

123 Main Street  
White Plains, New York 10601  
914 681.6200

report



July 25, 2005

The Honorable Jaclyn Brillig, Secretary  
New York State Board on Electric Generation  
Siting and the Environment  
Three Empire State Plaza  
Albany, New York 12223-1350

Subject: Case 99-F-1627, New York Power Authority  
Compliance Filing in Accordance with the Article X Certificate

Dear Secretary Brillig:

In accordance with the Opinion and Order granting a Certificate of Environmental Compatibility and Public Need for the New York Power Authority's 500 MW Combined Cycle Project, issued on October 2, 2002, enclosed please find enclosed an original and seven sets of the Protective Relay Coordination Study (Certificate Condition II.M).

Please contact me at 914-287-3438, if you need additional information.

Sincerely,

A handwritten signature in cursive script that reads 'Ellen Koivisto'.

Ellen Koivisto  
Manager, Licensing

cc: James DeWaal Malephyte, DPS (5 copies)  
David Macks, DPS  
Edward Schrom, DPS  
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**New York Power  
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123 Main Street  
White Plains, NY 10601

Original Issue Date: July 11, 2005

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Revision No.: 0

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## Poletti 500MW Combined Cycle Power Project (CCPP)

# Protective Relay Coordination Study Submittal to the Public Service Commission

Prepared by

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Protection & Control Section

Engineering - Power Generation

**POLETTI 500 MW COMBINED CYCLE POWER PROJECT  
PROTECTIVE RELAY COORDINATION STUDY  
SUBMITTAL TO THE PUBLIC SERVICE COMMISSION**

**1.0 SCOPE**

This report contains the protective relaying design and power system equipment information for the New York Power Authority's (NYPA) 500MW Combined Cycle Power Project 138KV feeder interconnections to the Con Edison (CE) 138KV Astoria West substation. The plant protective relay systems are illustrated on relay and metering one-line diagrams while the major equipment information is represented on the corresponding manufacturers' nameplate drawings. Relay and metering potential transformers (PT) and current transformers (CT) nameplate data as well as CT saturation (SAT) curves are provided. Also included in this report, is a summary of the fault current analysis results conducted at select 138KV Con Edison system busses both with and without the 500MW plant in-service.

**2.0 DESCRIPTION OF THE 138KV FEEDER RELAYING**

It is NYPA's protection philosophy to provide two (2) separate relaying systems for each zone of protection. Two (2) numerical line current differential relaying systems designated as first-line and second-line protection systems will protect each 138KV feeder to CE. These relays will also provide stub-bus protection for the 138KV busses. The communications media for the two current differential relays consist of two (2) separate fiber optic cables, identified as Route 1 and Route 2. Separate high speed lockout relays will be used for each current differential relay system. At the CE terminal, numerical overcurrent relays have been installed to provide back-up protection of both feeders, and breaker failure protection for each of the associated 138KV feeder circuit breakers.

**2.1. First Line Protection System**

- a. Relay: Alstom Type MiCom P541.
- b. Communication: Fiber Optic Cable, Route 1.
- c. CT: Inner CTs

**2.2. Second-Line Protection System**

- a. Relay: G.E. Type UR-L90
- b. Communication: Fiber Optic Cable, Route 2
- c. CT: Outer CT's

### 2.3. Back-Up Protection System

CE requires a separate overcurrent relay with instantaneous and time elements (50/51) to provide back-up protection. This relay is not required at NYPA terminal.

- a. Relay: Basler BE1-851
- b. CT: Same CT used for second-line protection system, Item 2.2

### 2.4 Direct Transfer Trip Systems

Two separate fiber optic cables provide both line relaying systems and direct transfer trip system between the two terminals.

Dual systems will be used for DTT between CE and NYPA terminals. The DTT functions will be accomplished by the line relaying systems described above. The DTT systems will be used for 138KV breaker failure relay, transformer differential relay, and bus differential relay operations.

### 2.5 138KV Breaker Failure Protection

One breaker relay will be used to provide breaker failure protection.

- a. Relay: ABB SBF-1
- b. Communication: Fiber optic via first-line and second-line relays

Operation of breaker failure relay will energize a separate lock-out relay. The lock-out relay output contacts will operate the DTT functions of the two line relaying systems.

### **3.0 DESCRIPTION OF THE 500MW COMBINED CYCLE PLANT RELAYING**

The 500MW combine cycle plant consists of two (2) 220.6MVA, 18KV gas turbine generator units (CT7A) & (CT7B) with two (2) 220MVA, 18KV/145KV generator step-up transformers (GSU 7A) & (GSU 7B) respectively, plus two (2) 43.4MVA, 18KV/4.16KV unit auxiliary transformers (UAT 7A & UAT 7B). There is one (1) 231MVA, 18KV steam turbine generator unit with a 234MVA 18KV/145KV generator step-up transformer (GSU 7S).

#### **3.1 Generator Protection**

Two (2) state-of-the-art numerical multi-function generator relays, primary and secondary systems from different manufacturers, have been installed for each unit. These relays are connected to the generator CTs, relaying PT's, and the secondary side of the neutral grounding transformer. Each generator relay is wired to trip its own dedicated lockout relay.

The following is a description of the generator protection functions that will be implemented by each relay:

##### **3.1.1. 87G: Generator Differential Protection for Phase Faults.**

The 87G function has variable slope characteristic with a minimum differential current pick-up setting.

##### **3.1.2. 59/27TN: Stator Ground Fault Protection.**

This protection function shall provide 100% ground fault protection for the complete stator winding and the associated neutral grounding system. A conventional 60Hz overvoltage unit (59) will detect ground faults from the generator terminal to about 95% of stator winding (designated as 0-95% protection). A third harmonic undervoltage unit (27TN) will protect the remaining 5% area of the stator winding (designated at 95%-100% protection). This is NYPA's preferred detection scheme to provide 100% stator ground fault protection. It is NYPA's criteria to trip with the operation of the 59 unit and to alarm with the 27TN unit.

##### **3.1.3. 21: Phase Distance Back-Up Protection Function.**

The 21 back-up function utilizes a mho operating characteristic with forward and reverse offset reach settings. Time delay tripping (typical set at 30-60 cycles) will be provided to coordinate with transmission line relaying systems. The relay is designed to accommodate the 30° phase shift between the step-up transformers for system phase faults.

##### **3.1.4. 40: Loss-of-Excitation Protection Function.**

Two independent zones of protection with offset mho characteristic are provided to detect machine loss-of-excitation condition. The

settings of these two zones will coordinate with machine capability curve, minimum excitation limiter curve and steady state stability limit. Independent time delays for each zone are provided. Steady-state stability limits shall be determined using established U.S. relaying practice, factoring in the effect of the GSU transformer.

**3.1.5. 46: Negative Sequence Protection Function.**

Two negative sequence overcurrent alarm and trip threshold functions are provided to properly coordinate with the machine  $I_2^2t$  characteristic.

**3.1.6. 32: Reverse Power Anti-Motoring Protection Function.**

This protection function will detect real power flowing into the generator.

**3.1.7. 24: Voltz/Hz Over-excitation Protection Function.**

The V/Hz protection is mainly used to protect the main step-up transformer from over-excitation conditions. Select inverse time characteristics shall be provided to properly coordinate with the permissible short time excitation (V/Hz) curve of the main step-up transformer.

**3.1.8. 60: Voltage Transformer Blown Fuse Detection.**

In the event of a blown PT fuse or loss-of-potential to the relay, all the protection functions that require voltage inputs for measurement will be blocked from operation. For example, functions 21, 40, 27 and 81U will be blocked. An alarm output contact shall be provided for the 60 relay operation.

