.076	0.012	OK			
Minor Shear	862.036	43697.076	0.02	OK			

P-M Ratio for the worst case - CORRODED



AISC 360-10 STEEL SECTION CHECK (Summary for Combo and Station)

Units : N, mm, C

Frame : 601 X Mid: 10289.981 Combo: D+BUO Design Type: Column
 Length: 768.108 Y Mid: 3746.815 Shape: L70X7 Frame Type: OMF
 Loc : 0. Z Mid: 2384.054 Class: Compact Princpl Rot: 45. degrees

Provision: ASD Analysis: Direct Analysis Reduction: Tau-b Fixed
 D/C Limit=0.95 2nd Order: General 2nd Order EA factor=0.8 EI factor=0.8
 AlphaPr/Py=0.028 AlphaPr/Pe=0.011 Tau_b=1.

OmegaB=1.67 OmegaC=1.67 OmegaTY=1.67 OmegaTF=2.
 OmegaV=1.67 OmegaV-RI=1.5 OmegaVT=1.67

A=931. I33=432190.531 r33=21.546 S33=8657.48 Av3=490.
 J=14618.088 I22=432190.531 r22=21.546 S22=8657.48 Av2=490.
 Ixy=-255896.053 Imax=688086.583 rmax=27.186 Smax=14633.103
 Rot= 45. deg Imin=176294.478 rmin=13.761 Smin=6208.444
 E=199947.979 Fy=248.211 Ry=1.5 z33=15597.925
 RLLF=1. Fu=399.896 z22=15597.925

STRESS CHECK FORCES & MOMENTS (Combo D+BUO)

Location	Pr	Mr33	Mr22	Vr2	Vr3	Tr
0.	-4050.431	343766.408	804368.164	607.582	981.468	-204.591

PMM DEMAND/CAPACITY RATIO (H2-1)

D/C Ratio: $0.519 = 0.034 + 0.249 + 0.235$
 $= fa/Fa + fbw/Fbw + fbz/Fbz$

AXIAL FORCE & BIAXIAL MOMENT DESIGN (H2-1)

Factor	L	K1	K2	B1	B2	Cm
Major Bending	1.	1.	1.	1.	1.	0.575
Minor Bending	1.	1.	1.	1.	1.	0.751

LTB	Lltb	Kltb	Cb
	1.	1.	1.

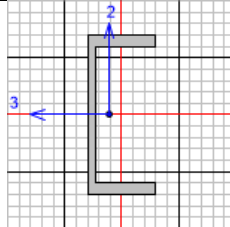
	Pr	Pnc/Omega	Pnt/Omega
	Force	Capacity	Capacity
Axial	-4050.431	117441.028	138374.075

	Mr	Mn/Omega	Mn/Omega	Mn/Omega
	Moment	Capacity	No LTB	Cb=1
Major Moment	811853.741	3262366.52	3262366.52	3262366.52
Minor Moment	325694.626	1384137.004		

SHEAR CHECK

			Force	Vr	Vn/Omega	Stress	Status
				Capacity	Ratio	Check	
Major Shear	607.582	43697.076	0.014	OK			
Minor Shear	981.468	43697.076	0.022	OK			

Deflection for the worst case - NEW



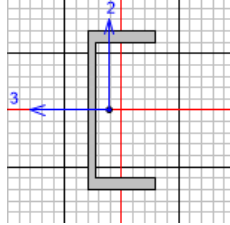
AISC 360-10 STEEL SECTION CHECK (Deflection Details)

Units : N, mm, C

Frame : 19 X Mid: 8869.462 Combo: def(D+BUO) Design Type: Beam
 Length: 3939.983 Y Mid: 7443.774 Shape: UPN140 Frame Type: OMF
 Loc : 0. Z Mid: 2000. Class: Slender Princpl Rot: 0. degrees

DEFLECTION CHECK (Combodef(D+BU))					
Type	Consider	Deflection	Limit	Ratio	Status
Dead Load	Yes	0.441	19.7	0.022	OK
Super DL+LL	Yes	0.	19.7	0.	OK
Live Load	Yes	0.	19.7	0.	OK
Total Load	Yes	0.441	19.7	0.022	OK
Total-Camber	Yes	0.441	19.7	0.022	OK

Deflection for the worst case - CORRODED

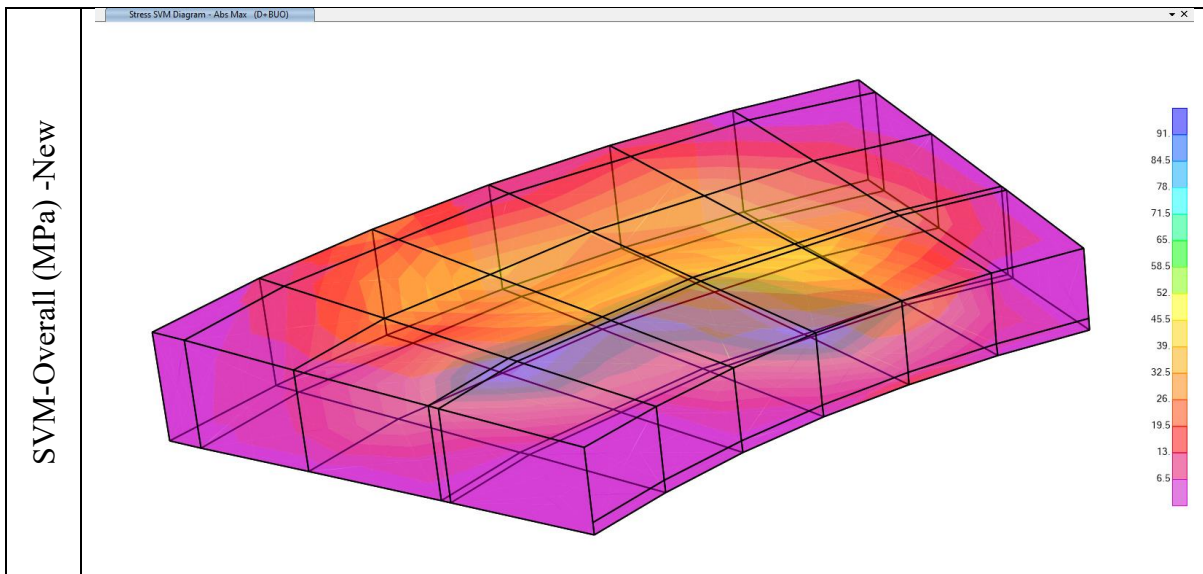


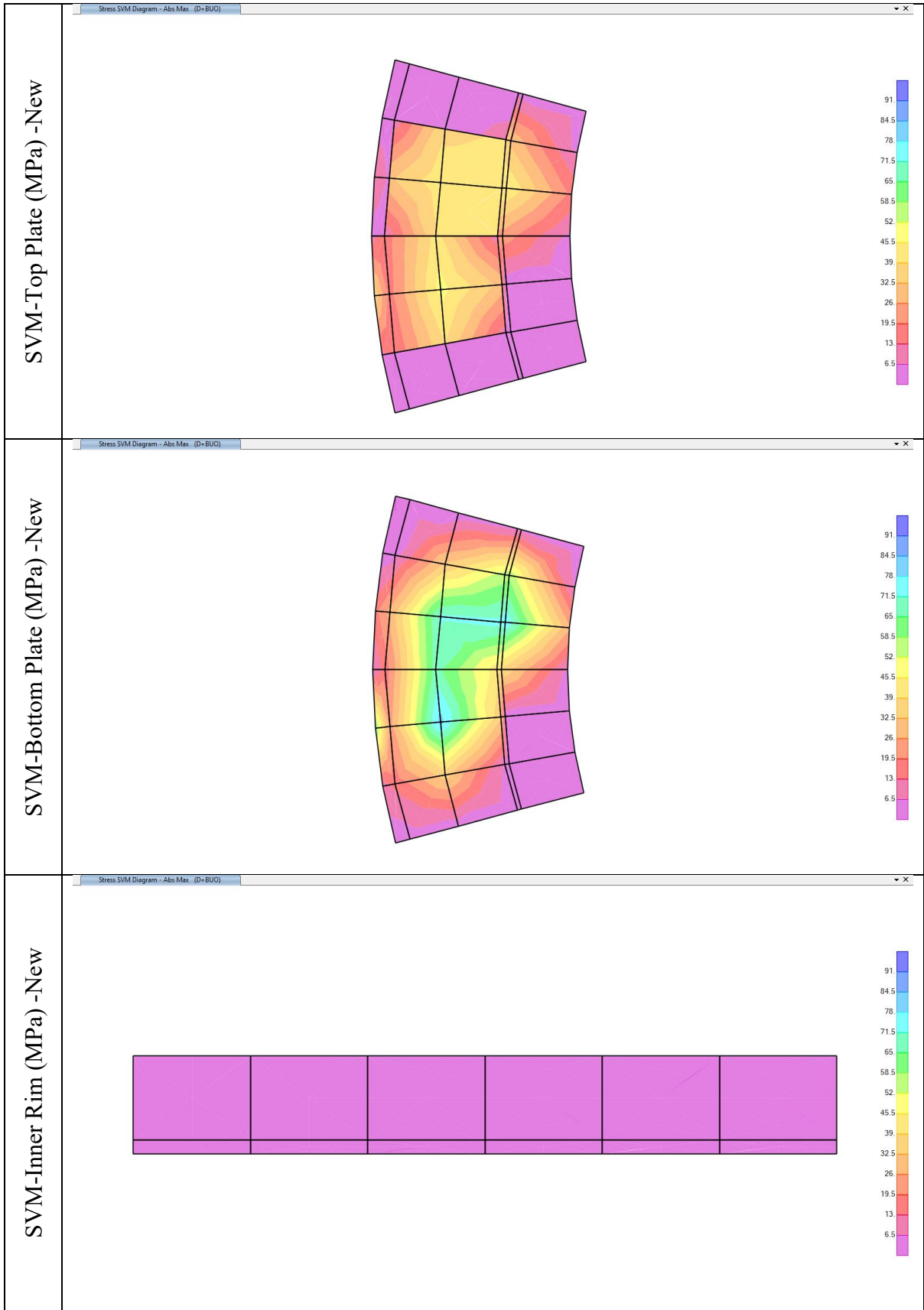
AISC 360-10 STEEL SECTION CHECK (Deflection Details)
Units : N, mm, C

