

Burns & McDonnell

Dynamic Foundations:

Basics of Analysis & Design

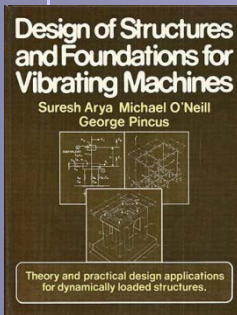
- Resources
- Types of Machines & Foundations
- When is Dynamic Analysis Required?
- What is Dynamic Analysis?
  - Basics of Dynamics
  - Preliminary Design
  - Machine Manufacturer Criteria
  - Detailed Analysis & Design
- Construction Considerations
- Questions



- ACI 351.3R-04. “Foundations for Dynamic Equipment.” American Concrete Institute, 2004.



- El Naggar, M.H. “Design of Machine Foundations- Lecture Notes.” Geotechnical Research Center, Department of Civil and Environmental Engineering, University of Western Ontario.  
<http://www.engga.uwo.ca/People/helnaggar/default.htm>



- Arya, Suresh; O’Neil, Michael, & Pincus, George. “Design of Structures and Foundations for Vibrating Machines.” Gulf Publishing Co, June 1979.

# Types of Dynamic Machines

## Pumps



# Types of Dynamic Machines

## Fans





# Types of Dynamic Machines

## Turbine Generators



# Types of Foundations

Block vs. Table Top  
Piles vs. Soil supported





# When is dynamic analysis required?

The level of analysis required is primarily dictated by the design requirements and performance parameters provided by the machine manufacturer.

Varying levels of dynamic analysis include:

1. Mass Ratio (Fdn wt : equipment wt)
2. Frequency Analysis
3. Forced Response Analysis



# What is the approach to dynamic analysis?

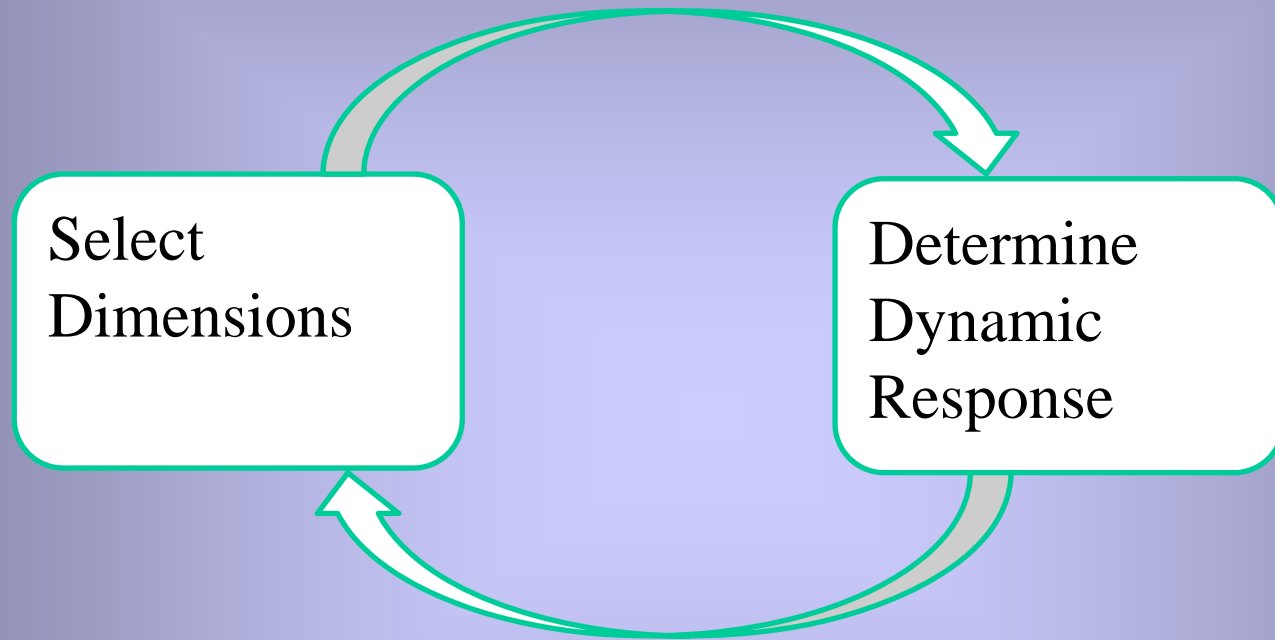


Figure 2.1: Basic Model of Single Degree of Freedom System

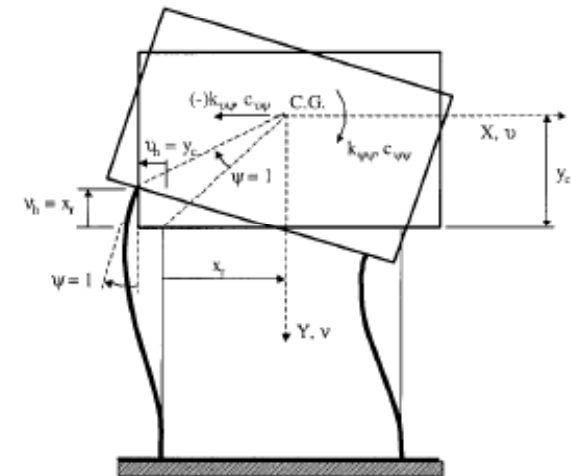
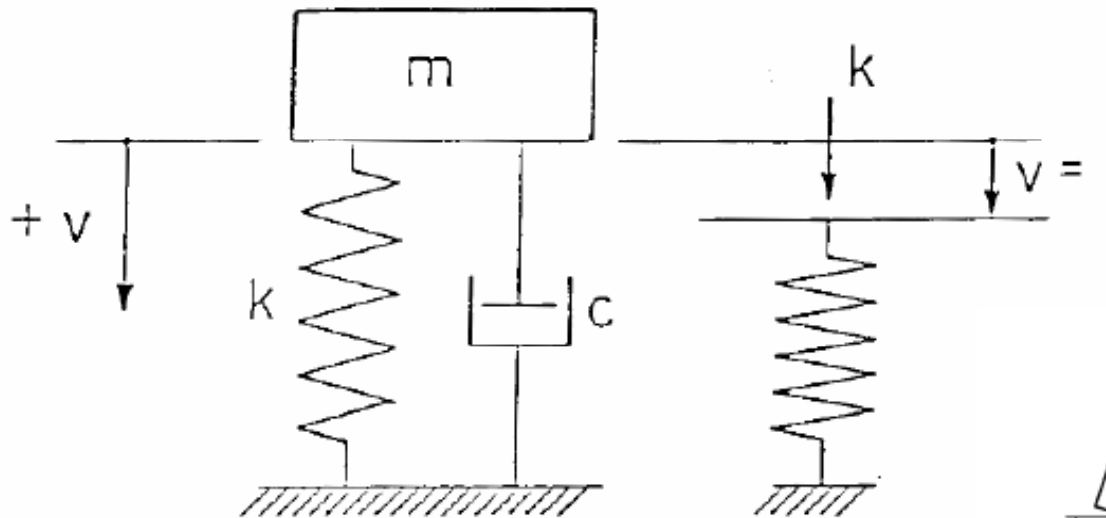
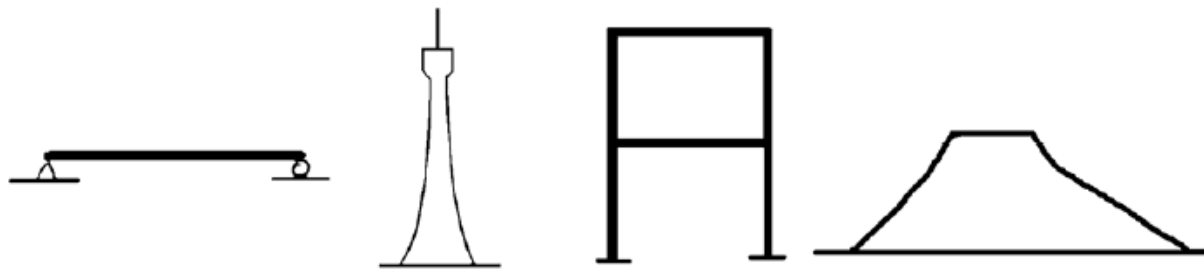


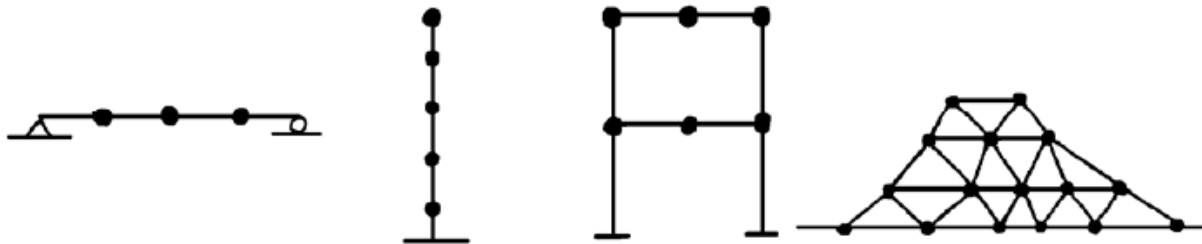
Fig. 4.8—Pile displacements for determination of group stiffness and damping related to unit rotation  $\psi$ .