**3.1.9. 78: Out-of-Step for Power Swing Detection.**

Two impedance relay functions, an outer unit and inner unit, will track the impedance locus of the generator during an out-of-step swing condition. The objective is to detect that the generator is going out of step and initiate separation from the system during the first swing.

**3.1.10. 81-U/O Under/Over Frequency Detection.**

81U (under-frequency) and 81O (over-frequency) protection will back up the manufacturer's generator control system under and over speed protection.

### 3.2 Generator Step-up (GSU) Transformer Protection

- 3.2.1. Two (2) numerical transformer differential relays (Device 87TP and 87TS), each with both instantaneous (IOC) and time (TOC) elements, each provide instantaneous protection for phase faults in the step-up transformer zone and back-up protection for transformer faults. Each relay is wired to trip its own dedicated lockout relay.
- 3.2.2. A separate numerical transformer neutral-ground overcurrent relay provides the ground TOC backup protection for ground faults on the system high side of the GSU. The operating times of TOC elements will be coordinated with both switchyard line relays and generator relays.

### 3.3 Unit Breaker Protection

- 3.3.1. A separate numerical breaker failure relay (Device 50/62BF) provides protection for the unit breakers. The phase overcurrent function is set above maximum load current and below the minimum three phase fault current. Each breaker failure relay trip its own dedicated BF lockout relay which sends DTT to trip the respective 138KV feeder at CE.

### 3.4 Unit Auxiliary Transformer (UAT) Protection

- 3.4.1. Each UAT transformer 7A & 7B is protected by a numerical transformer differential relay (Device 87T) including both instantaneous (IOC) and time (TOC) overcurrent elements for protection of phase faults in the UAT zone and backup protection for transformer faults. Each relay is wired to trip its associated GSU lockout relay as described in Section 3.1.1.
- 3.4.2. Two (2) separate numerical transformer neutral-ground overcurrent relays for each UAT transformer provides ground TOC backup protection for ground faults on the 480V station service busses 7A & 7C and 7B & 7D for UAT 7A and UAT 7B respectively.

LEGEND	
SYMBOL	APPARATUS
	DISTRIBUTION BUS OR POWER FEED
	LOW VOLTAGE CONTROL, POTENTIAL, OR CURRENT CABLES
	DRAW-OUT DEVICE, PLUG & RECEPTACLE
	RESISTOR
	DISCONNECT SWITCH
	MOTORIZED GROUND SWITCH
	DISCONNECTING SWITCH (MOTOR OPERATED) WITH GROUNDING SWITCH
	FUSE
	POTENTIAL TRANSFORMER
	INSTRUMENT CURRENT TRANSFORMER (WYE CONN.)
	AC GENERATOR
	TWO WINDING POWER TRANSFORMER
	THREE WINDING POWER TRANSFORMER
	NEUTRAL GROUNDING TRANSFORMER WITH RESISTOR IN SECONDARY WINDING.
	GAP TYPE SURGE ARRESTOR
	52G GENERATOR CIRCUIT BREAKER
	GEN DMM GENERATOR DIGITAL MULTI-METER
	M MOTOR
	A AMMETER
	WH WATT HOUR METER
	REV METER REVENUE METER
	V VOLTMETER
	VAR VAR METER
	VARH VARH METER
	SURGE ARRESTOR
	SURGE CAPACITOR
	DFR DIGITAL FAULT RECORDER
	MOTORIZED DOUBLE SIDE BREAK DISCONNECT SWITCH

PROTECTIVE RELAY & DEVICE FUNCTIONS	
27	UNDERVOLTAGE RELAY
50/62EF	BREAKER FAILURE RELAY C60
52G	GENERATOR BREAKER
59BN	BUS GROUND DETECTOR RELAY (ALSTOM P921)
63FP	TRANSFORMER FAULT PRESSURE RELAY (QUALITROL)
63FPX	TRANSFORMER FAULT PRESSURE SWITCH RELAY
86BF	BREAKER FAILURE LOCKOUT RELAY (ELECTROSWITCH)
63BP	TRANSFORMER FAULT PRESSURE RELAY (BUCHHOLZ)
86GRP1	GENERATOR PRIMARY LOCKOUT RELAY (ELECTROSWITCH)
86GRP2	GENERATOR PRIMARY LOCKOUT RELAY (ELECTROSWITCH)
86GRS1	GENERATOR SECONDARY LOCKOUT RELAY (ELECTROSWITCH)
86GRS2	GENERATOR SECONDARY LOCKOUT RELAY (ELECTROSWITCH)
86TP	GSU (PRIMARY PROTECTION) LOCKOUT RELAY (ELECTROSWITCH)
86TS	GSU (SECONDARY PROTECTION) LOCKOUT RELAY (ELECTROSWITCH)
89ND	NEUTRAL GROUND DISCONNECT SWITCH
89SS	LCI STATIC START DISCONNECT SWITCH
96G1	TRANSUCER (G)=WATTS/VARS, (W)=WATTS, (P)=POWER FACTOR, (R)=VARS
51TN3	STEP-UP TRANSFORMER NEUTRAL OVERCURRENT (ALSTOM P122)
51N-X	UNIT AUX TRANSFORMER NEUTRAL OVERCURRENT (ALSTOM P122)
51N-Y	UNIT AUX TRANSFORMER NEUTRAL OVERCURRENT (ALSTOM P122)
57G	GROUND SWITCH FOR GCB
89G	DISCONNECT SWITCH FOR GCB
80055X	BLOCKING CONTACT FROM TURBINE CONTROL PANEL FOR LOSS OF EXCITATION DURING LCI OPERATION

EX2100 FUNCTIONS (FOR GENERATOR)	
30EX	GLOBAL ALARM OUTPUT RELAY
94EX	TRIP OUTPUT RELAY

LOCATION OF EQUIPMENT / DEVICES	
	GENERATOR CONTROL PANEL DEVICE (PRIMARY PROTECTIVE RELAY PANEL)
	GENERATOR COMPARTMENT DEVICE
	GENERATOR TERMINAL ENCLOSURE
	TURBINE CONTROL PANEL DEVICE (MK-VI TCP)
	EX2100
	BY NYPA
	STATIC EXCITATION COMPARTMENT
	LCI / EX2100 COMPARTMENT
	PROTECTION PANEL#1 (SECONDARY PROTECTION-GENERATOR 7A, GSU 7A)
	PROTECTION PANEL#2 (SECONDARY PROTECTION-GENERATOR 7B, GSU 7B)
	PROTECTION PANEL#3 (SECONDARY PROTECTION-GENERATOR 7S, GSU 7S)
	PROTECTION PANEL#4 (PRIMARY PROTECTION-138KV LINE 7A)
	PROTECTION PANEL#5 (PRIMARY PROTECTION-138KV LINE 7B)
	PROTECTION PANEL#6 (PRIMARY PROTECTION-138KV LINE 7S)
	PROTECTION PANEL#7 (SECONDARY PROTECTION-138KV LINE 7A)
	PROTECTION PANEL#8 (SECONDARY PROTECTION-138KV LINE 7B)
	PROTECTION PANEL#9 (SECONDARY PROTECTION-138KV LINE 7S)
	PROTECTION PANEL#10 (PRIMARY AND SECONDARY PROTECTION LA7A)
	PROTECTION PANEL#11 (PRIMARY AND SECONDARY PROTECTION-UA7B)
	GE MCC
	GENERATOR BUSHING