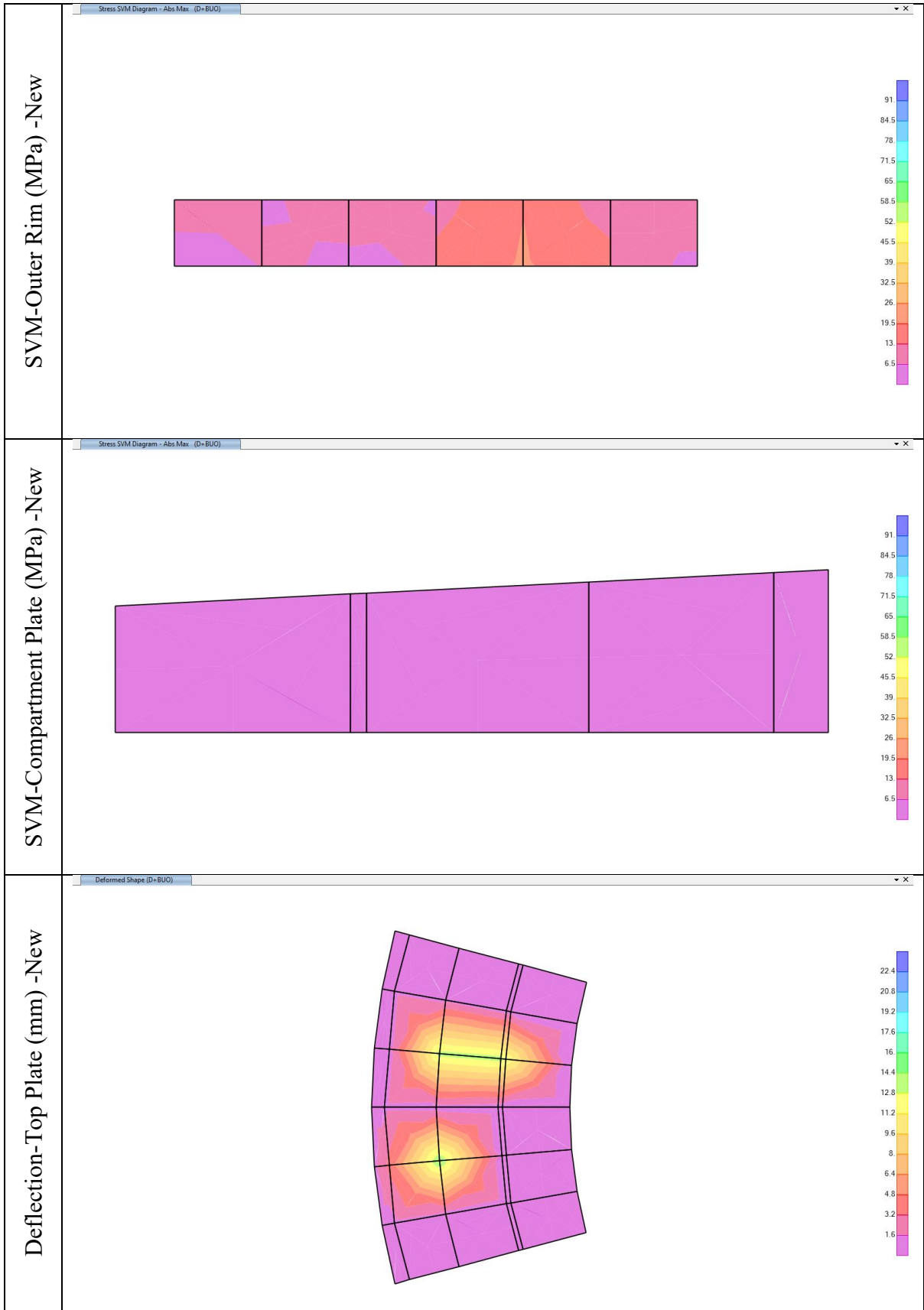
Frame : 19 X Mid: 8869.462 Combo: def(D+BUO) Design Type: Beam
Length: 3939.983 Y Mid: 7443.774 Shape: UPN140 Frame Type: OMF
Loc : 0. Z Mid: 2000. Class: Slender Princpl Rot: 0. degrees

DEFLECTION CHECK (Combodef(D+BU))					
Type	Consider	Deflection	Limit	Ratio	Status
Dead Load	Yes	0.49	19.7	0.025	OK
Super DL+LL	Yes	0.	19.7	0.	OK
Live Load	Yes	0.	19.7	0.	OK
Total Load	Yes	0.49	19.7	0.025	OK
Total-Camber	Yes	0.49	19.7	0.025	OK