# Basics of Dynamics – Types of Models

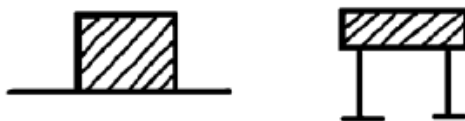
Figure 1.1



(a) distributed models



(b) lumped mass models

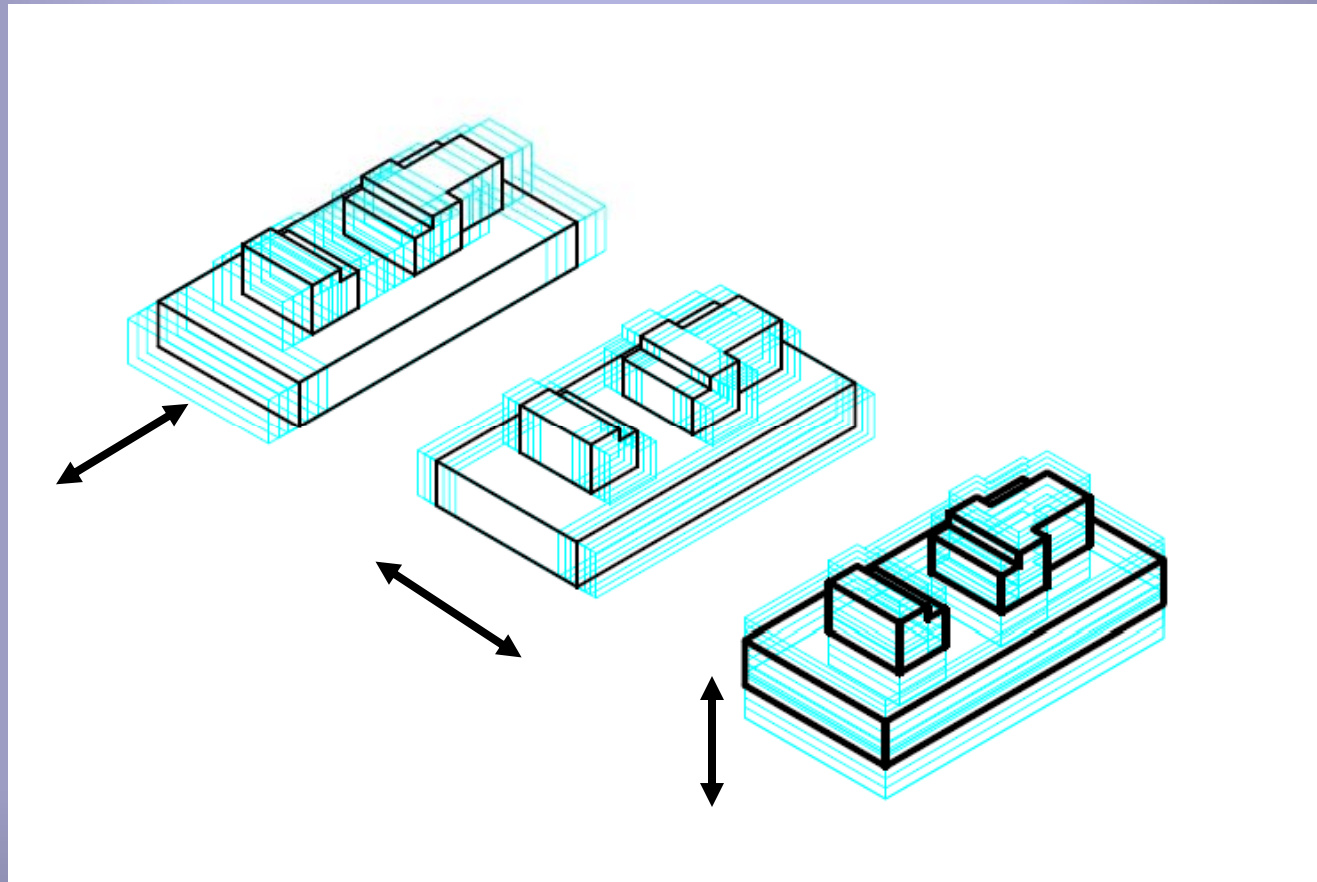


(c) - rigid bodies

Source: El Naggar, M.H. "Design of Machine Foundations."

# Basics of Dynamics – Rigid Body Modes

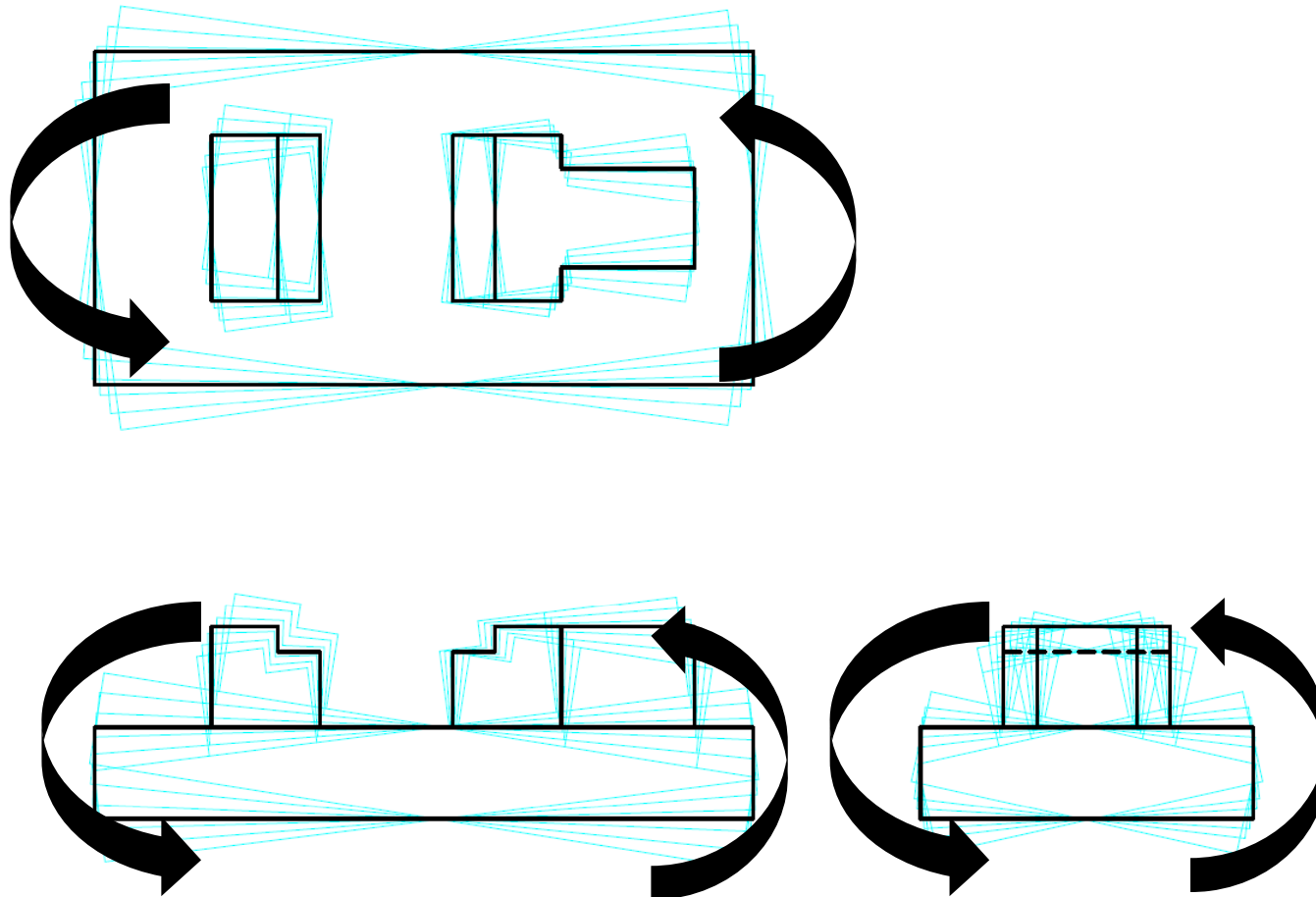
RIGID BODIES (Translational):





# Basics of Dynamics – Rigid Body Modes

RIGID BODIES (Rotational):



# Basics of Dynamics – Mode Shapes

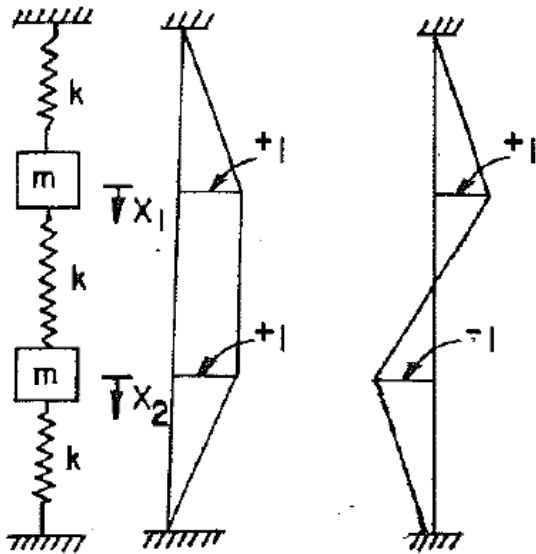


Figure 1-51. Normal modes of vibration.

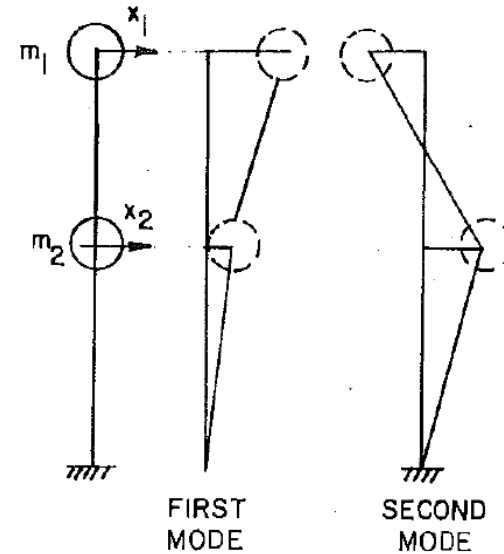


Figure 1-52. Modes of vibration of a two-degree-of-freedom system.