GENERATOR PRIMARY PROTECTION DGP54AACA OR G60 (MAKE: GE)	
50/27	INADVERTENT ENERGIZATION
24A / 24T	VOLTS PER HZ ALARM / TRIP
27P	GENERATOR UNDERVOLTAGE
32-1	REVERSE POWER
40-1, 40-2	LOSS OF EXCITATION
46A / 46T	NEGATIVE SEQUENCE ALARM / TRIP
59P	GENERATOR OVER VOLTAGE
64G1	GENERATOR STATOR GROUND FAULT
81U / 81O	UNDER FREQUENCY / OVER FREQUENCY
87S	GENERATOR DIFFERENTIAL RELAY
VTF	VOLTAGE TRANSFORMER FUSE FAILURE
51V	SYSTEM PHASE FAULT BACKUP
74	DGP ALARM OUTPUT CONTACT
94G	DGP TRIP OUTPUT CONTACT
27TN	THIRD HARMONIC NEUTRAL UNDERVOLTAGE (100% STATOR GROUND FAULT)

GENERATOR STEP-UP TRANSFORMER PRIMARY PROTECTION T60 (MAKE:GE)	
87TP	TRANSFORMER DIFFERENTIAL

GENERATOR STEP-UP TRANSFORMER SECONDARY PROTECTION P634 (MAKE:ALSTOM)	
87TS	TRANSFORMER DIFFERENTIAL
50/51	OVERCURRENT PROTECTION

UNIT AUX TRANSFORMER PRIMARY PROTECTION T60 (MAKE:GE)	
50	INSTANTANEOUS OVERCURRENT (HV)
51	OVERCURRENT (HV)
24	VOLTS PER HERTZ (HV)
50	INSTANTANEOUS OVERCURRENT (LV, X-WINDING)
51	OVERCURRENT (LV, X-WINDING)
50	INSTANTANEOUS OVERCURRENT (LV, Y-WINDING)
51	OVERCURRENT (LV, Y-WINDING)
87T	DIFFERENTIAL

UNIT AUX TRANSFORMER SECONDARY PROTECTION P122 (MAKE:ALSTOM)	
50	INSTANTANEOUS OVERCURRENT (HV)
51	OVERCURRENT (HV)
51GS	GROUND OVERCURRENT (HV)

GENERATOR SECONDARY PROTECTION P343 (MAKE: ALSTOM)	
51V/21	OVERCURRENT/UNDER IMPEDENCE
24	VOLTS PER HERTZ
27	UNDER VOLTAGE
27TN	THIRD HARMONIC NEUTRAL UNDERVOLTAGE (100% STATOR GROUND FAULT)
32	REVERSE POWER
40	LOSS OF EXCITATION
46	NEGATIVE SEQUENCE
50BF	BREAKER FAILURE
50/51	OVERCURRENT
50/27	INADVERTENT ENERGIZATION
59	OVERVOLTAGE
59N	NEUTRAL OVERVOLTAGE
64/67N	RESTRICTED EARTH FAULT
78	POLE SLIP (OUT OF STEP)
810/81U	FREQUENCY (OVER AND UNDER)
87G	GENERATOR DIFFERENTIAL
VTS	VOLTAGE TRANSFORMER SUPERVISION
C1S	CURRENT TRANSFORMER SUPERVISION

138KV LINE PRIMARY PROTECTION P541 (MAKE:ALSTOM)	
85-1	CURRENT DIFFERENTIAL RELAY WITH DTT1
86-1	SECONDARY LINE PROTECTION LOCKOUT RELAY

138KV LINE SECONDARY PROTECTION L90 (MAKE:GE)	
85-2	CURRENT DIFFERENTIAL RELAY WITH DTT2
86-2	SECONDARY LINE PROTECTION LOCKOUT RELAY

- NOTES**
- FOR ONE LINE DIAGRAM OF 4.16KV SWGR REFER TO DWG. E155 & FOR ONE LINE DIAGRAM OF 480V SWGR REFER TO DWG E154.
  - CT7A AND CT7B DRAWINGS ARE BASED ON GE ONE LINE DRAWING NO. 19406899. REV. 8
  - 517S DRAWING IS BASED ON GE ONE LINE DRAWING NO. 20701500. REV B.
  - FOR CT7A AND CT7B, 8955-1 AND 8955-2 ARE INTERLOCKED SUCH THAT ONLY ONE CAN BE CLOSED AT A TIME.

DRAWING RELEASE RECORD				PURPOSE	
REV.	DATE	REL'D BY	PREPARED	APPROVED	
7	07-01-02	VST	ADP/SB	EAC	ISSUED FOR CONSTRUCTION
6	01-31-02	VST	SUB		ISSUED FOR CONFERMED SPEC. #201
5	12-17-01	T/SR	SUB		FOR BID SPEC #201
4	08-06-03	VST	ADP/SB		CONSTRUCTION REVISION FOR D399

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TIME	12:00
BY	
FOR	



FOR CONSTRUCTION

RELAY & METERING DIAGRAM

POLETT: 500V COMBINED CYCLE PLAN

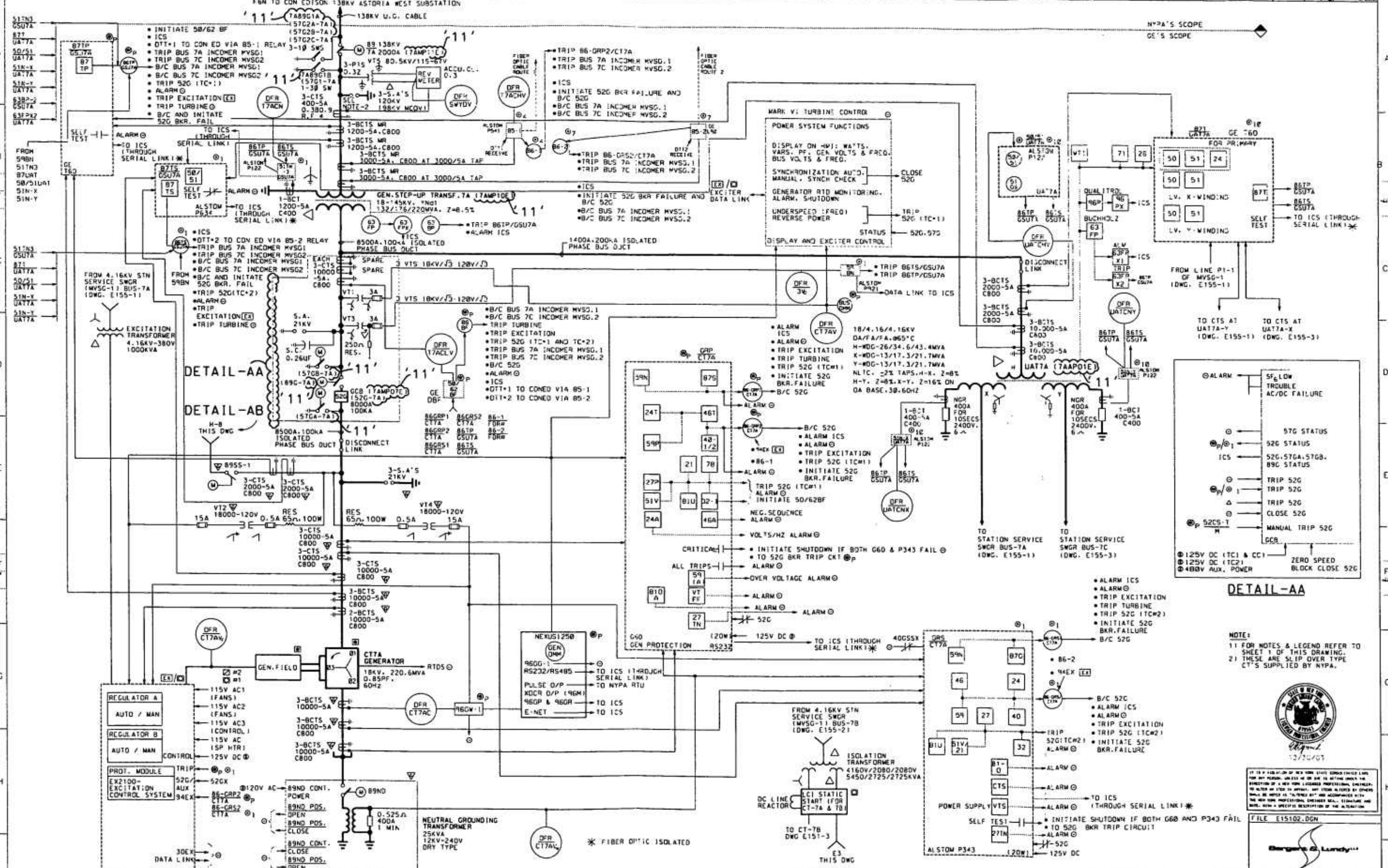
NEW YORK POWER AUTHORITY

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1 2 8

NYPA BAIETTI CAMMIA CADD PROTECTIVE RELAY SYSTEM





**DETAIL-AA**

NOTE:  
 1) FOR NOTES & LEGEND REFER TO SHEET 1 OF THIS DRAWING.  
 2) THESE ARE SLIP OVER TYPE CT'S SUPPLIED BY NYPA.