(V) Pontoon and Compartment Plates







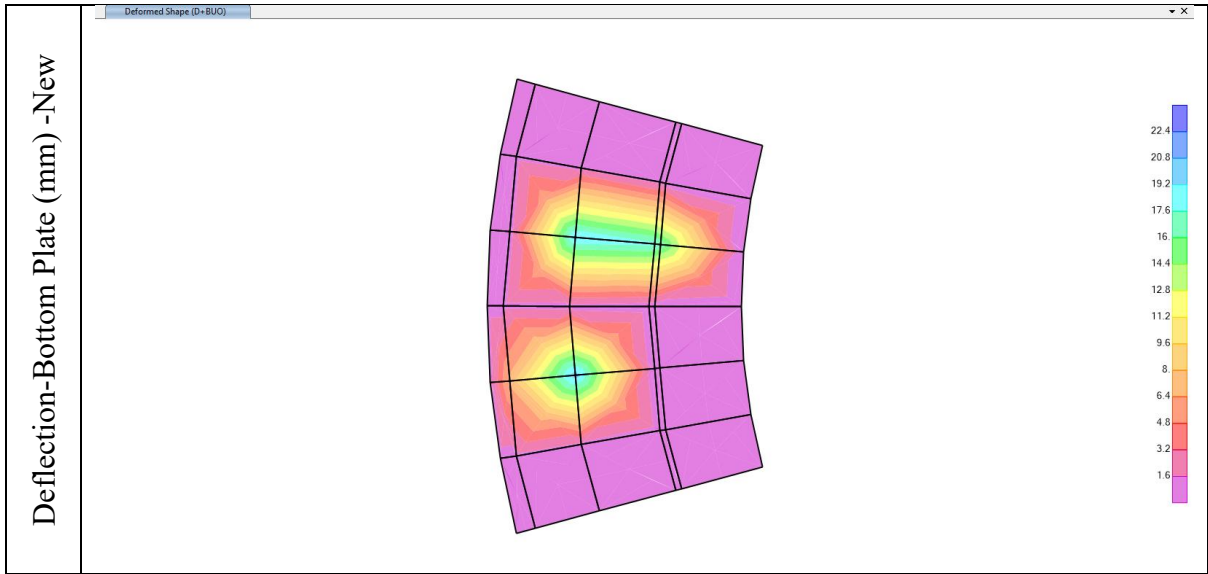
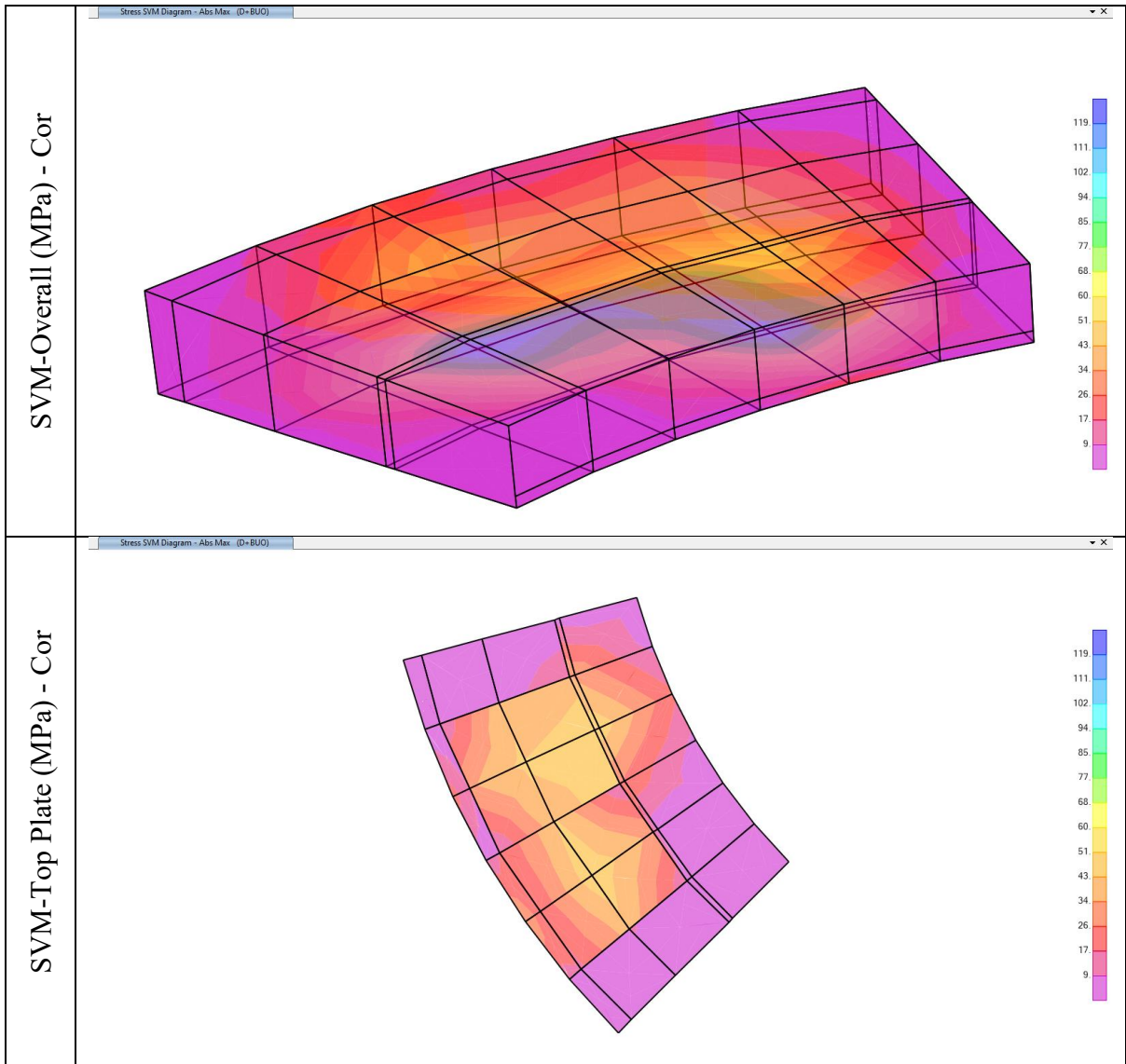
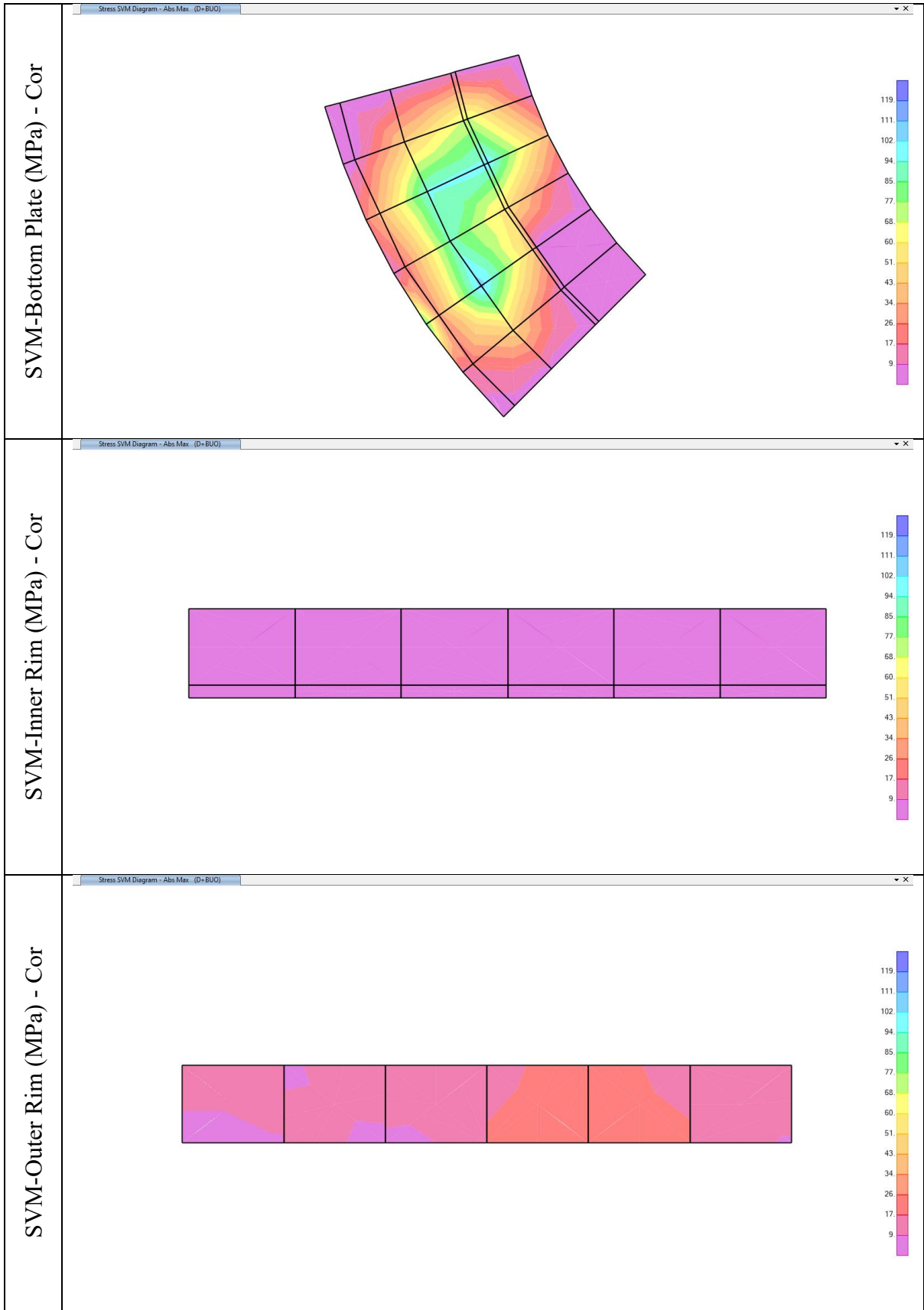


Figure 32: Pontoon Plates Results– Floating case - Intact Roof -New





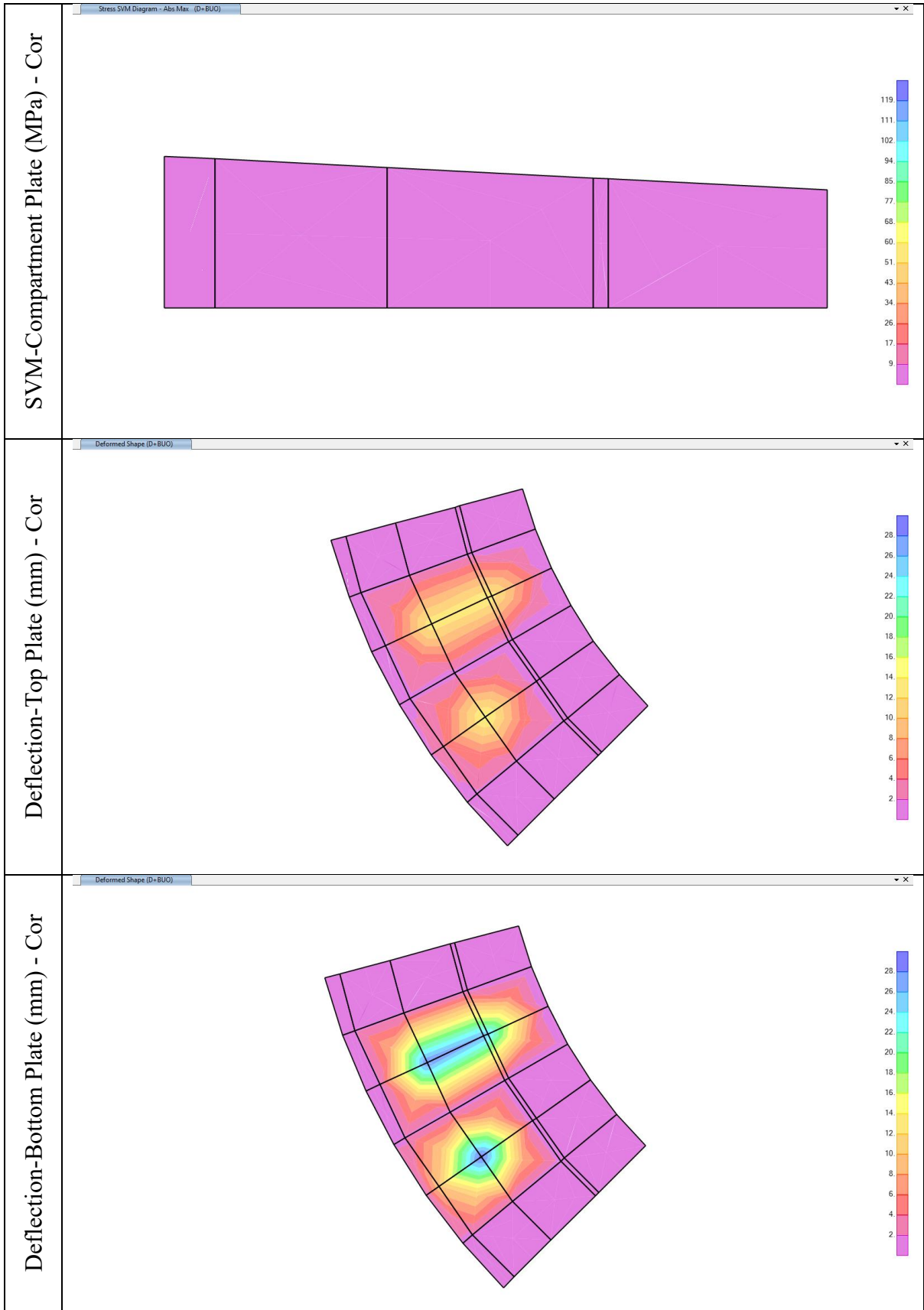


Figure 33: Pontoon Plates Results – Corroded – Floating case - Intact Roof

7.2.2. Punctured Roof

Since no hydrostatic load is applied to the deck section, only pontoon area is analyzed.