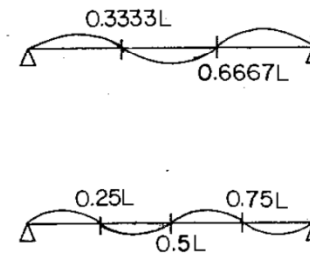
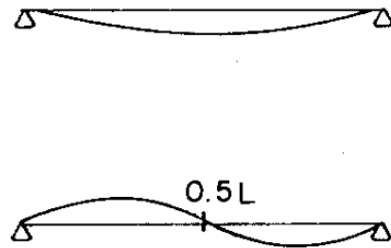
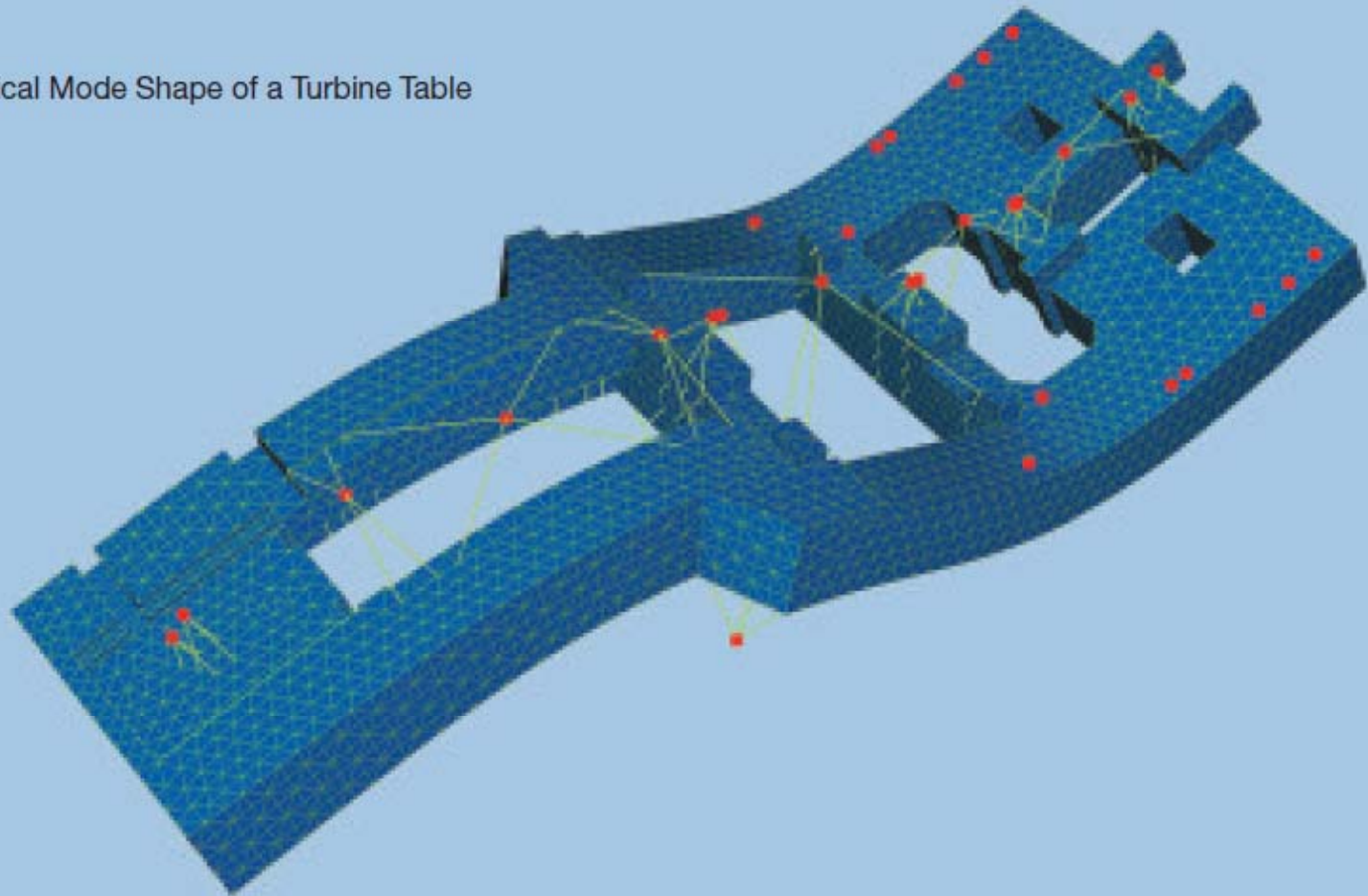


Figure 1-49. Various mode shapes of a hinged-hinged beam.

# Basics of Dynamics – Mode Shapes

Typical Mode Shape of a Turbine Table



Source: GERB Vibration Control systems

SDOF Equation of Motion:

$$m\ddot{v} + c\dot{v} + kv = \underbrace{P(t)}_{\text{Forcing function}}$$

$m$  = mass

$\ddot{v}$  = acceleration

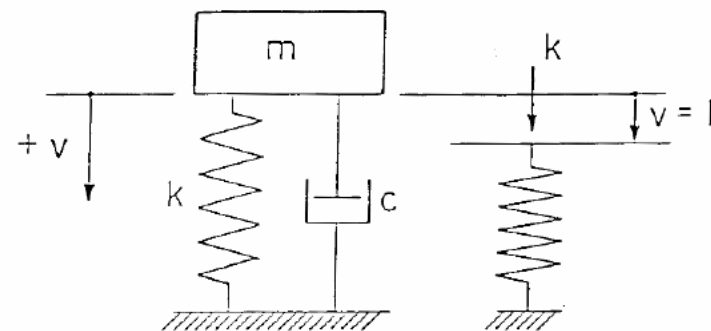
$c$  = damping

$\dot{v}$  = velocity

$k$  = stiffness

$v$  = displacement

Figure 2.1: Basic Model of Single Degree of Freedom System





For a rotating machine:

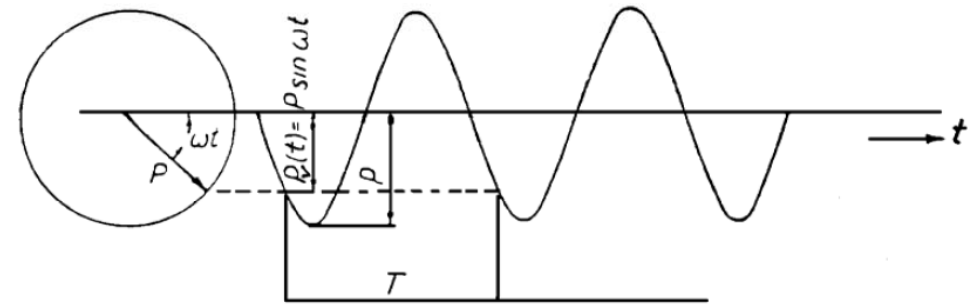
$$P = m_e e \omega^2$$

$m_e$  = rotating mass

$e$  = eccentricity

$\omega$  = circular frequency of rotation

Figure 1.2: Harmonic time history



$$P_v(t) = P \sin(\omega t)$$

$$P_h(t) = P \cos(\omega t)$$

For a rotating machine:

$$F_o = m_r e_m \omega_o^2 S_f / 12 \text{ lbf} \quad (3-3)$$

$$F_o = m_r e_m \omega_o^2 S_f / 1000 \text{ N}$$


where

- $F_o$  = dynamic force amplitude (zero-to-peak), lbf (N);
- $m_r$  = rotating mass, lbm (kg);
- $e_m$  = mass eccentricity, in. (mm);
- $\omega_o$  = circular operating frequency of the machine (rad/s); and
- $S_f$  = service factor, used to account for increased unbalance during the service life of the machine, generally greater than or equal to 2.

Source: ACI 351

**Table 3.1—Balance quality grades for selected groups of representative rigid rotors (excerpted from ANSI/ASA S2.19)**


Balance quality grade	Product of $e\omega$ , in./s (mm/s)	Rotor types—general examples
G1600	63 (1600)	Crankshaft/drives of rigidly mounted, large, two-cycle engines
G630	2.5 (630)	Crankshaft/drives of rigidly mounted, large, four-cycle engines
G250	10 (250)	Crankshaft/drives of rigidly mounted, fast, four-cylinder diesel engines
G100	4 (100)	Crankshaft/drives of fast diesel engines with six or more cylinders
G40	1.6 (40)	Crankshaft/drives of elastically mounted, fast four-cycle engines (gasoline or diesel) with six or more cylinders
G16	0.6 (16)	Parts of crushing machines; drive shafts (propeller shafts, cardan shafts) with special requirements; crankshaft/drives of engines with six or more cylinders under special requirements
G6.3	0.25 (6.3)	Parts of process plant machines; centrifuge drums, paper machinery rolls, print rolls; fans; flywheels; pump impellers; machine tool and general machinery parts; medium and large electric armatures (of electric motors having at least 80 mm shaft height) without special requirement
G2.5	0.1 (2.5)	Gas and steam turbines, including marine main turbines; rigid turbo-generator rotors; turbo-compressors; machine tool drives; medium and large electric armatures with special requirements; turbine driven pumps
G1	0.04 (1)	Grinding machine drives
G0.4	0.015 (0.4)	Spindles, discs, and armatures of precision grinders



# Preliminary Design – Rules of Thumb

The following guidelines may be used for the trial dimensions of the foundation block:

1. Generally, the base of the foundation should be above the ground water table. It should be resting on competent native soil (no backfill or vibration-sensitive soil).
2. The mass of the block should be 2-3 times the mass of the supported rotating machine, and 3-5 times the supported reciprocating machine.



# Preliminary Design – Rules of Thumb

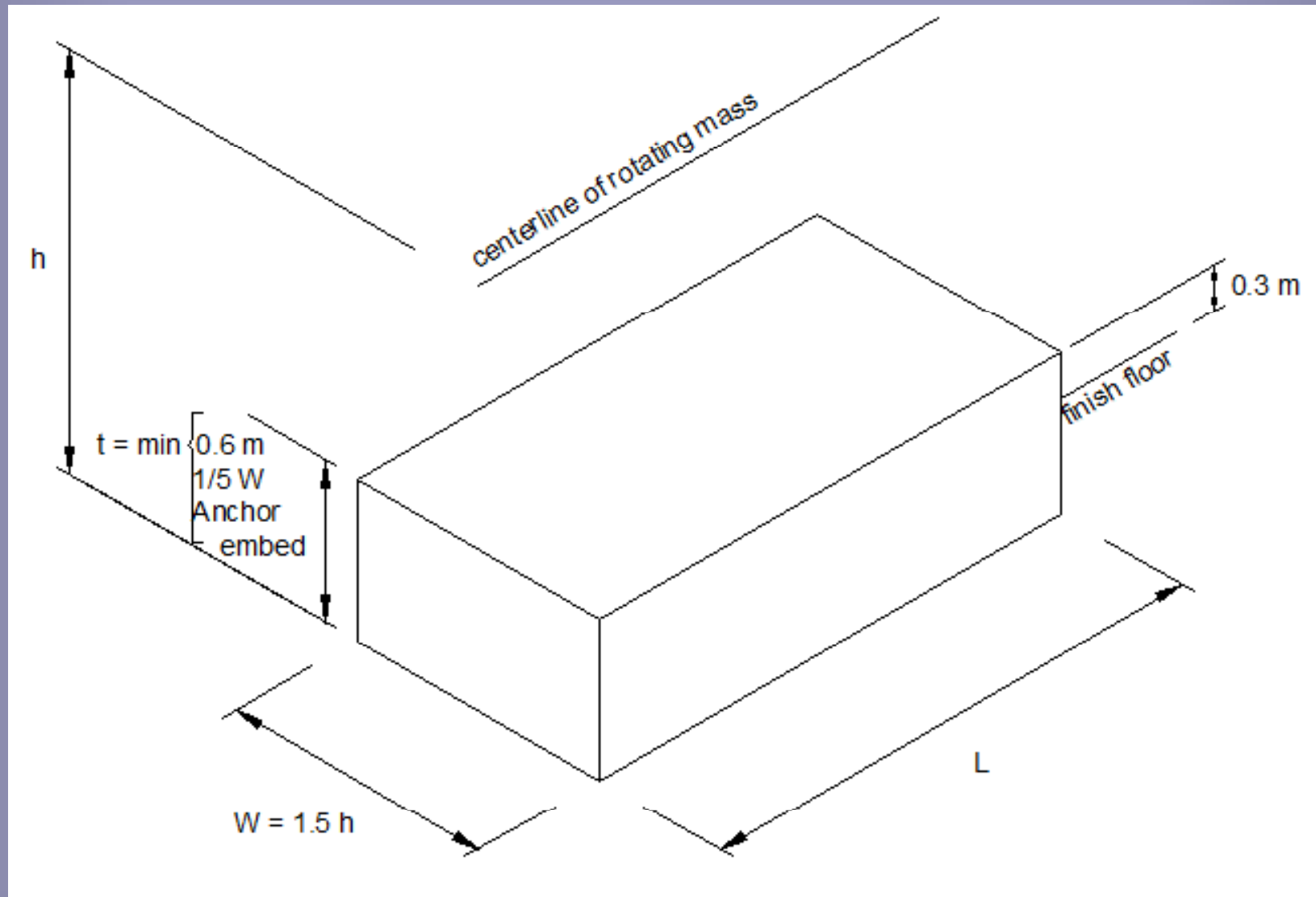
3. The top of the block should be 0.3 m above the elevation of the finished floor.