Bergman & Luchini  
 12/7/01

REV.	DATE	REL'D.	PREPARED	REVIEWED	APPROVED	PURPOSE
8	07-26-03	YST	RDPA/AB	EAC		CONSTRUCTION REVISION FOR D999
9	08-06-03	YST	RDPA/AB	EAC		CONSTRUCTION REVISION FOR D999
10	11-07-03	ARI	RDPA/AB	EAC		CONSTRUCTION REVISION FOR D999
11	12-30-03	ART	RDPA/AB			CONSTRUCTION REVISION FOR D999

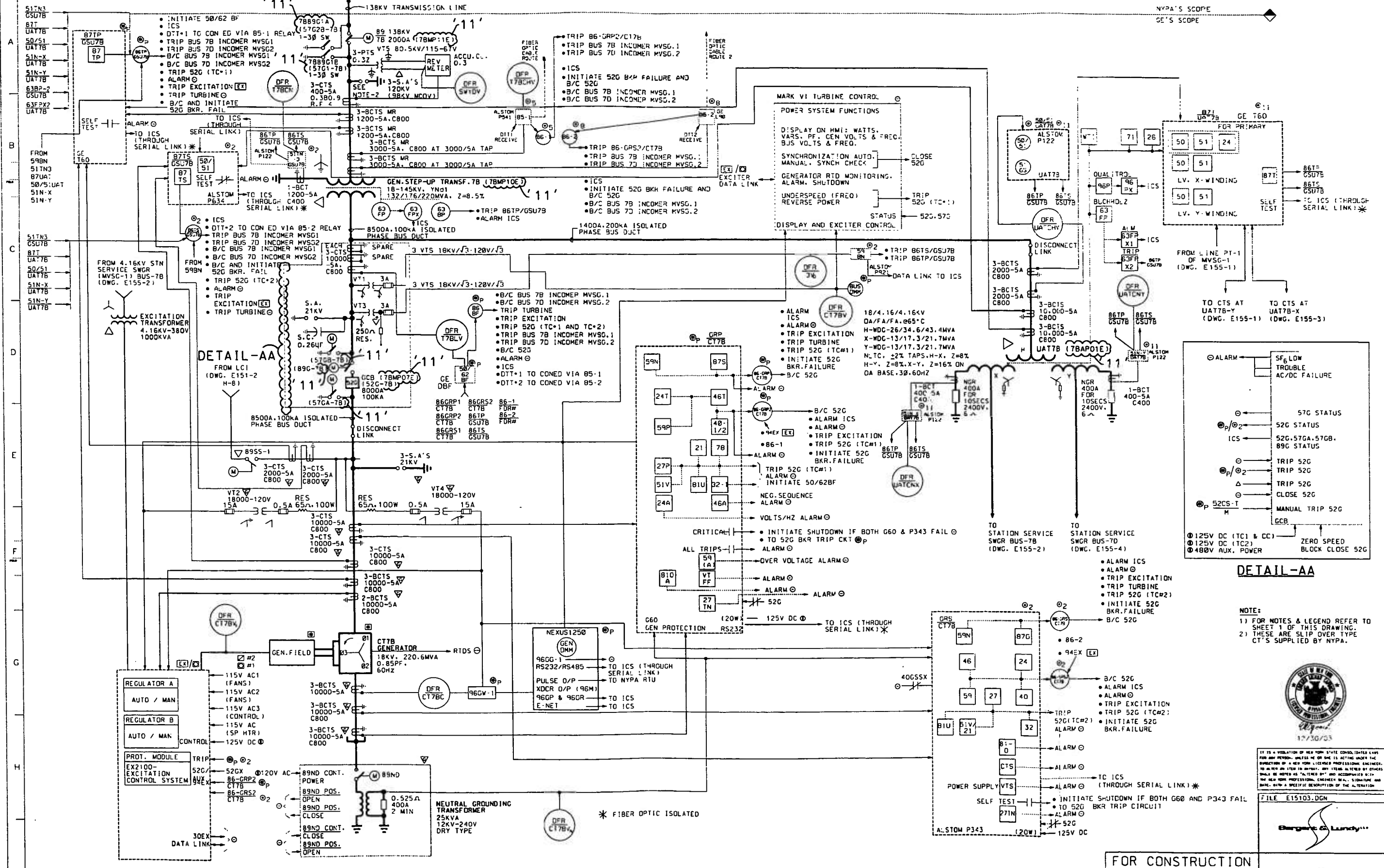
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1						

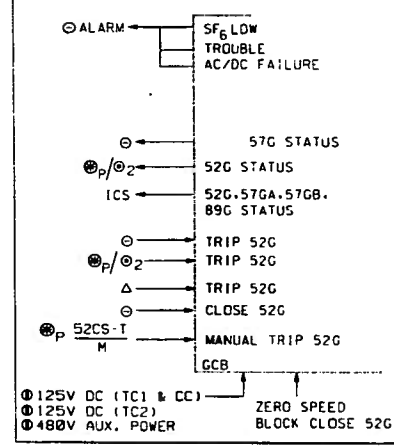
DATE	12/11/01
PROJECT	NYPA POLLETTI 500MW CAPP PROTECTIVE RELAY SYSTEM
DRAWING NO.	E151
REV.	3
DATE	12/11/01
BY	YST
CHECKED	YST
DESIGNED	YST
DRAWN	YST
SCALE	
PROJECT NO.	510X0009
PROJECT NAME	NYPA POLLETTI 500MW CAPP PROTECTIVE RELAY SYSTEM
PROJECT LOCATION	
PROJECT OWNER	NEW YORK POWER AUTHORITY

NYPA POLETTI 500MW CAPP PROTECTIVE RELAY SYSTEM

F85 TO CON EDISON 138KV ASTORIA WEST SUBSTATION



DETAIL-AA



DETAIL-AA

NOTE:  
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 Robert J. Lundy  
 17730/03

FOR CONSTRUCTION

RELAY & METERING DIAGRAM FOR CT7B & UAT7B

GENERAL ELECTRIC POWER PLANT ENGINEERING POWER PLANT SYSTEMS DEPARTMENT  
 POLETTI 500MW COMBINED CYCLE PLANT  
 NEW YORK POWER AUTHORITY 510X0009F E151 3 4 11

REV.	DATE	REV. D.	PREPARED	REVIEWED	APPROVED	PURPOSE
8	02-26-03	VST	RDP/AB	EAC		CONSTRUCTION REVISION FOR D999
9	08-06-03	VST	RDP/AB	EAC		CONSTRUCTION REVISION FOR D999
10	11-07-03	ART	RDP/AB	EAC		CONSTRUCTION REVISION FOR D999
11	12-30-03	VST	RDP/AB	EAC		CONSTRUCTION REVISION FOR D999

