

- $C$  is the effective thermal capacity of winding, in watt-hours per K (Wh/K),  
 =  $(0,25 \times \text{mass of aluminium conductor in kilograms (kg)}) + (0,408 \times \text{mass of epoxy and other winding insulation in kilograms (kg)})$ , or  
 =  $(0,107 \times \text{mass of copper conductor in kilograms (kg)}) + (0,408 \times \text{mass of epoxy and other winding insulation in kilograms (kg)})$ ;
- $P_r$  is the winding total losses (resistive losses + eddy losses) at rated load and rated temperature rise, in watts (W);
- $\Delta\vartheta_{HS,r}$  is the winding hot-spot temperature rise at rated load, in Kelvin (K);
- $\vartheta_e$  is the core contribution to winding hot-spot temperature rise at no load. This value should be the value given below or the value measured by the manufacturer during the temperature rise test on the transformer.  
 = 5 K for outer winding (usually HV)  
 = 25 K for inner winding (usually LV less than 1 kV).

NOTE 1 The core contribution values above are based on manufacturers' experience.

NOTE 2 Other winding insulation material and kind of epoxy material can be used. For such transformers the correspondent specific heat values of 24,5 Wmin/K and /kg (or 0,408 Wh/K and per kg) can be replaced by the values based on the manufacturer's experience.

### 5.10.3 Time constant test method

Time constants may also be estimated from the hot resistance cooling curve obtained during thermal tests.

### 5.11 Determination of winding time constant according to empirical constant

When the temperature rise changes, the time constant varies according to the empirical constant  $m$ .

$$\tau_R = \frac{C(\Delta\vartheta_{HS,r} - \vartheta_e)}{P_r} \quad (17)$$

If  $m$  is equal to 1, Equation (17) is correct for any load and any starting temperature. If  $m$  is not equal to 1, the time constant for any load and for any starting temperature for either a heating cycle or a cooling cycle is given by Equation (18).

$$\tau = \tau_R \frac{\left( \frac{\Delta\vartheta_U}{\Delta\vartheta_{HS,r}} \right) - \left( \frac{\Delta\vartheta_i}{\Delta\vartheta_{HS,r}} \right)}{\left( \frac{\Delta\vartheta_U}{\Delta\vartheta_{HS,r}} \right)^{\frac{1}{m}} - \left( \frac{\Delta\vartheta_i}{\Delta\vartheta_{HS,r}} \right)^{\frac{1}{m}}} \quad (18)$$

### 5.12 Calculation of loading capability

Equations (10) through (18) should be used to determine hot-spot temperatures during a load cycle. They should also be used to determine the short-time or continuous loading, which results in the maximum temperatures given in Table 1 or any other limiting temperatures.

The initial hot-spot temperature rise for the initial loading factor  $I_i$  should be obtained from Equation (11) and is determined as follows:

$$\Delta\vartheta_i = \Delta\vartheta_{HS,r} [I_i]^{2m} \quad (19)$$

where