4. The thickness of the block should be the greatest of 0.6 m, the anchorage length of the anchor bolts and  $1/5$  the least dimension of the footing.

5. The width should be 1-1.5 times the vertical distance from the base to the machine centerline to increase damping in rocking mode.



# Preliminary Design – Rules of Thumb






# Preliminary Design – Rules of Thumb

6. The length is estimated from the mass requirement and estimated thickness and width of the foundation. The length should then be increased by 0.3 m for access maintenance purposes.

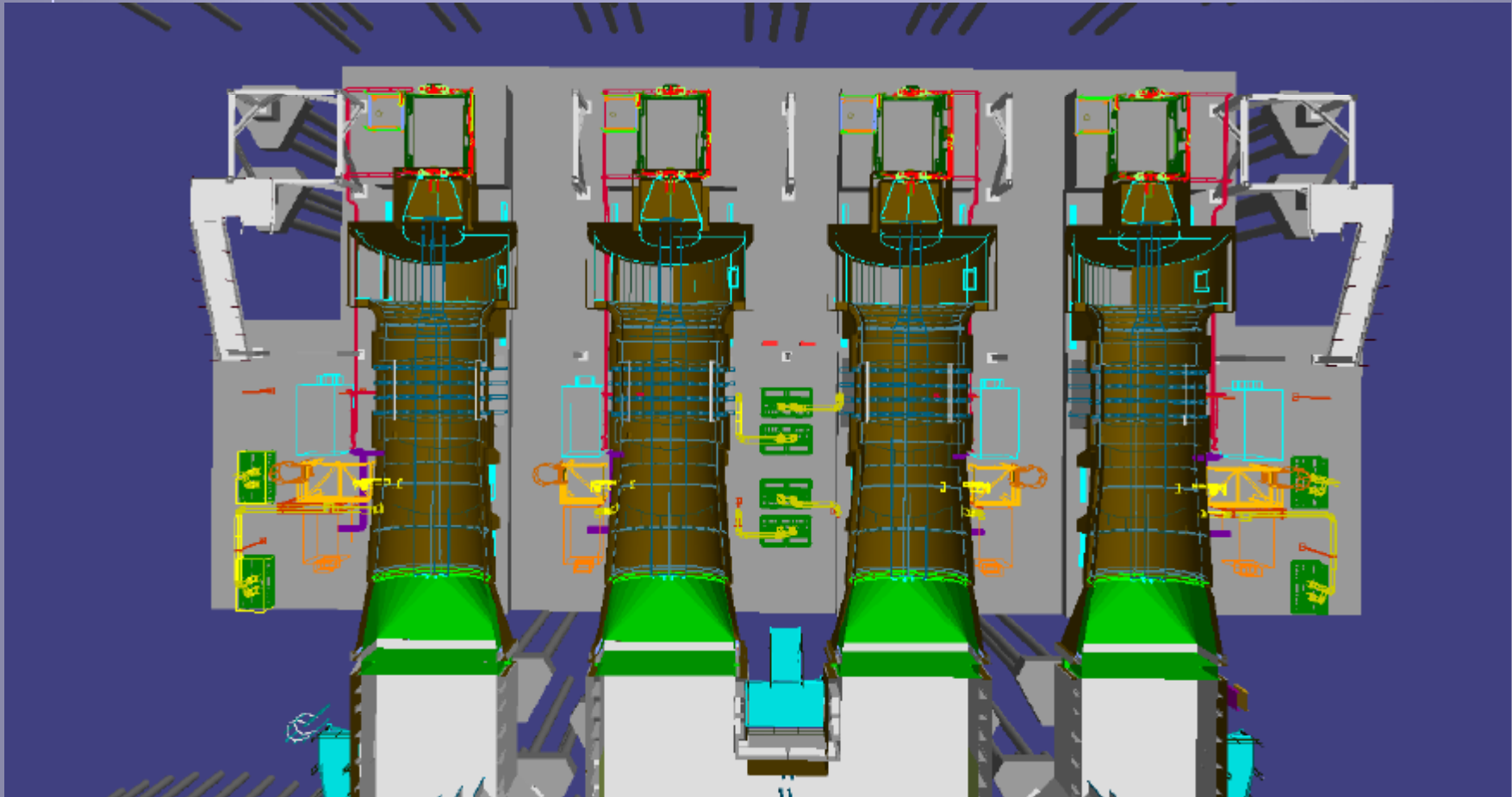
7. The length and width of the foundation are adjusted so that the center of gravity of the machine plus equipment lies within 5% of the foundation dimension in each direction, from the foundation center of gravity.



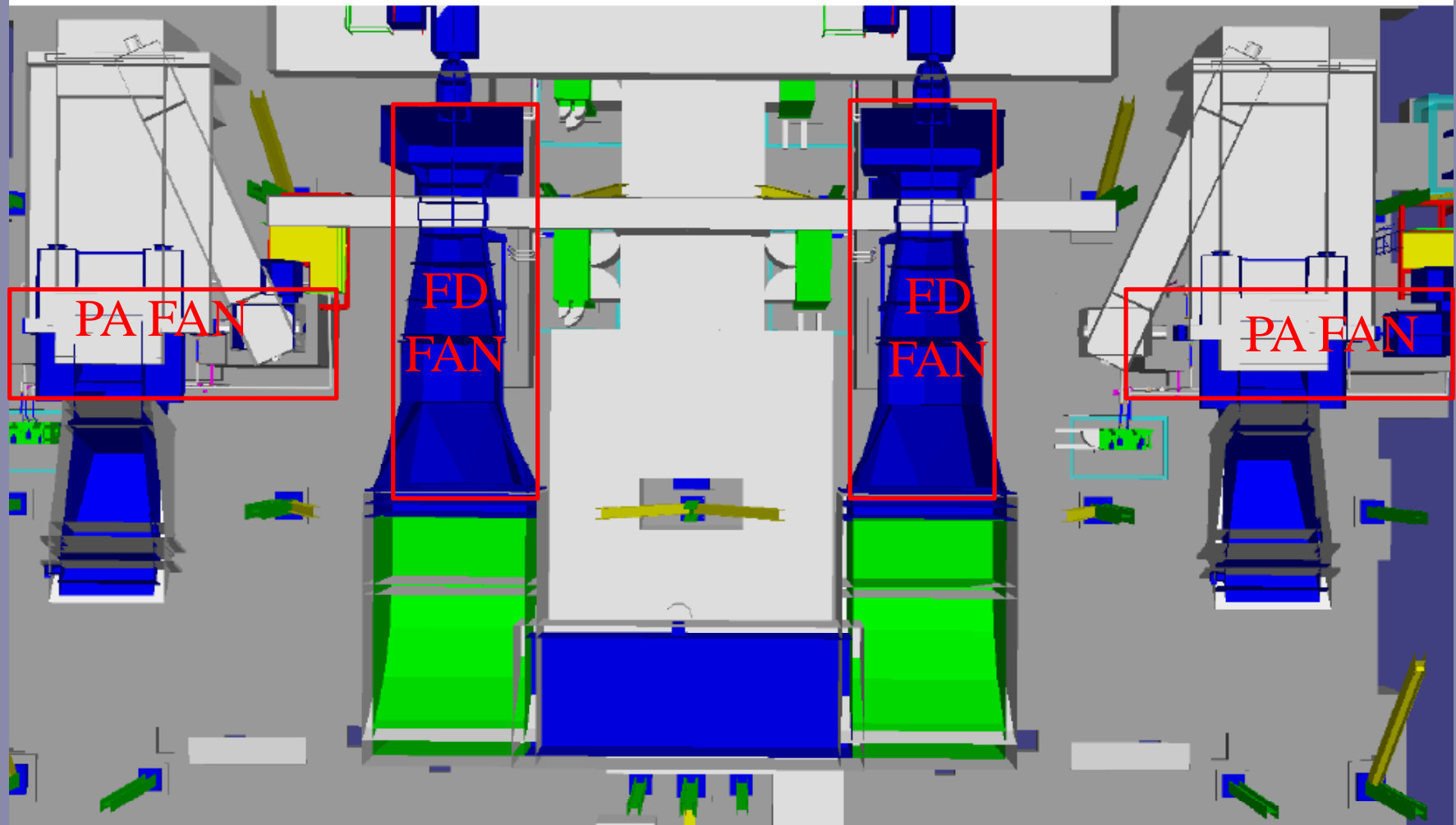
# Preliminary Design – Rules of Thumb

8. It is desirable to increase the embedded depth of the foundation to increase the damping and provide lateral restraint as well.
9. Ensure dimensions fit with all physical constraints.