(I) Overall view

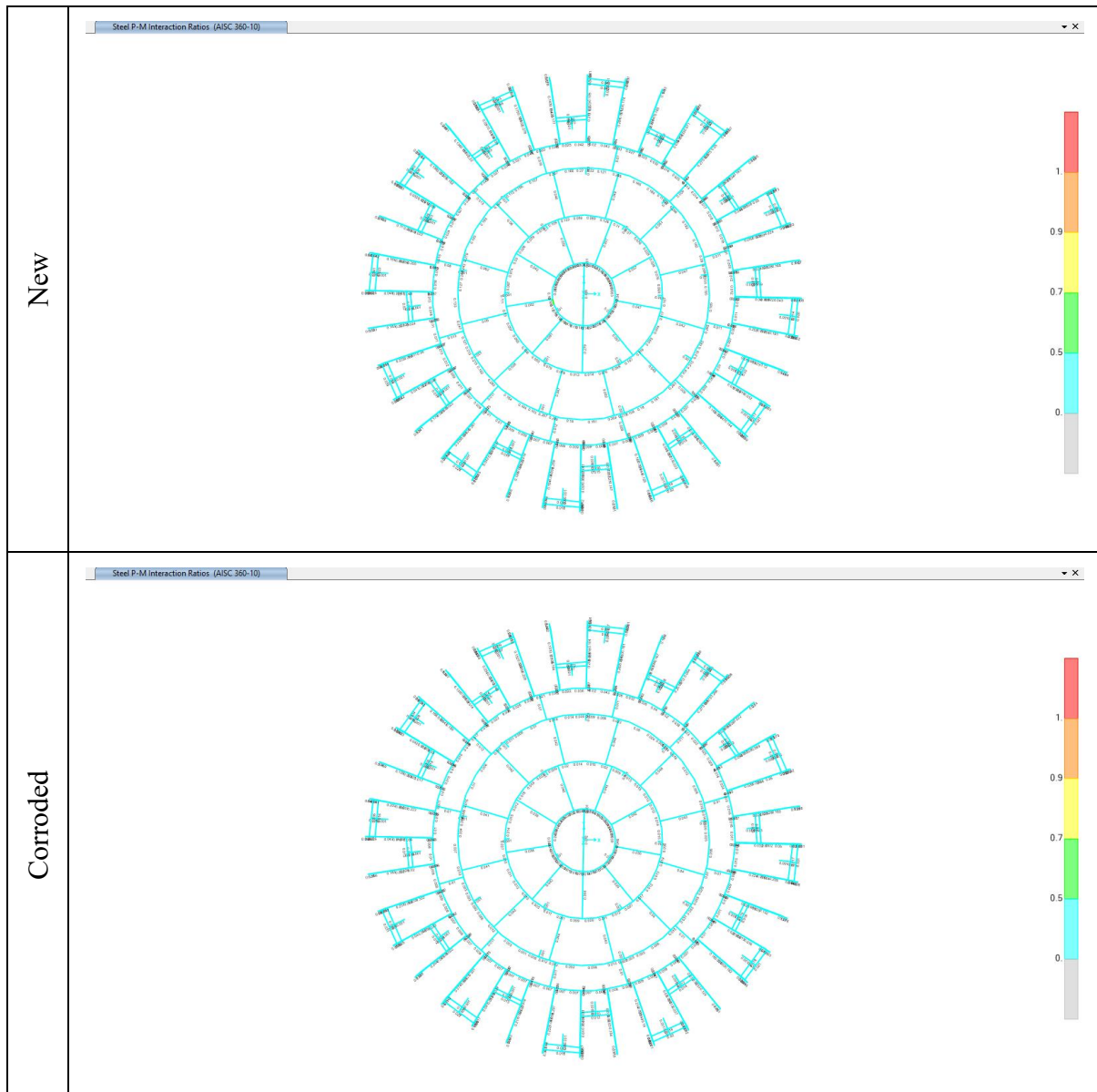


Figure 34: P-M Ratio of the Roof Structure – Floating Case - Punctured

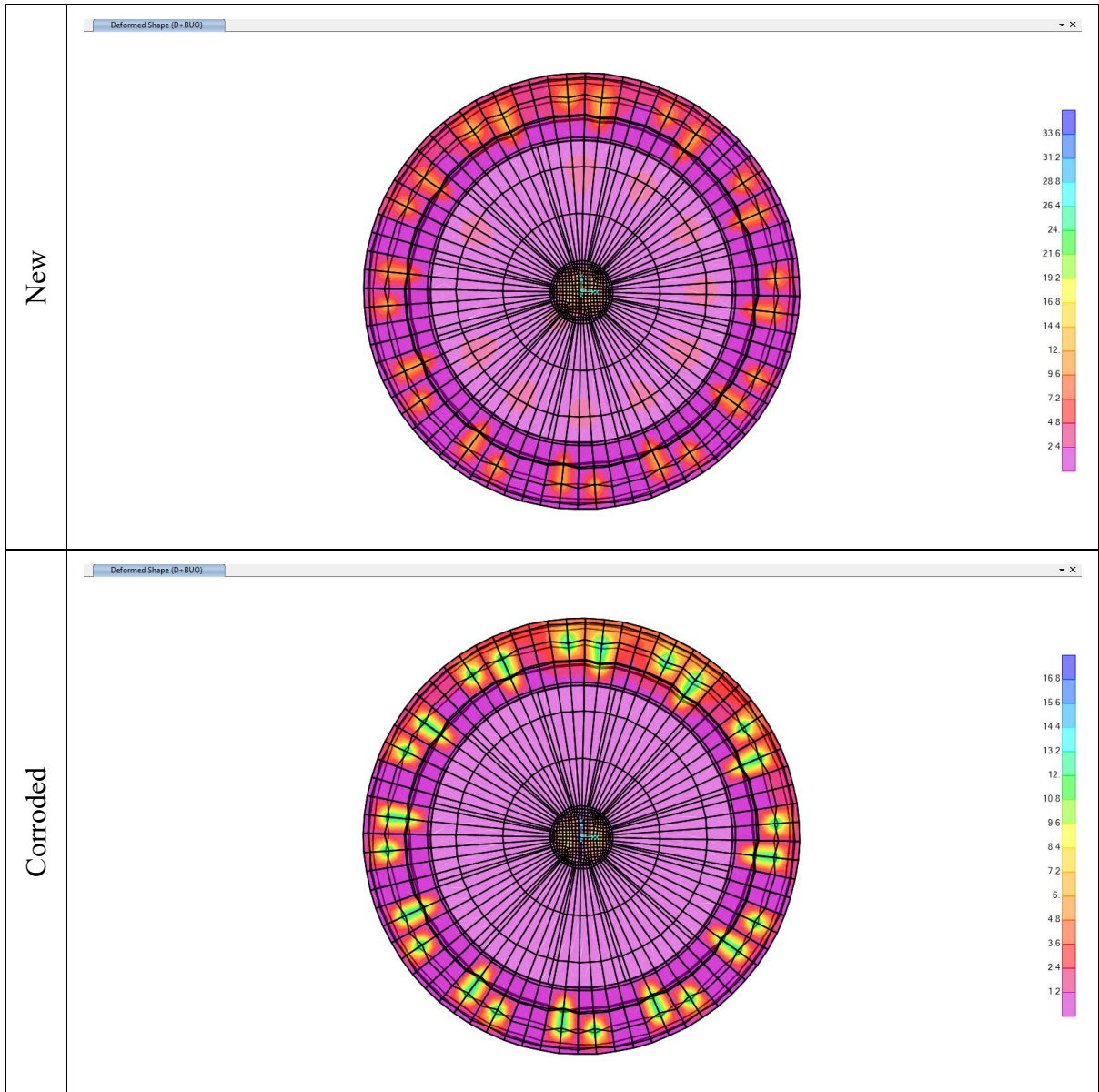


Figure 35: SVM of the Roof Structure (MPa) –Floating Case- Punctured

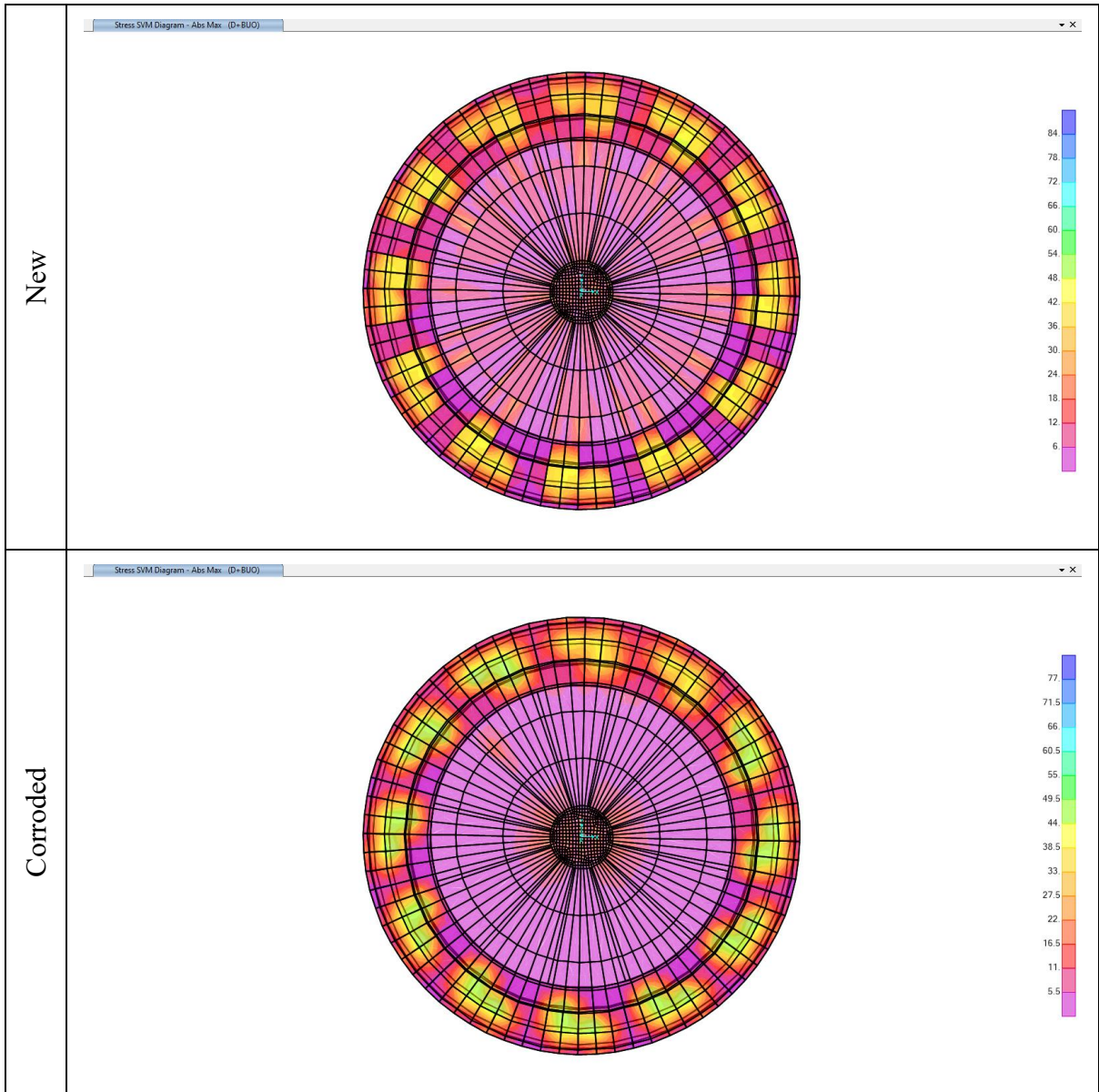


Figure 36: Deflection of Plates (mm) – Floating case- Punctured

(II) Pontoon Frame

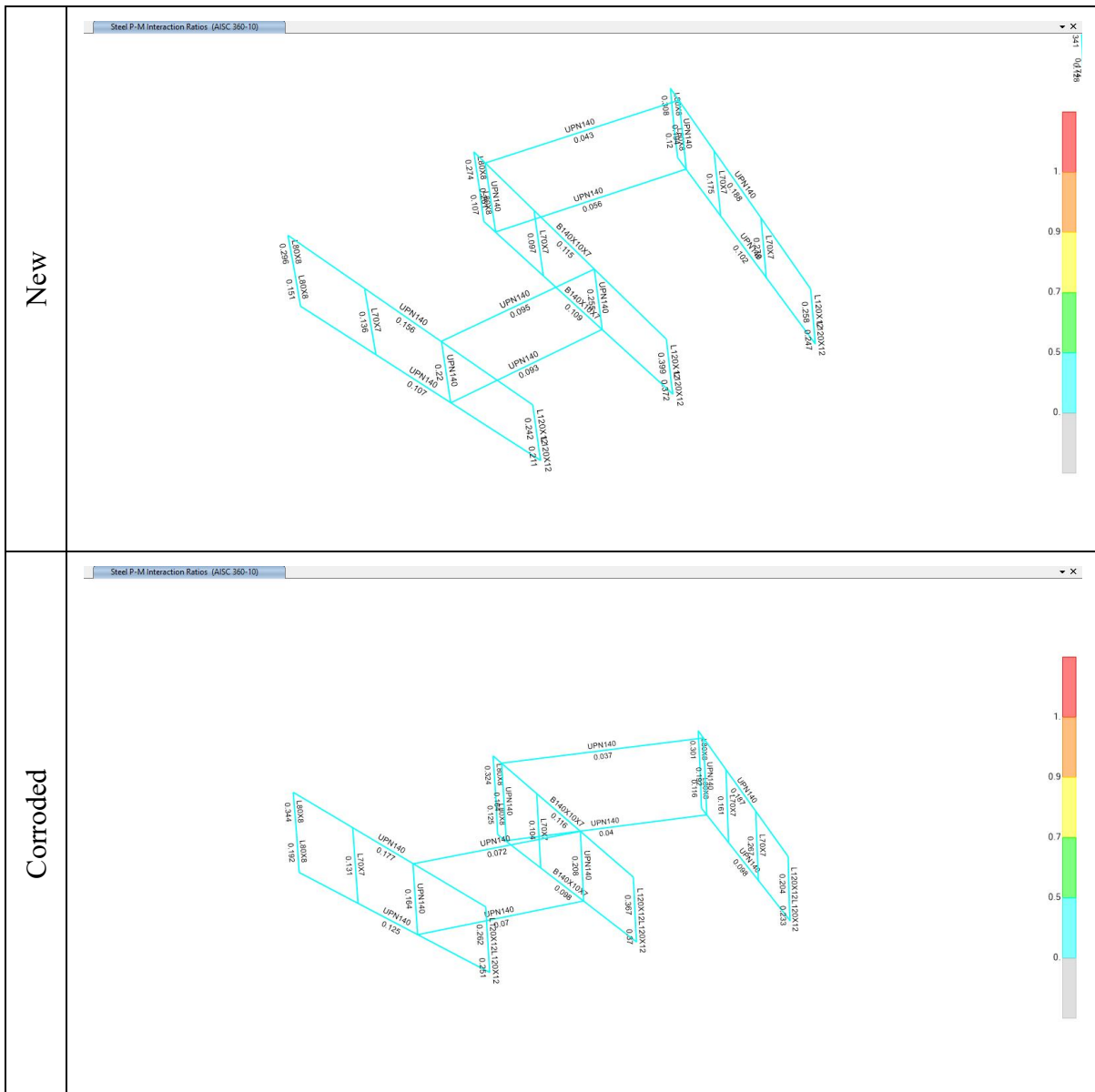
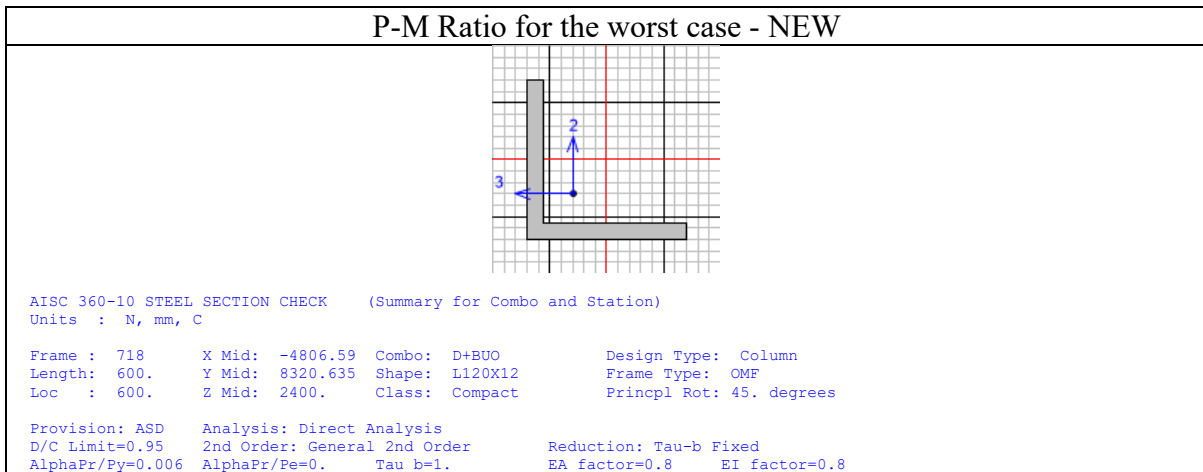


Figure 37: P-M Ratio for Frames in a Pontoon Compartment-Floating Case- Punctured



OmegaB=1.67	OmegaC=1.67	OmegaTY=1.67	OmegaTF=2.	
OmegaV=1.67	OmegaV-RI=1.5	OmegaVT=1.67		
A=2736.	I33=3732570.947	r33=36.936	S33=43615.528	Av3=1440.
J=126247.68	I22=3732570.947	r22=36.936	S22=43615.528	Av2=1440.
Ixy=-2210021.05	Imax=5942592.	rmax=46.605	Smax=73720.125	
Rot= 45. deg	Imin=1522549.89	rmin=23.59	Smin=31277.526	
E=199947.979	Fy=248.211	Ry=1.5	z33=78580.8	
RLLF=1.	Fu=399.896		z22=78580.8	

STRESS CHECK FORCES & MOMENTS (Combo D+BUO)