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NYPA POLETTI 500MW CAPP PROTECTIVE RELAY SYSTEM

FIG. 10. 220V FEEDER LINE/245/100V/450V SUBSTATION

START SCOPE  
STOP SCOPE

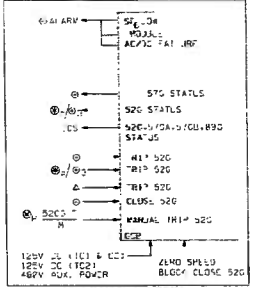
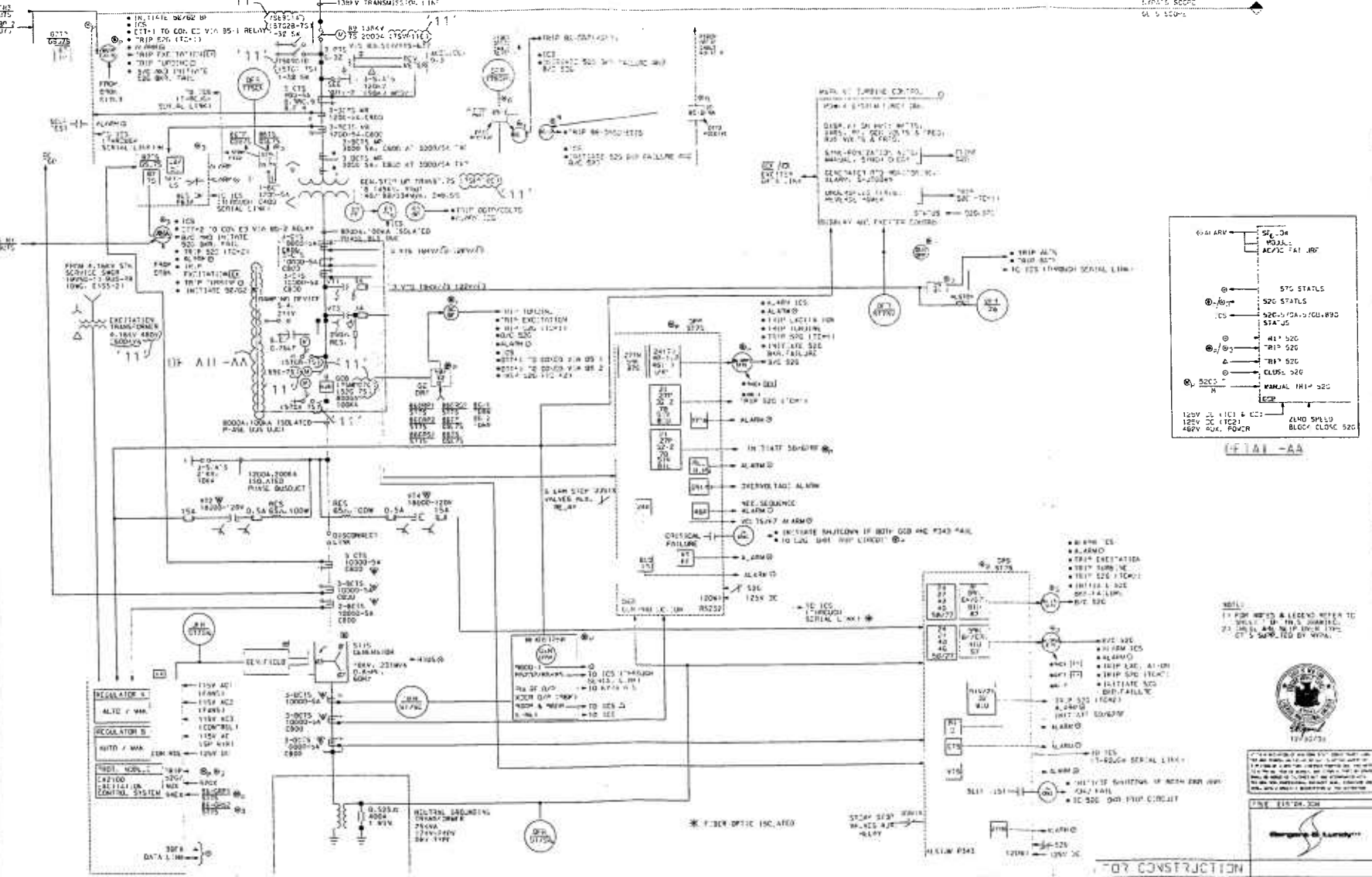


FIG. 10A - AA

NOTE:  
 1. FOR WEATS & LEGEND REFER TO SHEET 10-B. THIS SHEET IS A PART OF THE 220V FEEDER LINE/245/100V/450V SUBSTATION.



FOR CONSTRUCTION  
 NEW YORK POWER AUTHORITY  
 NEW YORK POWER AUTHORITY  
 NEW YORK POWER AUTHORITY

NO.	DATE	BY	REVISION	DESCRIPTION
1	11-11-64	WJ	REVISED	CONSTRUCTION
2	11-11-64	WJ	REVISED	CONSTRUCTION
3	11-11-64	WJ	REVISED	CONSTRUCTION
4	11-11-64	WJ	REVISED	CONSTRUCTION
5	11-11-64	WJ	REVISED	CONSTRUCTION
6	11-11-64	WJ	REVISED	CONSTRUCTION
7	11-11-64	WJ	REVISED	CONSTRUCTION
8	11-11-64	WJ	REVISED	CONSTRUCTION
9	11-11-64	WJ	REVISED	CONSTRUCTION
10	11-11-64	WJ	REVISED	CONSTRUCTION
11	11-11-64	WJ	REVISED	CONSTRUCTION
12	11-11-64	WJ	REVISED	CONSTRUCTION


NYP& POLETTI 500MW CAPP PROTECTIVE RELAY SYSTEM



SIZE B DWG NO 365B7110 SH 1 REV -

REVISIONS			
REV	DESCRIPTION	DATE	APPROVED


REVISE ON CAD ONLY  
UG PART: 365B7110G0001



## Hydrogen - Cooled Generator


HYDROGEN-COOLED GENERATOR NO. 337X305		RATING
2 POLES	3 PHASE WYE CONN. 60HERTZ	3600 RPM GAS 98% PURITY AT 30P51G
TOTAL TEMPERATURE AT RATING		KVA: 220600
GUARANTEED NOT TO EXCEED:		ARMATURE AMPS: 7076
100 °C ON ARMATURE BY DETECTOR		ARMATURE VOLTS: 18000
110 °C ON FIELD BY RESISTANCE		FIELD AMPS: 1952
MAXIMUM COLD GAS TEMPERATURE: 40 °C		EXCITATION VOLTS: 315
INLET LIQUID: 33 °C		POWER FACTOR: 0.85

CAUTION BEFORE INSTALLING, OPERATING, OR DISMANTLING, READ INST. GEK-110103



GE Power Systems  
General Electric Company

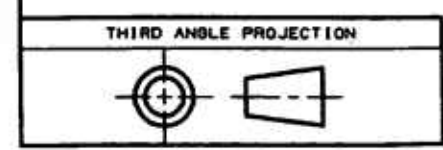
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UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES. TOLERANCES ON: 2 PL DECIMALS ± 3 PL DECIMALS ± ANGLES ± FRACTIONS ±	SIGNATURES DRAWN J. HELGUEROS CHECKED F.SCHROEDER ENGRG ISSUED F.SCHROEDER	DATE 02-09-06 02-09-09  02-09-09	 <b>GE Power Generation</b> GENERAL ELECTRIC COMPANY GENERATOR Schenectady, NY
<h3>DATA PLATE</h3> <p>FIRST MADE FOR 337X305 <span style="float: right;">B7FO</span></p>			DISTR TO
SIM TO: 361B9497	SCALE NONE	SHEET 1	SIZE B CAGE CODE DWG NO 365B7110

DT-2N

N6DC

NYPA POLETTI 500MW CCPP CTG #1 NAMEPLATE

NOTE:

1. MAKE FROM N.P. 275800. DATA TO BE ENGRAVED OR ETCHED. LETTER SIZE IS .19 AND STYLE SHALL BE "LEROY" PER NAMEPLATE DRAWING. DO NOT ENGRAVE OR ETCH ENCIRCLED LETTER "A". SUBSTITUTE THE APPROPRIATE TURBINE NUMBER FROM THE "NAMEPLATE UNIT RATING" TABLE. DATA AS IDENTIFIED BELOW MUST BE LOCATED IN APPROXIMATE CENTER OF ALLOCATED SPACE.

