

**CODE****10.7 — Deep flexural members**

**10.7.1** — Flexural members with overall depth to clear span ratios greater than  $\frac{2}{5}$  for continuous spans, or  $\frac{4}{5}$  for simple spans, shall be designed as deep flexural members taking into account nonlinear distribution of strain and lateral buckling. (See also 12.10.6.)

**10.7.2** — Shear strength of deep flexural members shall be in accordance with 11.8.

**10.7.3** — Minimum flexural tension reinforcement shall conform to 10.5.

**10.7.4** — Minimum horizontal and vertical reinforcement in the side faces of deep flexural members shall be the greater of the requirements of 11.8.8, 11.8.9, and 11.8.10 or 14.3.2 and 14.3.3.

**10.8 — Design dimensions for compression members****10.8.1 — Isolated compression member with multiple spirals**

Outer limits of the effective cross section of a compression member with two or more interlocking spirals shall be taken at a distance outside the extreme limits of the spirals equal to the minimum concrete cover required by 7.7.

**10.8.2 — Compression member built monolithically with wall**

Outer limits of the effective cross section of a spirally reinforced or tied reinforced compression member built monolithically with a concrete wall or pier shall be taken not greater than  $1\frac{1}{2}$  in. outside the spiral or tie reinforcement.

**10.8.3 — Equivalent circular compression member**

As an alternative to using the full gross area for design of a compression member with a square, octagonal, or other shaped cross section, it shall be permitted to use a circular section with a diameter equal to the least lateral dimension of the actual shape. Gross area considered, required percentage of reinforcement, and design strength shall be based on that circular section.

**10.8.4 — Limits of section**

For a compression member with a cross section larger than required by considerations of loading, it shall be permitted to base the minimum reinforcement and

**COMMENTARY****R10.7 — Deep flexural members**

The code does not contain detailed requirements for designing deep beams for flexure except that nonlinearity of strain distribution and lateral buckling must be considered.

Suggestions for the design of deep beams for flexure are given in References 10.17, 10.18, and 10.19.

**R10.8 — Design dimensions for compression members**

With the 1971 edition of the ACI Building Code, minimum sizes for compression members were eliminated to allow wider utilization of reinforced concrete compression members in smaller size and lightly loaded structures, such as low rise residential and light office buildings. The engineer should recognize the need for careful workmanship, as well as the increased significance of shrinkage stresses with small sections.

**R10.8.2, R10.8.3, R10.8.4** — For column design,<sup>10.20</sup> the code provisions for quantity of reinforcement, both vertical and spiral, are based on the gross column area and core area, and the design strength of the column is based on the gross area of the column section. In some cases, however, the gross area is larger than necessary to carry the factored load. The basis of 10.8.2, 10.8.3, and 10.8.4 is that it is satisfactory to design a column of sufficient size to carry the factored load and then simply add concrete around the designed section without increasing the reinforcement to meet the minimum percentages required by 10.9.1. The additional concrete must not be considered as carrying load; however, the effects of the additional concrete on member stiffness must be included in the structural analysis. The effects of the additional concrete also must be considered in design of the other parts of the structure that interact with the oversize member.

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strength on a reduced effective area  $A_g$  not less than one-half the total area. This provision shall not apply in regions of high seismic risk.

### 10.9 — Limits for reinforcement of compression members

**10.9.1** — Area of longitudinal reinforcement for non-composite compression members shall be not less than 0.01 nor more than 0.08 times gross area  $A_g$  of section.

## COMMENTARY

ABC ZONES 3,4

### R10.9 — Limits for reinforcement of compression members

**R10.9.1** — This section prescribes the limits on the amount of longitudinal reinforcement for noncomposite compression members. If the use of high reinforcement ratios would involve practical difficulties in the placing of concrete, a lower percentage and hence a larger column, or higher strength concrete or reinforcement (see R9.4) should be considered. The percentage of reinforcement in columns should usually not exceed 4 percent if the column bars are required to be lap spliced.

**Minimum reinforcement.** Since the design methods for columns incorporate separate terms for the load carried by concrete and by reinforcement, it is necessary to specify some minimum amount of reinforcement to ensure that only reinforced concrete columns are designed by these procedures. Reinforcement is necessary to provide resistance to bending, which may exist whether or not computations show that bending exists, and to reduce the effects of creep and shrinkage of the concrete under sustained compressive stresses. Tests have shown that creep and shrinkage tend to transfer load from the concrete to the reinforcement, with a consequent increase in stress in the reinforcement, and that this increase is greater as the ratio of reinforcement decreases. Unless a lower limit is placed on this ratio, the stress in the reinforcement may increase to the yield level under sustained service loads. This phenomenon was emphasized in the report of ACI Committee 105<sup>10,21</sup> and minimum reinforcement ratios of 0.01 and 0.005 were recommended for spiral and tied columns, respectively. However, in all editions of the code since 1936, the minimum ratio has been 0.01 for both types of laterally reinforced columns.

**Maximum reinforcement.** Extensive tests of the ACI column investigation<sup>10,21</sup> included reinforcement ratios no greater than 0.06. Although other tests with as much as 17 percent reinforcement in the form of bars produced results similar to those obtained previously, it is necessary to note that the loads in these tests were applied through bearing plates on the ends of the columns and the problem of transferring a proportional amount of the load to the bars was thus minimized or avoided. Maximum ratios of 0.08 and 0.03 were recommended by ACI Committee 105<sup>10,21</sup> for spiral and tied columns, respectively. In the 1936 ACI Building Code, these limits were made 0.08 and 0.04, respectively. In the 1956 code, the limit for tied columns with bending was raised to 0.08. Since the 1963 code, it has been required that bending be considered in the design of all