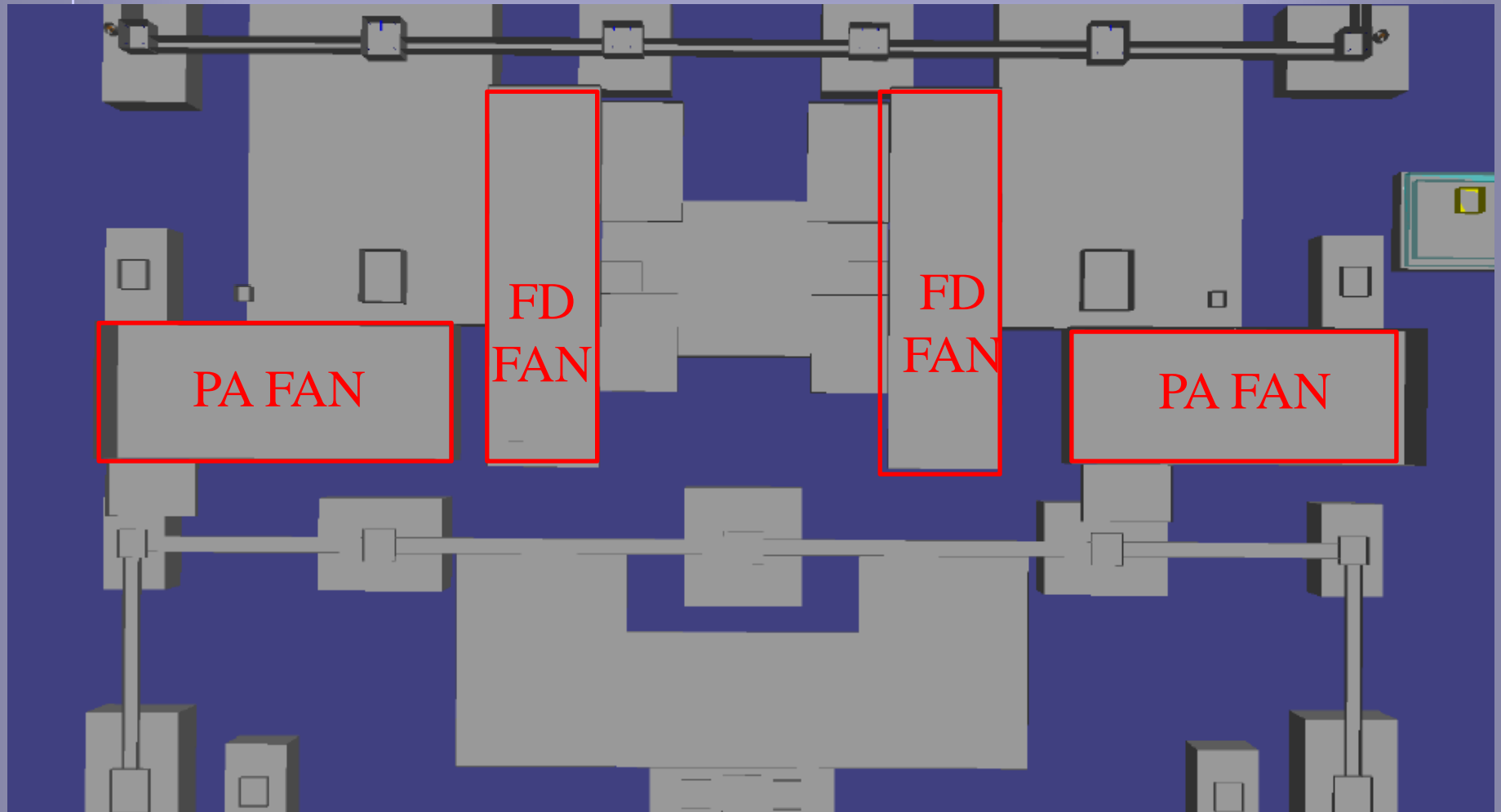
# Preliminary Design – Physical Constraints



# Preliminary Design – Physical Constraints

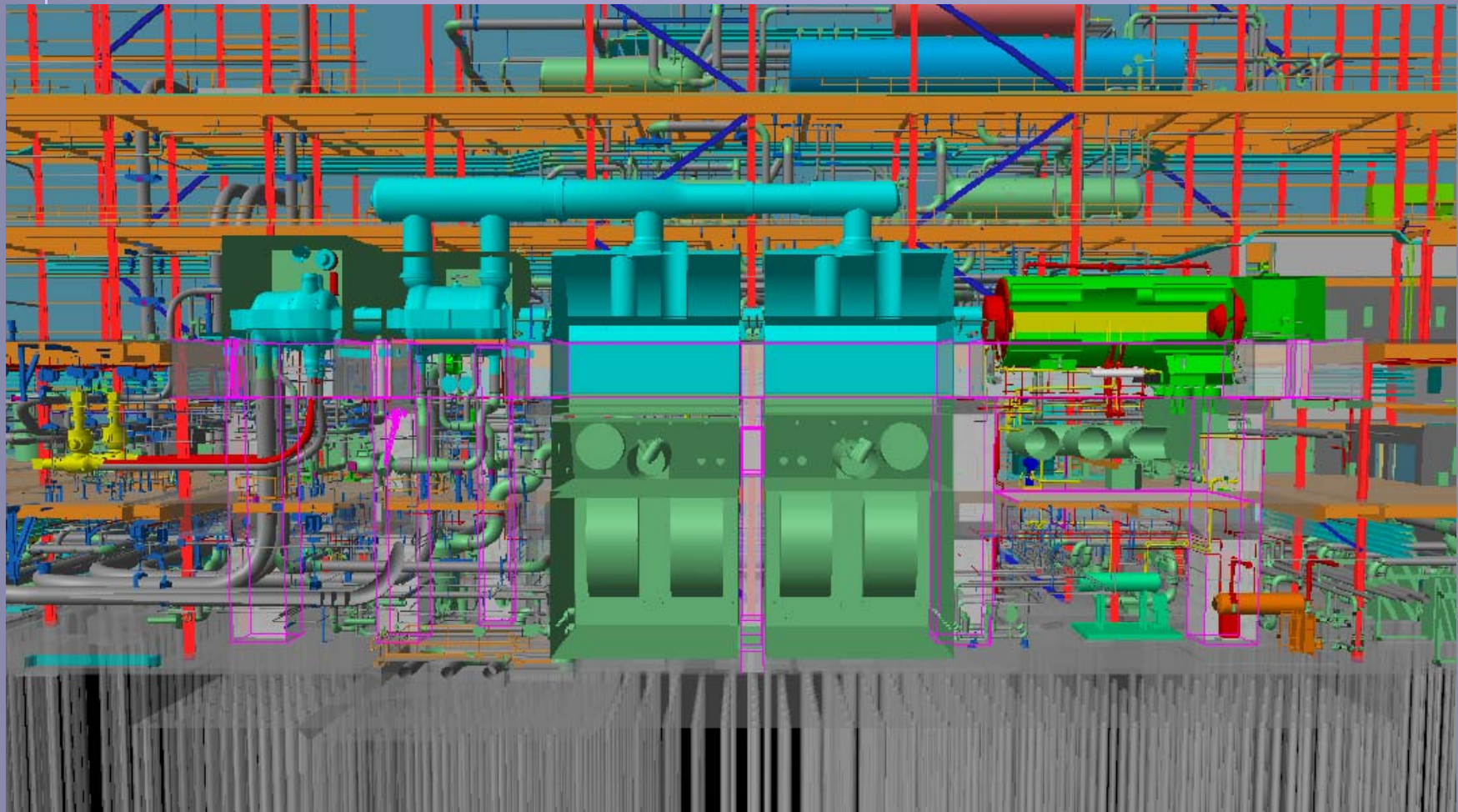


# Preliminary Design – Physical Constraints





# Preliminary Design – Physical Constraints



# Detailed Dynamic Analysis

## Design Checks:

### Preliminary

- Mass ratio

### Frequency (Modal) Analysis

- Natural frequency outside of a range the of operating frequency

### Forced Response (Time History)

- Maximum displacement amplitude
  - Min foundation stiffness in all directions
  - Relative displacements between bearings (multiple rotors)
- Maximum velocity
- Maximum acceleration

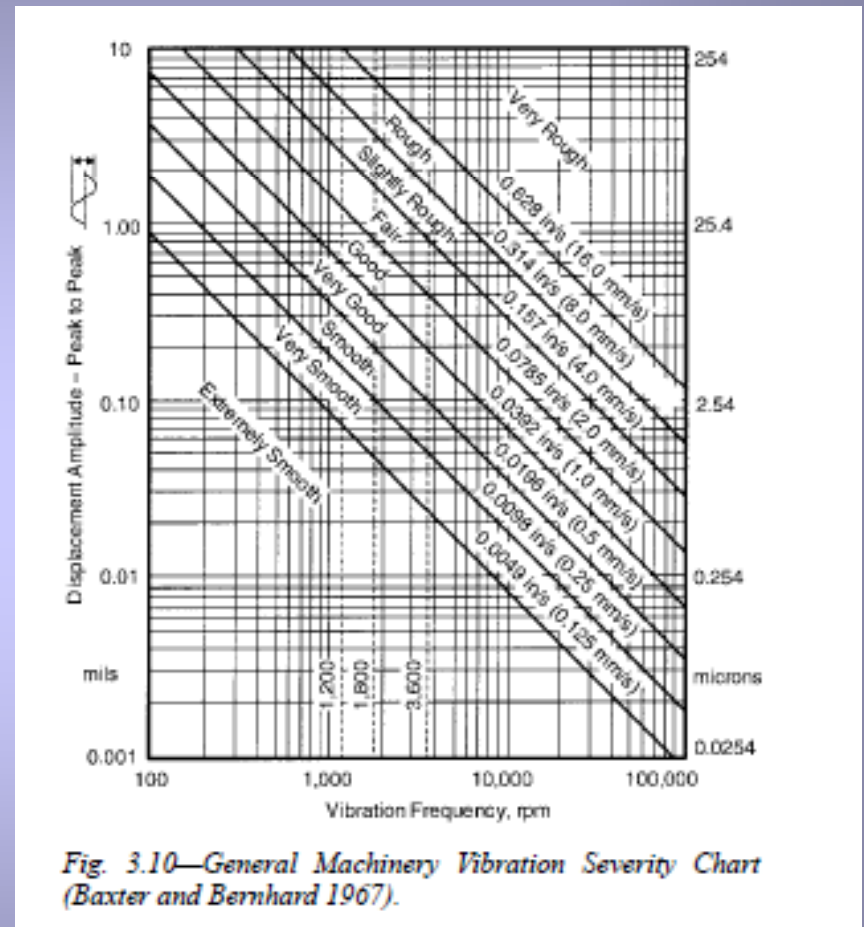
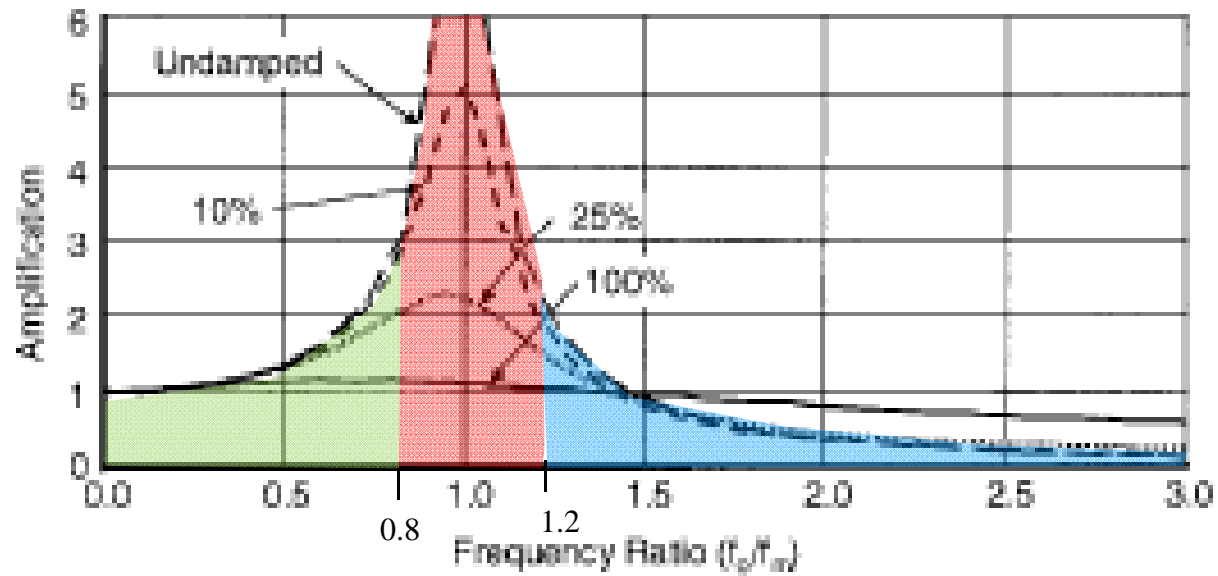


Fig. 3.10—General Machinery Vibration Severity Chart (Baxter and Bernhard 1967).