REVISIONS			
REV	DESCRIPTION	DATE	APPROVED

REVISE ON CAD ONLY  
UG PART: GR0767-A004  
( SPEC: 357B8071 )

GE GAS TURBINE

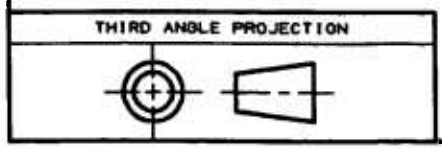
GREENVILLE, S.C. USA

NO:   A   AIR IN: 59° F ALT: 20 FT  
 BASE: N/A PEAK: N/A FUEL: NATURAL GAS  
 TURBINE EXHAUST: BASE: N/A PEAK: N/A PRESS: 17.8 in H2O  
 CPRSR: STAGES: 18 RPM 3600 CPRSR TURBINE: STAGES: 3  
 POWER TURBINE: STAGES: N/A RPM N/A

**CAUTION!** BEFORE INSTALLING, OPERATING, OR DISMANTLING-READ GEX 110103

SCHENECTADY, NY - GREENVILLE, SC  
N.P. 275800

NAMEPLATE UNIT RATING					
PT	TURBINE NO. (A)	PT	TURBINE NO. (A)	PT	TURBINE NO. (A)
1	298125				
2	298126				



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UNLESS OTHERWISE SPECIFIED	SIGNATURES	DATE	GE Power Generation GENERAL ELECTRIC COMPANY GAS TURBINE Greenville, SC
DIMENSIONS ARE IN INCHES.	DRAWN FRANK J NORTH II	02-12-12	
TOLERANCES ON:	CHECKED FRANK J NORTH II	02-12-10	NAMEPLATE, UNIT RATING FIRST MADE FOR ML-7A1WFA255-1T2 A004
2 PL DECIMALS ± -	ENGRG NOEL MENDEZ	02-11-27	
3 PL DECIMALS ± -	ISSUED FRANK J NORTH II	12-12-02	
ANGLES ± - -	QUALITY FRANK J NORTH II	02-12-02	
FRACTIONS ± - ✓			
APPLIED PRACTICES 348A9200	SIM TO: 357B2889	SCALE NONE	SHEET 1


DT-1N

NYPA POLETTI 500MW CCPP GT#1 NAMEPLATE

SIZE Dwg NO 365B7112 SH 1 REV --

REVISIONS			
REV	DESCRIPTION	DATE	APPROVED

REVISE ON CAD ONLY  
UG PART: 365B7112G0001



## Hydrogen - Cooled Generator

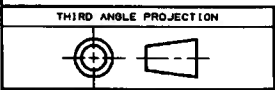
HYDROGEN-COOLED GENERATOR NO. 337X304		RATING	
2 POLES	3 PHASE WYE CONN.	60 HERTZ	3600 RPM GAS 98% PURITY AT 30PSIG
TOTAL TEMPERATURE AT RATING		KVA:	220600
GUARANTEED NOT TO EXCEED:		ARMATURE AMPS:	7076
100 °C ON ARMATURE BY DETECTOR		ARMATURE VOLTS:	18000
110 °C ON FIELD BY RESISTANCE		FIELD AMPS:	1952
MAXIMUM COLD GAS TEMPERATURE: 40 °C		EXCITATION VOLTS:	315
INLET LIQUID: 33 °C		POWER FACTOR:	0.85

CAUTION BEFORE INSTALLING, OPERATING, OR DISMANTLING, READ INST. GEK-110103

<div style="border: 1px solid black; padding: 5px; display: flex; justify-content: space-between;"> <span>GE Power Systems General Electric Company</span> <span>Schenectady, New York Made In U.S.A.</span> </div>	
---	--


APPLIED PRACTICES	348A9200
IT. NOMENCLATURE	IDENT
LIST OF COMPLEMENTARY DOCUMENTS	

61



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BOM ISSUED

UNLESS OTHERWISE SPECIFIED	SIGNATURES	DATE	GENERAL ELECTRIC COMPANY	
DIMENSIONS ARE IN INCHES.	DRAWN J.HELGUEROS	02-09-09	 GE Power Generation Schenectady, NY	
TOLERANCES ON:	CHECKED F.SCHROEDER	02-09-10		
2 PL. DECIMALS ±	ENGRS		<b>DATA PLATE</b> FIRST MADE FOR 337X304 B7F0	
3 PL. DECIMALS ±	ISSUED F.SCHROEDER	02-09-10		
ANGLES ±			SIZE	DWG NO
FRACTIONS ±			<b>B</b>	365B7112
			SIM TO: 361B9497	SCALE NONE
				SHEET 1

DT-2N

N6DC

NYPA POLETTI 500MW CAPP CTG.#2 NAMEPLATE

SIZE **B** DWG NO 357B8072 SM REV -


FORMAT\_WIZARD 2.1

NOTE:

1. MAKE FROM N.P. 275800. DATA TO BE ENGRAVED OR ETCHED. LETTER SIZE IS .19 AND STYLE SHALL BE "LEROY" PER NAMEPLATE DRAWING. DO NOT ENGRAVE OR ETCH ENCIRCLED LETTER "A". SUBSTITUTE THE APPROPRIATE TURBINE NUMBER FROM THE "NAMEPLATE UNIT RATING" TABLE. DATA AS IDENTIFIED BELOW MUST BE LOCATED IN APPROXIMATE CENTER OF ALLOCATED SPACE.

REVISIONS			
REV	DESCRIPTION	DATE	APPROVED

REVISE ON CAD ONLY  
UG PART: GR0767-A005  
( SPEC: 357B8072 )



**GE GAS TURBINE**

GREENVILLE, S.C. USA

NO: <sup>Ⓐ</sup> \_\_\_\_\_ AIR IN: 59° F ALT: 20 FT


BASE: N/A PEAK: N/A FUEL: AVIATION KEROSENE

TURBINE EXHAUST: BASE: N/A PEAK: N/A PRESS: 17.8 In H2O

CPRSR: STAGES: 18 RPM 3600 CPRSR TURBINE: STAGES: 3


POWER TURBINE: STAGES: N/A RPM N/A

**CAUTION!** BEFORE INSTALLING, OPERATING, OR DISMANTLING-READ GEX 110103

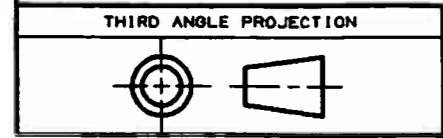


SCHENECTADY, NY - GREENVILLE, SC

N.P. 275800




NAMEPLATE UNIT RATING					
PT	TURBINE NO. Ⓐ	PT	TURBINE NO. Ⓐ	PT	TURBINE NO. Ⓐ
1	298125				
2	298126				



DT-IN

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UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES. TOLERANCES ON: 2 PL DECIMALS ± - 3 PL DECIMALS ± - ANGLES ± - - FRACTIONS ± - ✓	SIGNATURES	DATE	 GE Power Generation GENERAL ELECTRIC COMPANY GAS TURBINE Greenville, SC
	DRAWN FRANK J NORTH II	02-12-10	
APPLIED PRACTICES 348A9200	CHECKED FRANK J NORTH II	02-12-10	NAMEPLATE, UNIT RATING FIRST MADE FOR ML-7A1WFA255-1T2 A005
	ENGRO NOEL MENDEZ	02-11-27	
	ISSUED FRANK J NORTH II	12-12-02	
	QUALITY FRANK J NORTH II	02-12-02	
SIM TO: 357B2889	SCALE NONE	SHEET 1	SIZE <b>B</b> CAGE CODE _____ DWG NO 357B8072 DISTR TO