Location	Pr	Mr33	Mr22	Vr2	Vr3	Tr
600.	-2434.149	-305078.735	2590300.036	704.471	-7518.267	-377.42

PMM DEMAND/CAPACITY RATIO (H2-1)

D/C Ratio: 0.399 = 0.007 + 0.098 + 0.294
= fa/Fa + fbw/Fbw + fbz/Fbz

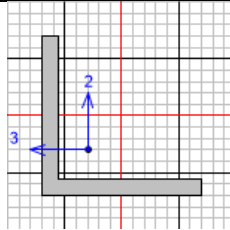
AXIAL FORCE & BIAXIAL MOMENT DESIGN (H2-1)

Factor	L	K1	K2	B1	B2	Cm
Major Bending	1.	1.	1.	1.	1.	0.284
Minor Bending	1.	1.	1.	1.	1.	0.318
	Lltb	Kltb	Cb			
LTB	1.	1.	1.			
	Pr	Pnc/Omega	Pnt/Omega			
	Force	Capacity	Capacity			
Axial	-2434.149	360423.678	406650.343			
	Mr	Mn/Omega	Mn/Omega	Mn/Omega		
	Moment	Capacity	No LTB	Cb=1		
Major Moment	1615895.478	16435479.14	16435479.14	16435479.14		
Minor Moment	2047341.963	6973145.024				

SHEAR CHECK

	Vr	Vn/Omega	Stress	Status
	Force	Capacity	Ratio	Check
Major Shear	704.471	128415.898	0.005	OK
Minor Shear	7518.267	128415.898	0.059	OK

P-M Ratio for the worst case - CORRODED



AISC 360-10 STEEL SECTION CHECK (Summary for Combo and Station)

Units : N, mm, C

Frame : 263	X Mid: -2.312	Combo: D+BUO	Design Type: Column
Length: 100.	Y Mid: 9609.177	Shape: L120X12	Frame Type: OMF
Loc : 0.	Z Mid: 2050.	Class: Compact	Princpl Rot: 45. degrees

Provision: ASD Analysis: Direct Analysis
D/C Limit=0.95 2nd Order: General 2nd Order Reduction: Tau-b Fixed
AlphaPr/Py=0.006 AlphaPr/Pe=1E-05 Tau_b=1. EA factor=0.8 EI factor=0.8

OmegaB=1.67	OmegaC=1.67	OmegaTY=1.67	OmegaTF=2.	
OmegaV=1.67	OmegaV-RI=1.5	OmegaVT=1.67		
A=2736.	I33=3732570.947	r33=36.936	S33=43615.528	Av3=1440.
J=126247.68	I22=3732570.947	r22=36.936	S22=43615.528	Av2=1440.
Ixy=-2210021.05	Imax=5942592.	rmax=46.605	Smax=73720.125	
Rot= 45. deg	Imin=1522549.89	rmin=23.59	Smin=31277.526	
E=199947.979	Fy=248.211	Ry=1.5	z33=78580.8	
RLLF=1.	Fu=399.896		z22=78580.8	

STRESS CHECK FORCES & MOMENTS (Combo D+BUO)

Location	Pr	Mr33	Mr22	Vr2	Vr3	Tr
0.	2672.264	-565505.626	-2741574.58	1385.094	-2382.62	-617.152

PMM DEMAND/CAPACITY RATIO (H2-1)

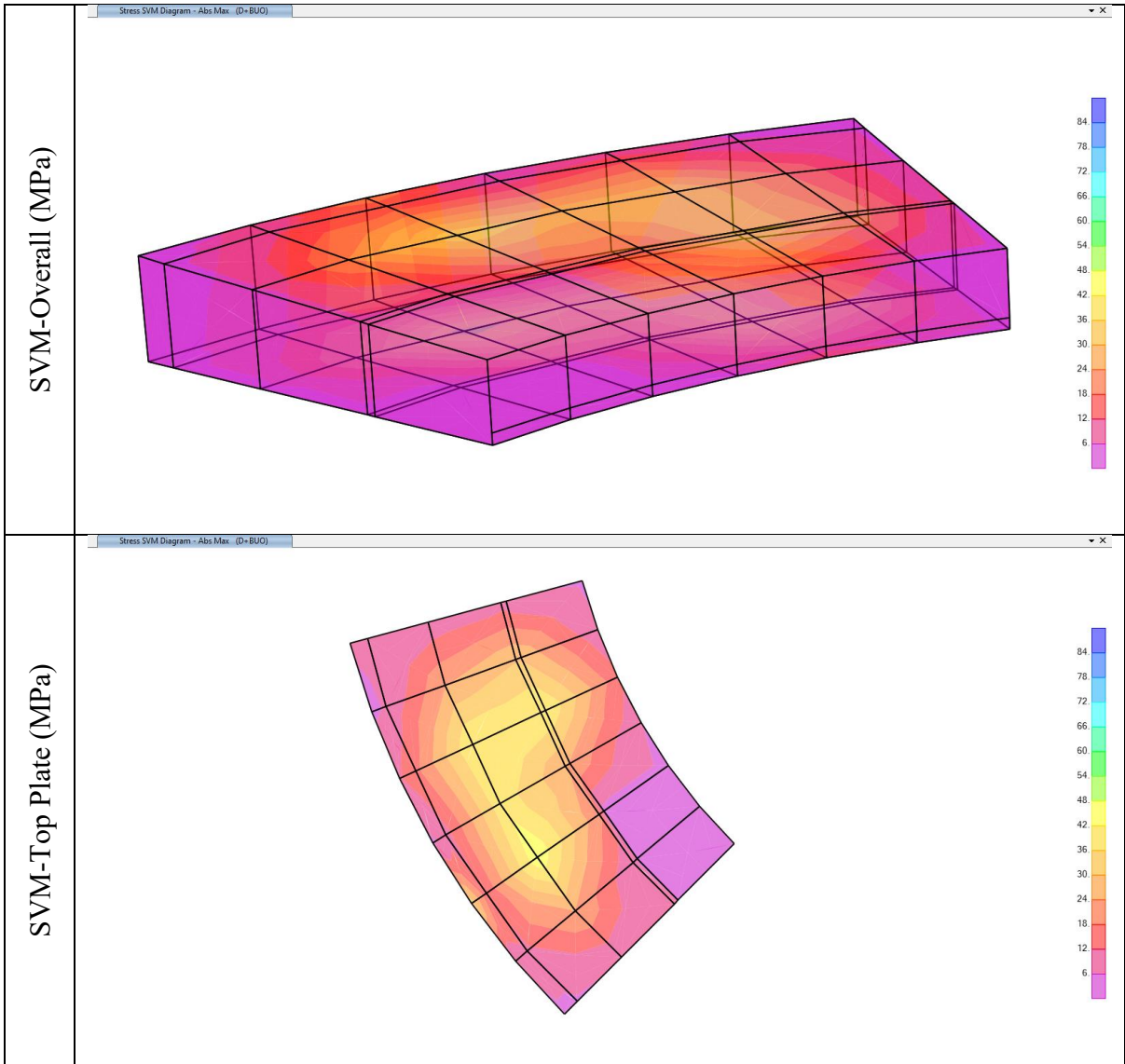
D/C Ratio: 0.37 = 0.007 + 0.142 + 0.221
= fa/Fa + fbw/Fbw + fbz/Fbz

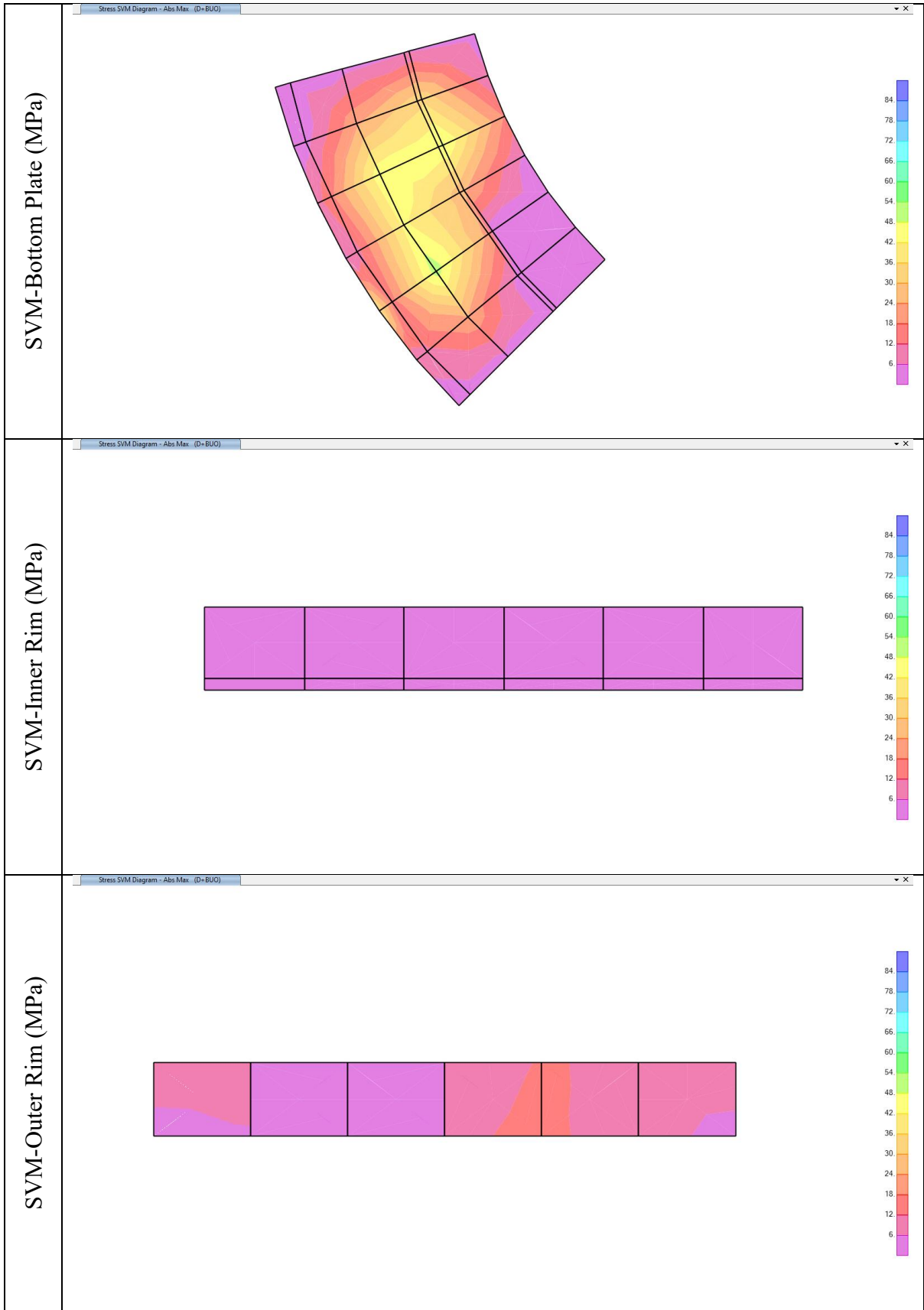
AXIAL FORCE & BIAXIAL MOMENT DESIGN (H2-1)