# Dynamic Amplification

## Amplification Factor & Natural Frequency Avoidance



**Fig. 3.14—Force transmissibility.**

# Dynamic Amplification – Natural Frequency

## Natural Frequency Equation

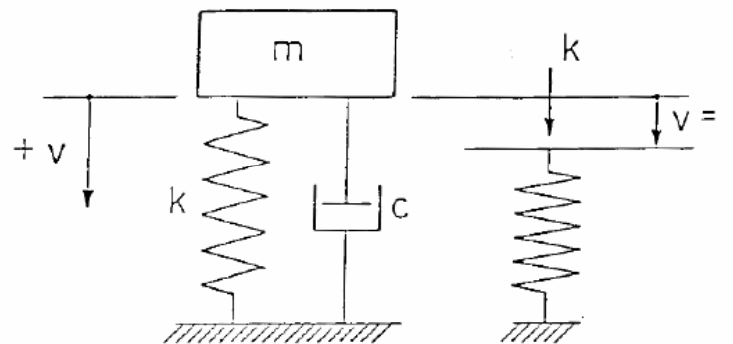
$$f_n = \frac{1}{2\pi} \sqrt{\frac{k}{m}}$$

$f_n = \text{natural frequency}$

$k = \text{stiffness}$

$m = \text{mass}$

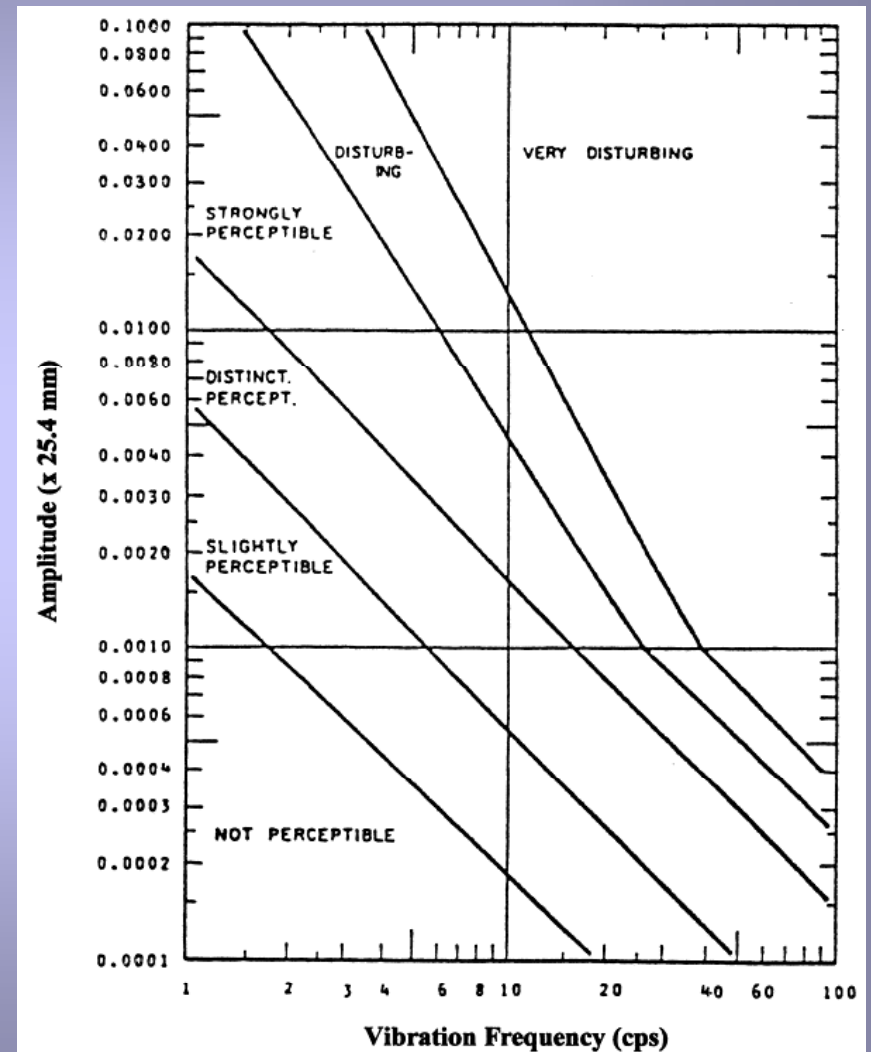
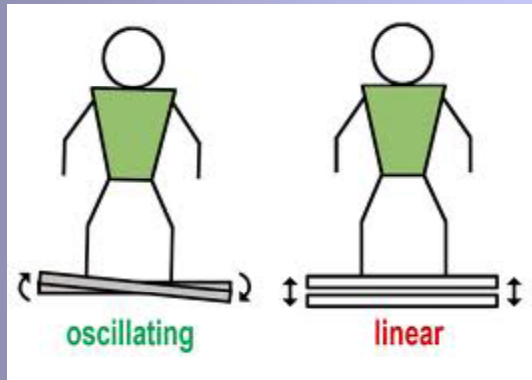
Figure 2.1: Basic Model of Single Degree of Freedom System



# Other Design Considerations

Interesting fact:

Motion which may be noticed by persons is on the order of 1/100 of that which is likely to cause damage to machines.



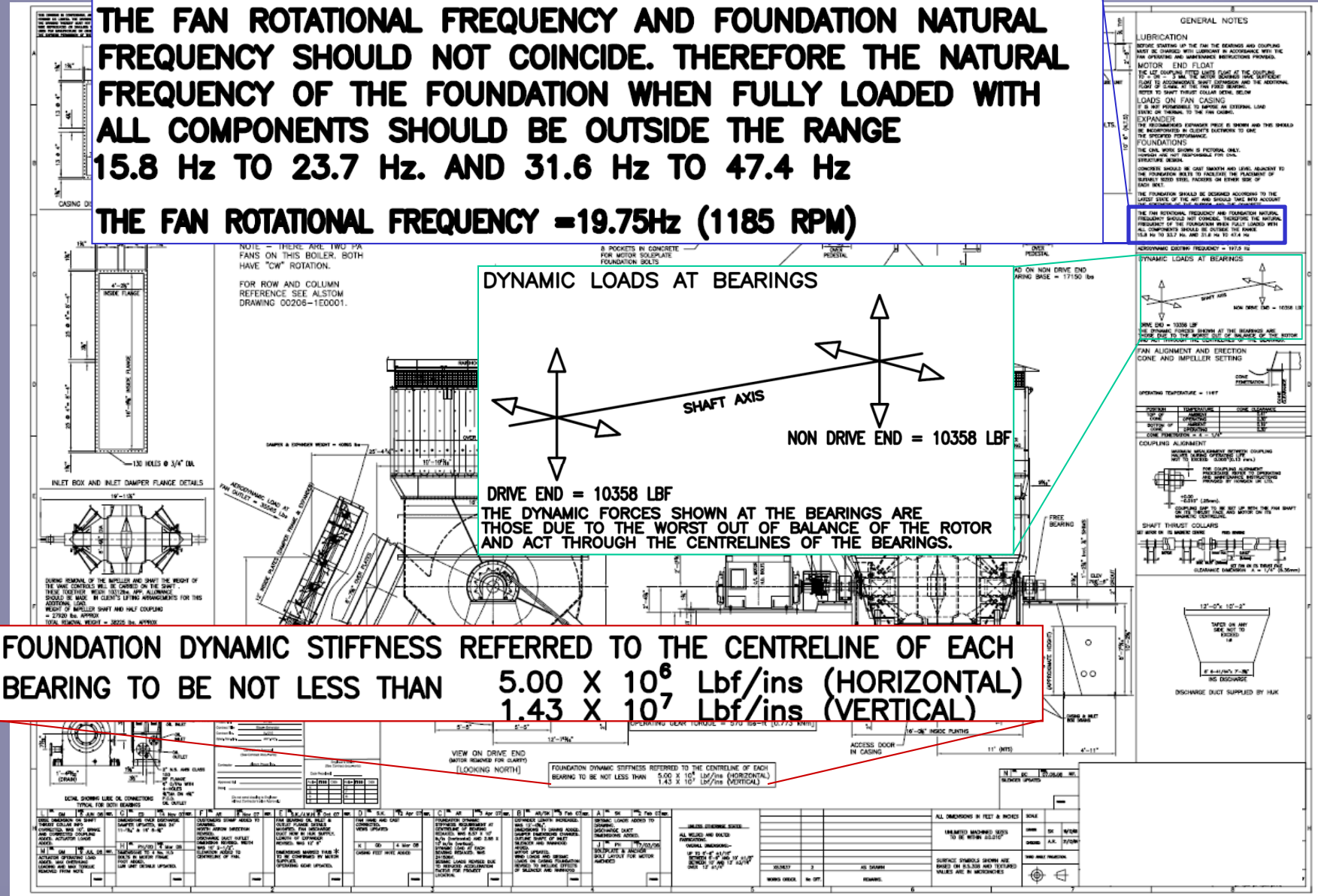
Source: Whitman & Richart. "Design Procedures for Dynamically Loaded Foundations"



# Machine Manufacturer's Design Criteria

**THE FAN ROTATIONAL FREQUENCY AND FOUNDATION NATURAL FREQUENCY SHOULD NOT COINCIDE. THEREFORE THE NATURAL FREQUENCY OF THE FOUNDATION WHEN FULLY LOADED WITH ALL COMPONENTS SHOULD BE OUTSIDE THE RANGE 15.8 Hz TO 23.7 Hz. AND 31.6 Hz TO 47.4 Hz**