NYPA POLETTI 500MW CCPP GT#2 NAMEPLATE

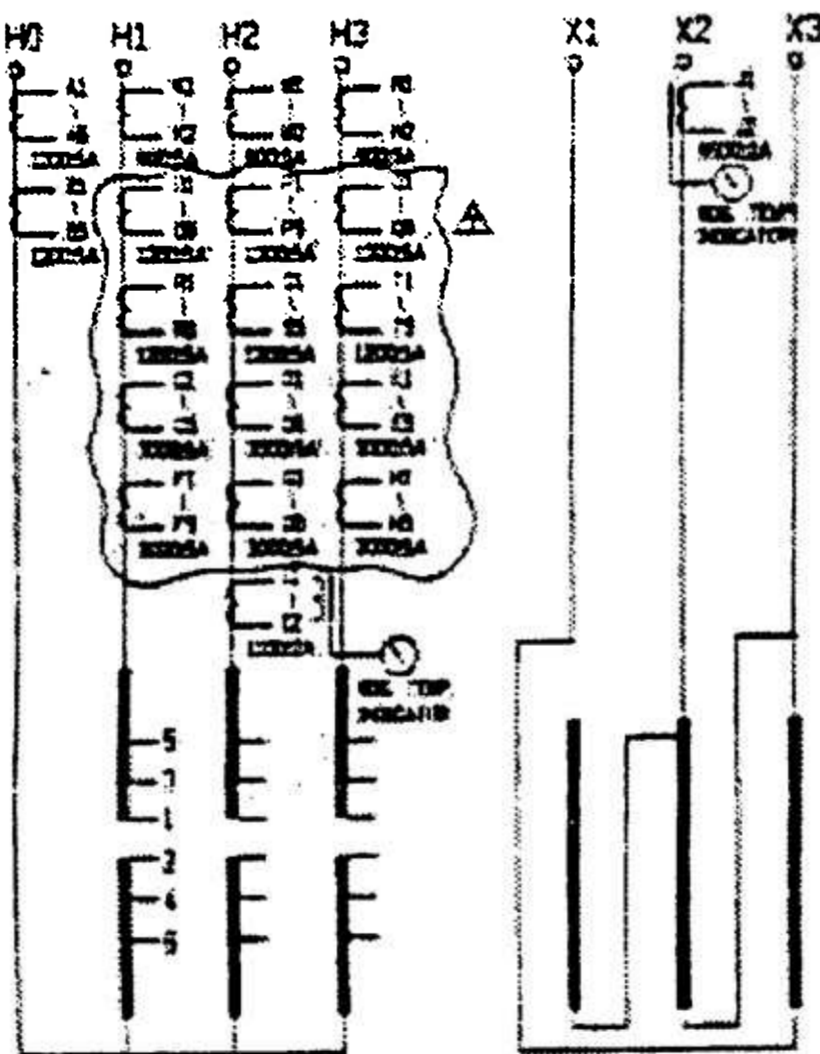


# TRANSFORMER

3 PHASE		50 HZ	CORE FORM	STANDARD IEEE C57.12					
TYPE OF COOLING		ONAN/ONAF/ONAF		OUTDOOR USE					
WINDING	CONN. TO	CAPACITY (MVA)			VOLTAGE RATING (KV)	CURRENT (A)			IMPULSE (B/L)
		ONAN	ONAF	ONAF		ONAN	ONAF	ONAF	
HV	H1, H2, H3	132	176	220	145	525	701	875	650 KV
LV	X1, X2, X3				15	4234	5645	7057	NEUTRAL 150 KV 150 KV

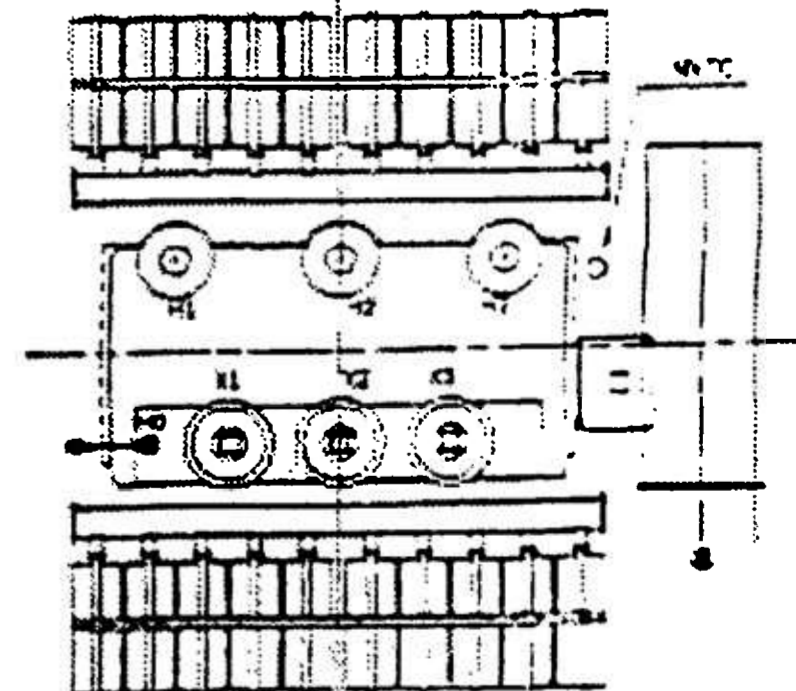
LOAD CAPABILITY 40% AMBIENT TEMP.	INSULATING OIL	MINERAL OIL	APPROXIMATE WEIGHTS	
WINDING MATERIAL	COPPER		COPE & WINDINGS	174,605 LB
TEMP. RISE	65 °C		TANK & FITTINGS	100,710 LB
IMPEDANCE	%		OIL 11,200 GALLONS	84,105 LB
WTC AT 132 MVA			OIL FOR MAIN TANK 9,750 GALLONS	73,345 LB
			OIL FOR RADIATORS 1,000 GALLONS	7,845 LB
			OIL FOR CONDENSATOR 1,250 GALLONS	9,810 LB
			TOTAL WEIGHT	259,515 LB

POSITION	CT NO.	CURRENT MULTI. RATIO										ACCURACY
		SECONDARY CONNECTIONS										
S	A	12005A	10005A	8005A	6005A	5005A	4005A	3005A	2005A	1005A	1005A	200
		X1-X5	X2-X5	X3-X5	X1-X4	X2-X4	X3-X4	X4-X5	X1-X2	X1-X3	X2-X3	
S	B	12005A	10005A	8005A	6005A	5005A	4005A	3005A	2005A	1005A	200	
		X1-X5	X2-X5	X3-X5	X1-X4	X2-X4	X3-X4	X4-X5	X1-X2	X1-X3	X2-X3	
H	C	30005A	25005A	22005A	20005A	15005A	12005A	10005A	8005A	5005A	3005A	500
		X1-X5	X1-X4	X1-X3	X2-X5	X2-X4	X2-X3	X1-X2	X3-X5	X4-X5	X1-X4	
S	D	11002A										-
		X1-X2										
S	E	5002A										-
		X1-X2										
H	F	6005A										500
		X1-X2										
H	G	12005A	10005A	8005A	6005A	5005A	4005A	3005A	2005A	1005A	200	
		X1-X5	X2-X5	X3-X5	X1-X4	X2-X4	X3-X4	X4-X5	X1-X2	X1-X3	X2-X3	