Factor	L	K1	K2	B1	B2	Cm
Major Bending	1.	1.	1.	1.	1.	1.
Minor Bending	1.	1.	1.	1.	1.	1.
	Lltb	Kltb	Cb			
LTB	1.	1.	1.			
	Pr	Pnc/Omega	Pnt/Omega			

	Force	Capacity	Capacity
Axial	2672.264	393551.64	406650.343
	Mr	Mn/Omega	Mn/Omega
	Moment	Capacity	No LTB
Major Moment	-2338458.84	16435479.14	16435479.14
Minor Moment	-1538713.12	6973145.024	
SHEAR CHECK			
		Vr	Vn/Omega
		Force	Capacity
Major Shear	1385.094	128415.898	0.011
Minor Shear	2382.62	128415.898	0.019
			Status
		Stress	Check
		Ratio	
			OK
			OK

(III) Pontoon Plates - Intact Compartment





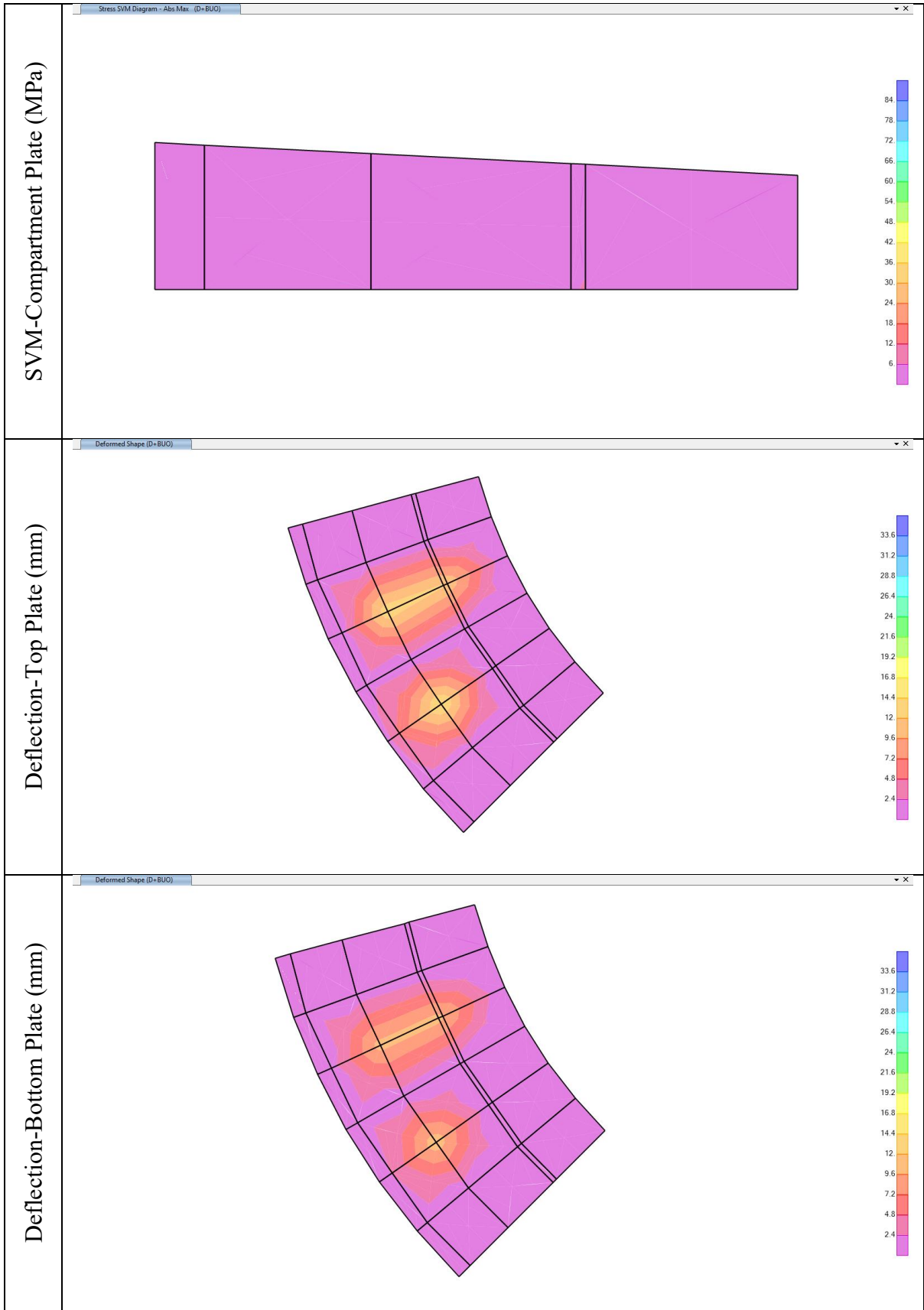
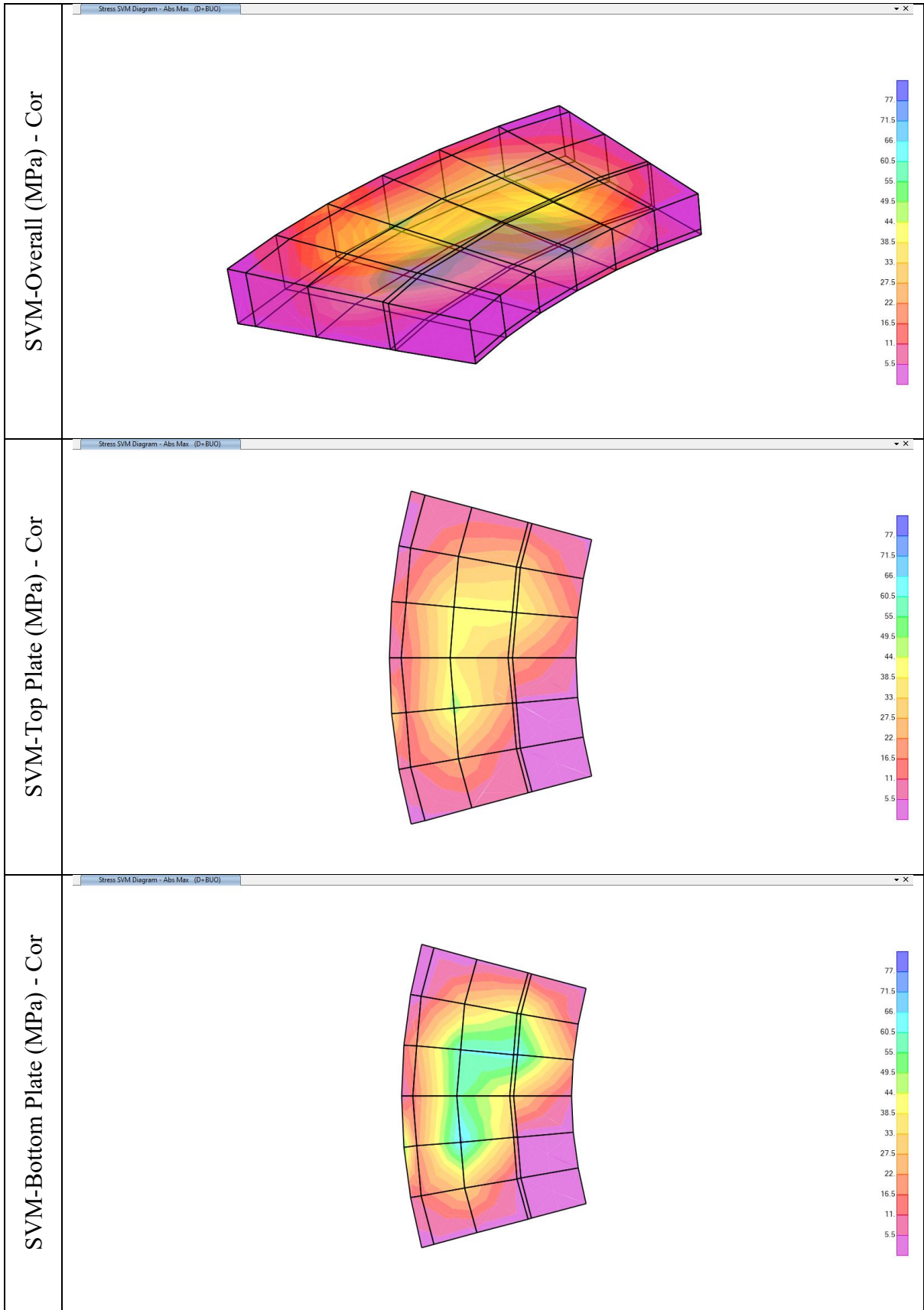
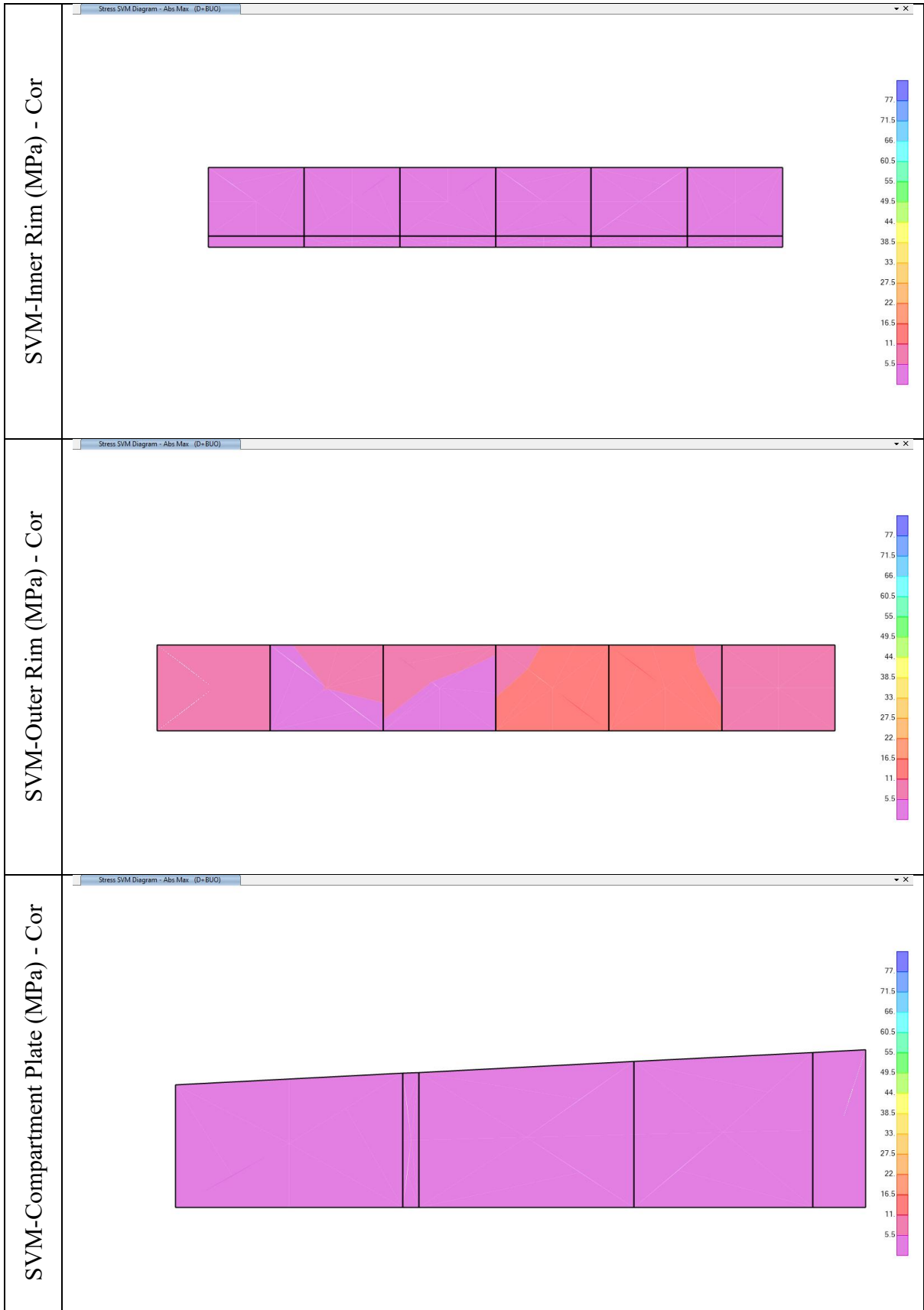