**THE FAN ROTATIONAL FREQUENCY = 19.75Hz (1185 RPM)**





# Machine Manufacturer's Design Criteria

For a rotating machine:

$$F_o = m_r e_m \omega_o^2 S_f / 12 \text{ lbf}$$

## Design Input: Common

$$\omega := 1185 \text{ rpm}$$

$$g = 32.174 \frac{\text{ft}}{\text{s}^2}$$

$$Q := 0.25 \frac{\text{in}}{\text{s}}$$

Product of eccentricity and operating frequency. Designated as "Q" in Table 3.1, ACI 351.3R (Based on ANSI/ASA S2.19). Industry standard Q=0.25 per table.

$$e := \frac{Q}{\omega} = 2.015 \times 10^{-3} \text{ in}$$

$$S_f := 6.75$$

Service factor

## Design Input:

$$w_{\text{rotor}} := 38.225 \text{ kip}$$

$$m_{\text{rotor}} := \frac{w_{\text{rotor}}}{g} = 3.822 \times 10^4 \text{ lb}$$

$$F_{\text{rotor}} := S_f \cdot m_{\text{rotor}} \cdot e \cdot \omega^2 = 20.732 \text{ kip}$$

Total imbalance force @ rotor

$$F_{\text{bearing}} := \frac{F_{\text{rotor}}}{2} = 10.366 \text{ kip}$$

Imbalance force per bearing

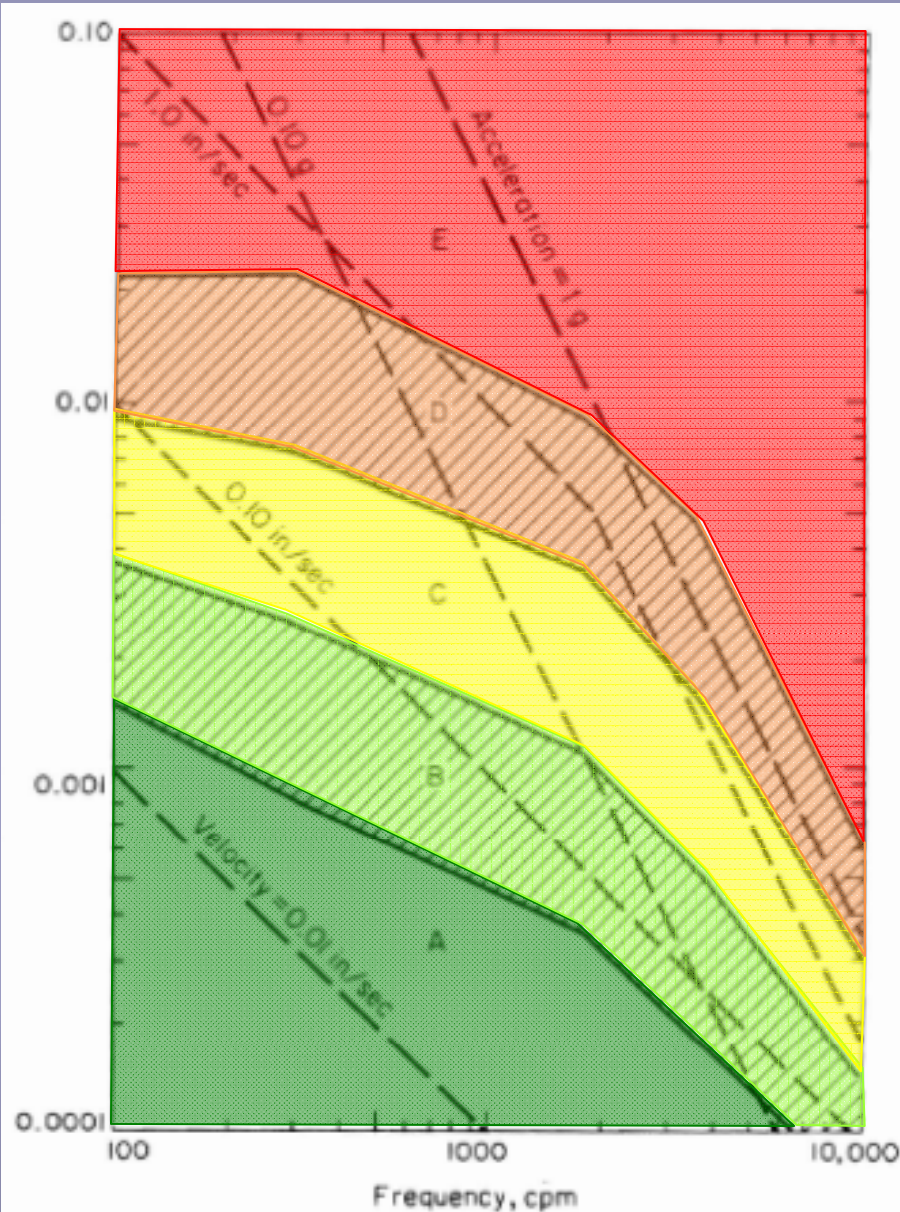


# Machine Manufacturer's Design Criteria

Additional loads for a turbine:

- Bowed rotor
- Loss of blade
- Generator short circuit
- Condenser vacuum
- Valve trips

# Machine Performance



## Performance Zones

**A=No Faults, New**


**B=Minor Faults,  
Good Condition**

**C = Faulty, Correct  
In 10 Days To Save  
\$\$**

**D = Failure Is Near,  
Correct In 2 Days**

**E = Stop Now**

Source: ACI 351 & Richard P. Ray,  
Ph.D., P.E., University of South Carolina



# Computer Modeling - Soil Considerations

To accurately account for soil-structure interactions for damping and stiffness effects on the system, a program which accounts for the geotechnical analysis is necessary.

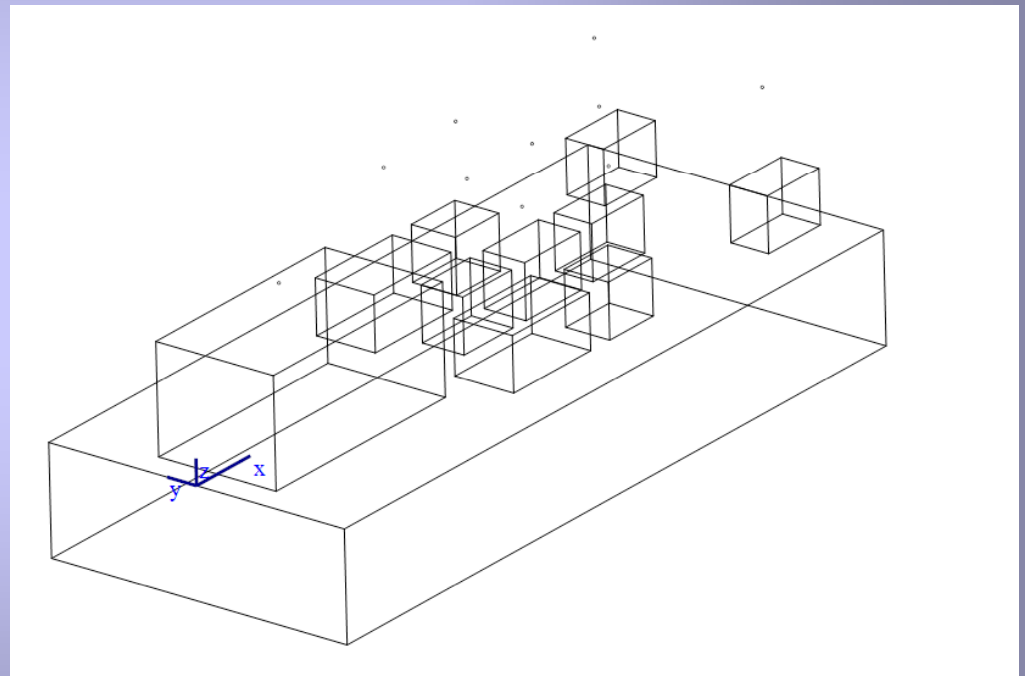
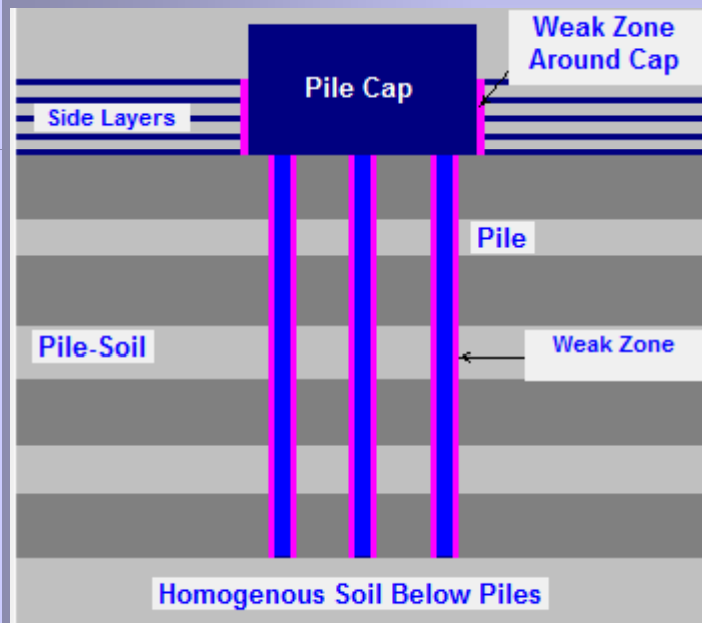
Geotechnical parameters required for analysis include:

- G, shear modulus
- mass density
- Poisson's ratio
- damping ratio
- depths and thickness of soil layers

# Computer Modeling - Soil Considerations

Input:

