

- *†15-4** The trailer hitch from Figure 1-1 (p. 11) has loads applied as shown in Figure P15-1. The tongue weight of 100 kg acts downward and the pull force of 4 905 N acts horizontally. Using the dimensions of the ball bracket in Figure 1-5 (p. 14), draw a free-body diagram of the ball bracket and find the tensile and shear loads applied to the two bolts that attach the bracket to the channel in Figure 1-1. Size and specify the bolts and their preload for a safety factor of at least 1.7.

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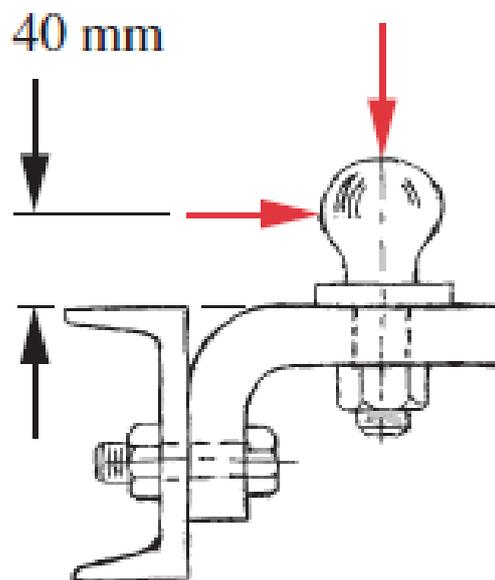


FIGURE P15-1

Problems 15-4 to 15-6

PROBLEM 15-4

Statement: The trailer hitch from Figure 1-1 (p. 12) has loads applied as shown in Figure P3-2. The tongue weight of 100 kg acts downward and the pull force of 4905 N acts horizontally. Using the dimensions of the ball bracket in Figure 1-5 (p. 15), draw a free-body diagram of the ball bracket and find the tensile and shear loads applied to the two bolts that attach the bracket to the channel in Figure 1-1. Size and specify the bolts and their preload for a safety factor of at least 1.7.

Given:	Hitch dimensions:	$a := 40\text{-mm}$	Tongue weight	$M_{tongue} := 100\text{-kg}$
		$b := 31\text{-mm}$	Pull force	$F_{pull} := 4.905\text{-kN}$
		$c := 70\text{-mm}$	Number of bolts	$N_{bolts} := 2$
		$d := 20\text{-mm}$	Young's modulus	$E := 206.8\text{-GPa}$
		$t := 19\text{-mm}$	Design safety factor	$N_d := 1.7$
			Bolt modulus	$E_{bolt} := E$
			Member modulus	$E_{memb} := E$

Assumptions: The shear load will be taken by friction between the hitch and the support.

Design Choices:

Use M12 x 1.75 , class 8.8 bolts.

Material properties for class 8.8:

Proof strength $S_p := 600\text{-MPa}$

Yield strength $S_y := 660\text{-MPa}$

Bolt diameter $d_b := 12\text{-mm}$

Clamp length $l := 30\text{-mm}$

Preload fraction $f_p := 0.59$

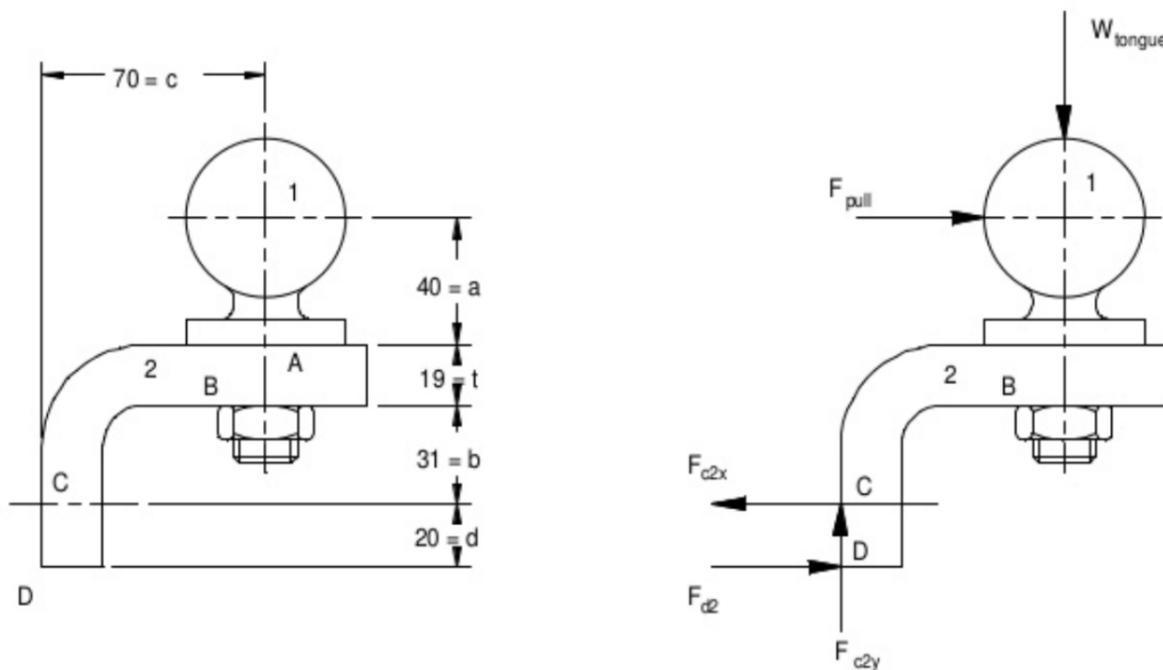


FIGURE S15-4

Dimensions and Free Body Diagram for Problem 15-4

Solution: See Figure S15-4 and Mathcad file P1504.