Figure 38: Pontoon Plates Results - Floating Case - Punctured - New





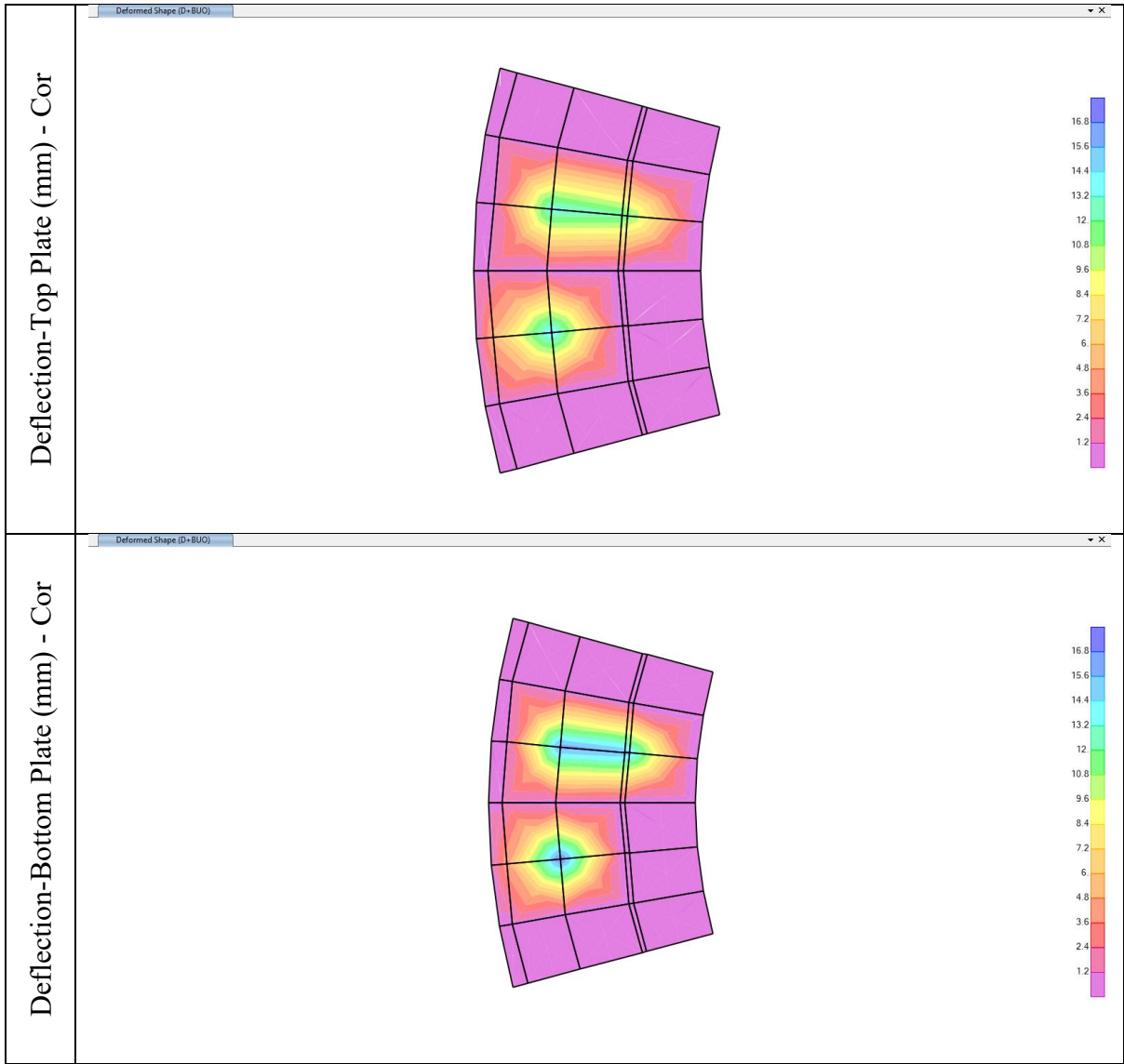


Figure 39: Pontoon Plates Results - Floating Case - Punctured - Corroded

8. Feedback Data to Mechanical Design

Table 5: Roof Structure Approximate Weight

Object Type	Material	Total Weight
Text	Text	kgf
Frame	A53GrB	1614.59
Frame	A36	12918.09
Area	A283C	54876.47
Total		69410

9. Native File Index

Case	File Name
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PROJECT NO: A238		Page 60 of 61

Maintenance Case - New	TK-2050-FloatingRoof-211022
Maintenance Case - Corroded	TK-2050-FloatingRoof-211022-COR
Floating Case - Intact	TK-2050-FloatingRoof-211022-FI
Floating Case - Intact- Corroded	TK-2050-FloatingRoof-211022-FIC
Floating Case - Punctured	TK-2050-FloatingRoof-211022-FP
Floating Case - Punctured	TK-2050-FloatingRoof-211022-FPC