Geotechnical parameters, Physical characteristics, Dynamic load



# Computer Modeling - Soil Considerations

## Response Output: Stiffness and Displacements

	Frequency (rpm)	Horizontal Stiffness X (lb./ft)	Horizontal Damping X (lb./ft/S)	Horizontal Stiffness Y (lb./ft)	Horizontal Damping Y (lb./ft/S)	Vertical Stiffness Z (lb./ft)	Vertical Damping Z (lb./ft/S)	Rocking Stiffness X (lb.ft./Rad)	Rocking Damping X (lb.ft./Rad/S)	Rocking Stiffness Y (lb.ft./Rad)	Rocking Damping Y (lb.ft./Rad/S)	Torsional Stiffness Z (lb.ft./Rad)	Torsional Damping Z (lb.ft./Rad/S)
▶ 1	0.00	1.77E+08	3.98E+06	1.84E+08	4.13E+06	2.90E+08	6.95E+06	6.56E+10	3.58E+08	2.01E+11	9.81E+08	1.65E+11	7.12E+08
2	50.00	1.78E+08	3.71E+06	1.84E+08	3.84E+06	2.95E+08	6.06E+06	6.51E+10	2.74E+08	1.98E+11	8.36E+08	1.62E+11	6.16E+08
3	100.00	1.78E+08	3.41E+06	1.85E+08	3.53E+06	2.97E+08	5.79E+06	6.39E+10	2.63E+08	1.90E+11	9.21E+08	1.58E+11	6.53E+08
4	150.00	1.82E+08	3.27E+06	1.90E+08	3.38E+06	2.96E+08	5.68E+06	6.25E+10	2.71E+08	1.80E+11	1.04E+09	1.53E+11	7.06E+08
5	200.00	1.84E+08	3.19E+06	1.93E+08	3.30E+06	2.92E+08	5.65E+06	6.10E+10	2.84E+08	1.71E+11	1.16E+09	1.49E+11	7.56E+08
6	250.00	1.85E+08	3.15E+06	1.95E+08	3.24E+06	2.88E+08	5.66E+06	5.96E+10	2.97E+08	1.63E+11	1.26E+09	1.45E+11	8.01E+08
7	300.00	1.85E+08	3.13E+06	1.98E+08	3.20E+06	2.82E+08	5.69E+06	5.84E+10	3.10E+08	1.56E+11	1.35E+09	1.42E+11	8.39E+08

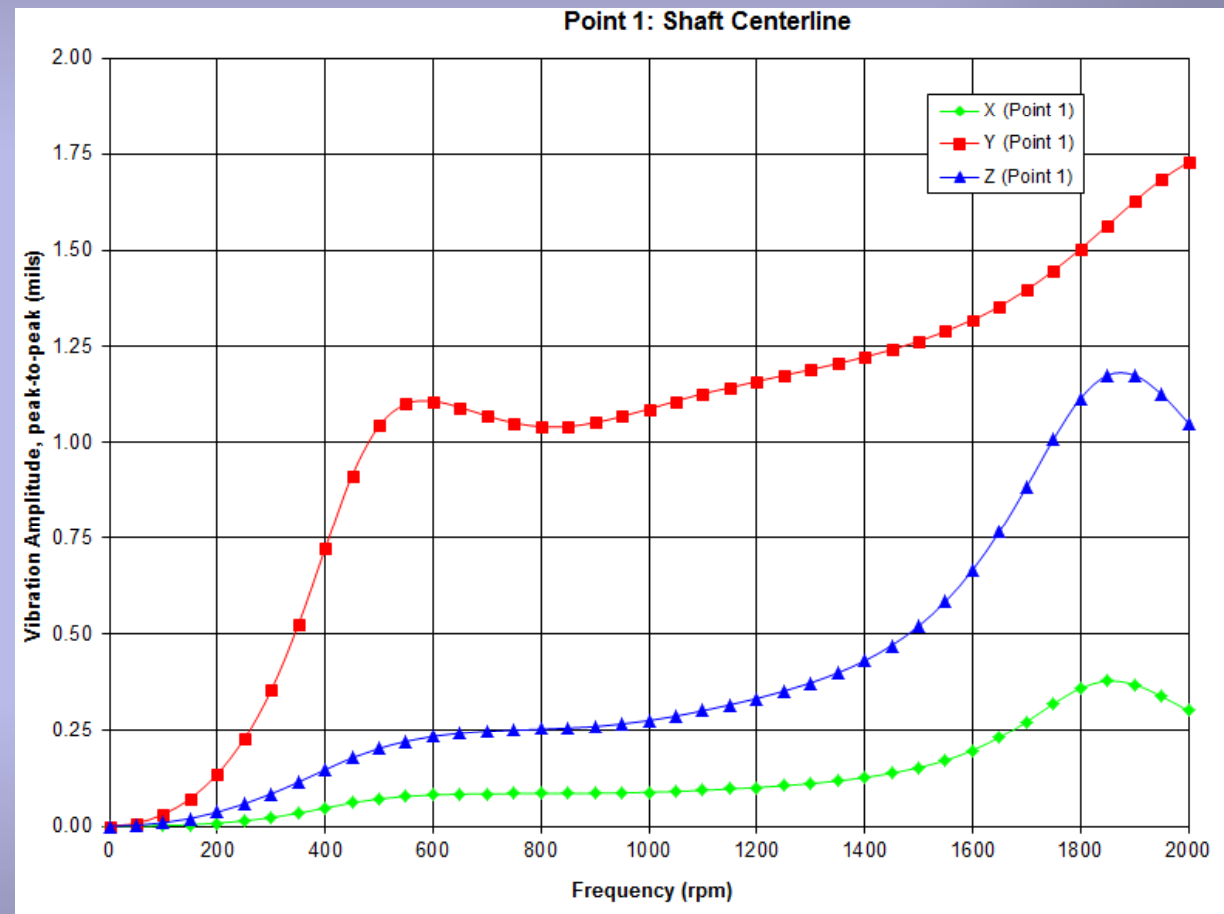
Center of Gravity		Resultant Points					
	Frequency (rpm)	Translational Response at CG - X (ft)	Translational Response at CG - Y (ft)	Translational Response at CG - Z (ft)	Rotational Response at CG - X (Rad)	Rotational Response at CG - Y (Rad)	Rotational Response at CG - Z (Rad)
1	0.00	2.11E-16	7.72E-15	3.46E-15	3.30E-16	3.18E-17	4.50E-17
2	50.00	5.96E-09	2.13E-07	9.33E-08	9.19E-09	8.91E-10	1.26E-09
3	100.00	2.57E-08	8.70E-07	3.72E-07	3.82E-08	3.76E-09	5.26E-09
4	150.00	6.39E-08	2.01E-06	8.47E-07	9.08E-08	9.10E-09	1.25E-08
5	200.00	1.30E-07	3.77E-06	1.53E-06	1.73E-07	1.76E-08	2.37E-08
6	250.00	2.35E-07	6.32E-06	2.44E-06	2.94E-07	3.01E-08	3.97E-08
7	300.00	3.98E-07	9.87E-06	3.56E-06	4.64E-07	4.77E-08	6.17E-08



# Computer Modeling - Soil Considerations

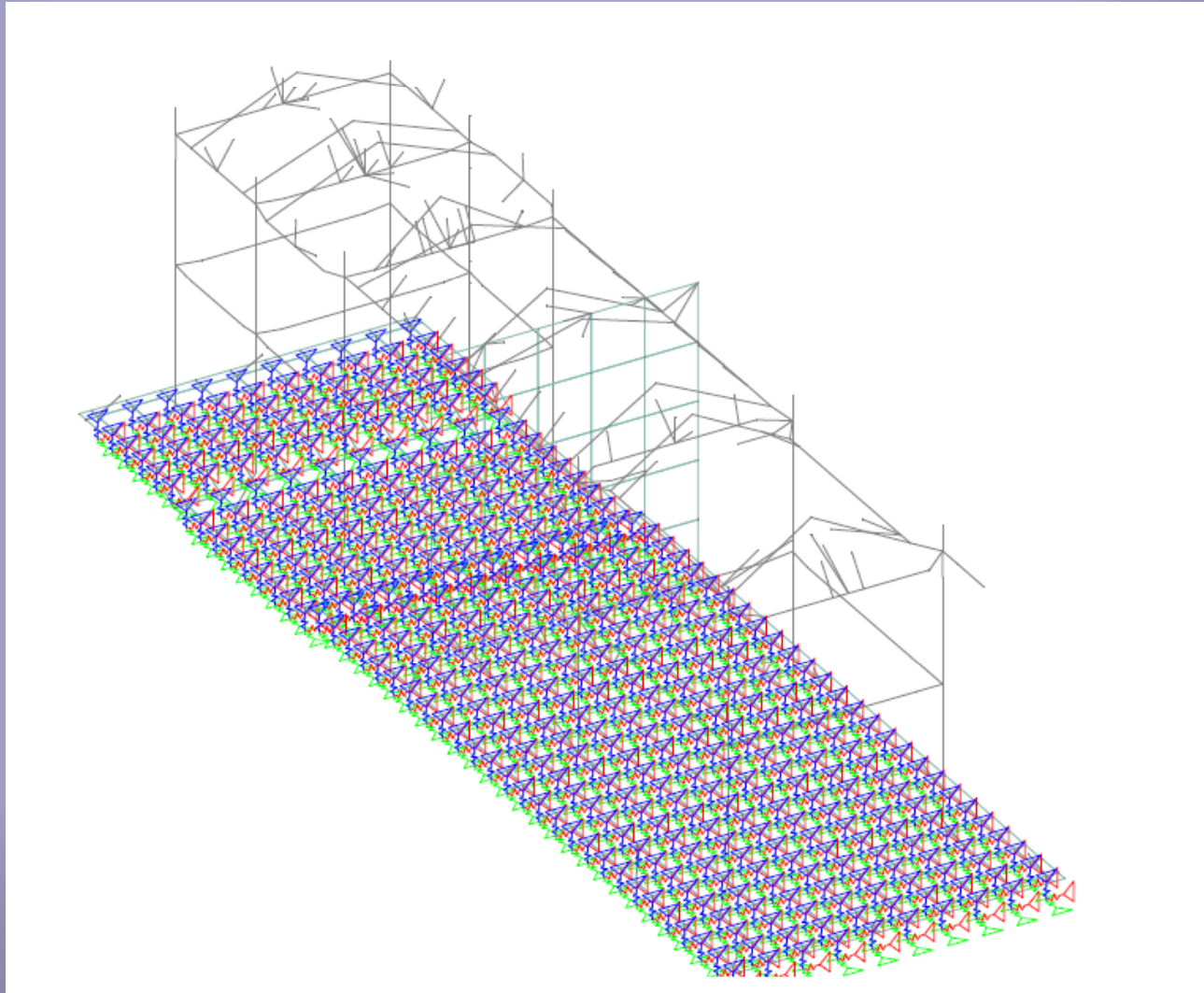
## Check against Machine Requirements:

- Vibration Amplitudes
- Vibration Velocities
- Foundation Stiffness



# Computer Modeling - Structural

## Structural modeling – Steam Turbine-Generator



# Construction Considerations





# Construction Considerations





# Construction Considerations





# Construction Considerations





# Construction Considerations



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# Construction Considerations





# Construction Considerations

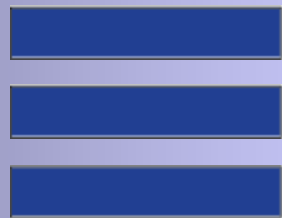




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Dynamic Foundations:

Basics of Analysis & Design

**Thanks for Attending.  
Have a Great Day.**