1. The weight on the tongue is

$$W_{tongue} := M_{tongue} \cdot g \qquad W_{tongue} = 0.981 \cdot kN$$

2. The FBD of the hitch and bracket assembly is shown in Figure 3-4. The known external forces that act on the ball are F_{pull} and W_{tongue} . The reactions on the bracket are at points C and D . The bolts at C provide tensile (F_{c2x}) and shear (F_{c2y}) forces, and the bracket resists rotation about point D where the reaction force F_{d2} is applied by the channel to which the bracket is bolted.

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15-4-2

3. Solving for the reactions by summing the horizontal and vertical forces and the moments about D :

$$\sum F_x: (F_{pull} - F_{c2x}) + F_{d2} = 0 \qquad (1)$$

$$\sum F_y: F_{c2y} - W_{tongue} = 0 \qquad (2)$$

$$\sum M_D: F_{c2x} \cdot d - F_{pull} \cdot (a + t + b + d) - W_{tongue} \cdot c = 0 \qquad (3)$$

4. Solving equation (3) for F_{c2x}

$$\sum F_y: F_{c2y} - W_{tongue} = 0 \qquad (2)$$

$$\sum M_D: F_{c2x} \cdot d - F_{pull} \cdot (a + t + b + d) - W_{tongue} \cdot c = 0 \qquad (3)$$

4. Solving equation (3) for F_{c2x}

$$F_{c2x} := \frac{F_{pull} \cdot (a + t + b + d) + W_{tongue} \cdot c}{d} \qquad F_{c2x} = 30.41 \cdot kN \qquad (4)$$

5. Substituting into (1) and solving for F_{d2}

$$F_{d2} := F_{c2x} - F_{pull} \qquad F_{d2} = 25.505 \cdot kN \qquad (5)$$

6. Solving (2) for F_{c2y}

$$F_{c2y} := W_{tongue} \qquad F_{c2y} = 0.981 \cdot kN \qquad (6)$$

7. The loads applied to the two bolts that attach the bracket to the channel are:

$$\text{Axial force on two bolts} \qquad F_{c2x} = 30.4 \cdot kN \qquad P_{tot} := F_{c2x}$$

$$\text{Shear force taken by friction} \qquad F_{c2y} = 0.98 \cdot kN$$

8. Determine the load per bolt. $P := \frac{P_{tot}}{N_{bolts}} \qquad P = 15.20 \cdot kN$

9. Get the tensile stress area from Table 15-2. $A_t := 84.27 \cdot mm^2$

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$$A_t := 84.27 \cdot \text{mm}^2$$

10. Calculate the preload.

$$F_i := f_p \cdot S_p \cdot A_t \quad F_i = 29.83 \cdot \text{kN}$$

11. Determine the relevant ratios for this joint from equations 15-18a and b.

Joint aspect ratio: $j := \frac{d_b}{l} \quad j = 0.400$

Plate to bolt modulus: $r := \frac{E_{memb}}{E_{bolt}} \quad r = 1$

12. Calculate $C_r = C$ using equation 15.19 and the coefficients p_i from Table 15-8 for $j = 0.4$.

Coefficients from Table 15-8: $p_0 := 0.7351$

$$p_1 := -1.2612$$

$$p_2 := 1.1111$$

$$p_3 := -0.3779$$

Joint stiffness constant: $C := p_3 \cdot r^3 + p_2 \cdot r^2 + p_1 \cdot r + p_0 \quad C = 0.207$

13. The portions of the applied load P felt by the bolt and the material can now be found from equations 15.13.

$$P_b := C \cdot P \quad P_b = 3.15 \cdot \text{kN}$$

$$P_m := (1 - C) \cdot P \quad P_m = 12.1 \cdot \text{kN}$$

14. Find the resulting loads in bolt and material after the load P is applied.

$$F_b := F_i + P_b \quad F_b = 32.98 \cdot \text{kN}$$

$$F_m := F_i - P_m \quad F_m = 17.78 \cdot \text{kN}$$

15. The maximum tensile stress in the bolt is

$$\sigma_b := \frac{F_b}{A_t} \quad \sigma_b = 391.4 \cdot \text{MPa}$$

16. This is a uniaxial stress situation, so the principal stress and von Mises stress are identical to the applied tensile stress. The safety factor against yielding for class 8.8 with $S_y = 660 \cdot \text{MPa}$ is then

$$N_y := \frac{S_y}{\sigma_b} \quad N_y = 1.7$$

17. The load required to separate the joint and the safety factor against joint separation are found from equations 15.14c and 15.14d.

$$P_0 := \frac{F_i}{1 - C} \quad P_0 = 37.6 \cdot \text{kN}$$

$$\sigma_b := \frac{F}{A_t}$$

$$\sigma_b = 391.4 \text{ MPa}$$

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$$N_y := \frac{S_y}{\sigma_b}$$

$$N_y = 1.7$$

17. The load required to separate the joint and the safety factor against joint separation are found from equations 15.14c and 15.14d.

$$P_0 := \frac{F_i}{1 - C}$$

$$P_0 = 37.6 \text{ kN}$$

$$N_{sep} := \frac{P_0}{P}$$

$$N_{sep} = 2.5$$