VOLTAGE (KV)	CURRENT (A)			NO. VOLTAGE TAP CHANGER
	ONAN/ONAF	ONAF	ONAF	
152.250	501	667	834	1
148.625	513	684	855	2
145.000	528	701	876	3
141.375	539	719	896	4
137.750	553	733	922	5

WITHSTAND COMPLETE TRANSFORMER 1.5PSI PRESSURE



PURCHASER: General Electric Company  
 DATE OF TEST: Oct. 2002  
 YEAR OF MANUFACTURE: Oct. 2002  
 PURCHASER'S ORDER NUMBER: 131131173-100  
 SERIAL NO.: 01007

**FORTUNE ELECTRIC CO., LTD.**  
 MADE IN TAIWAN

INSTRUCTION MANUAL: 24-9505  
 IR-NL-22-5775

SYM	DATE	REVISIONS
Δ	10/2/02	1. Initial design
Δ	10/9/02	2. Change with GE drawing
Δ	5/13/02	3. Add ECTOPROTECT for 1st tap change
Δ	5/07/02	4. Add BECTOPROTECT for 1st tap change
Δ	1/16/02	5. Change drawing to alter
Δ	1/21/01	6. APPROXIMATE WEIGHTS CHANGE
Δ	1/23/01	7. HV DCI SETPOINT CHANGED

MATERIAL: STAINLESS STEEL PLATE: 161-300x500

000-114118F

UNIT	SCALE
in/mm	1:1

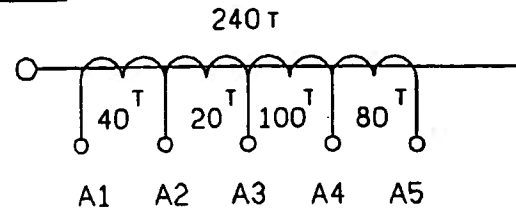
DATE: Y. M. D.	03 - 12 - 01
DRW: Y. C. Hsu	
CHKD: S. W. MAHO	03 - 12 - 01
APPROV: I. C. CHENG	03 - 12 - 01



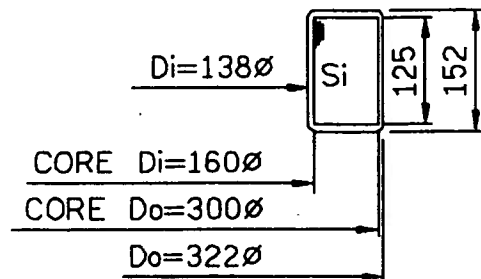
GENERAL ELECTRIC INTERNATIONAL, INC.  
 POWER PLANT SYSTEMS DEPARTMENT  
 FORTUNE ELECTRIC CO., LTD.



HO



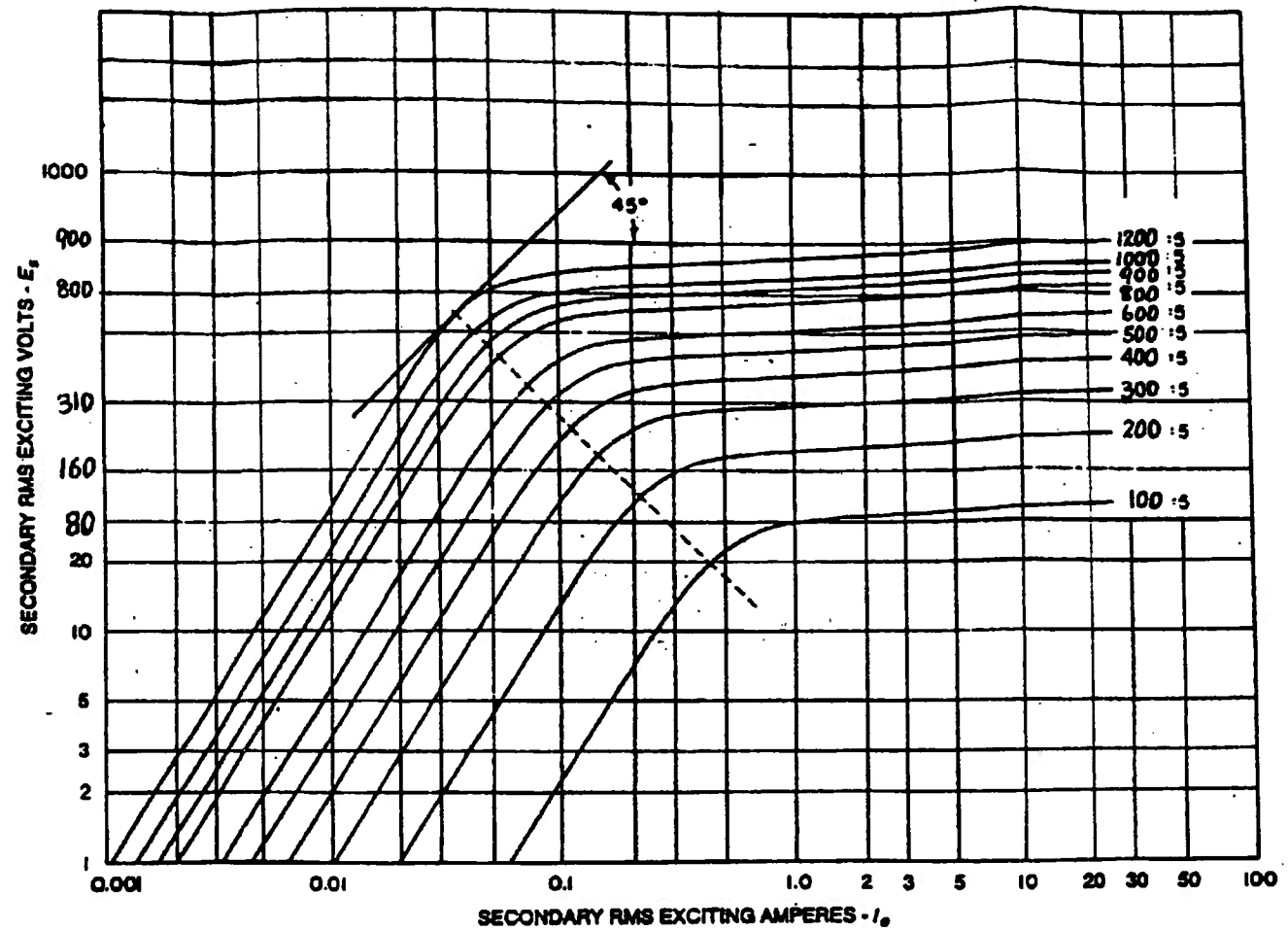
CT NO.	MULTI RATIO	SECONDARY CONNECTIONS	ACCURACY	CAPACITY (VA)
A	1200/5A	X1-X5	C800	200
	1000/5A	X2-X5		
	900/5A	X3-X5		
	800/5A	X1-X4		
	600/5A	X2-X4		
	500/5A	X3-X4		
	400/5A	X4-X5		
	300/5A	X1-X3		
	200/5A	X1-X2		
	100/5A	X2-X3		



SECONDARY RESISTANCE ON MAX.TAP 5.1 Ω (AT 75°C)

CORE AREA 8750 mm<sup>2</sup>

CORE MEAN LENGTH 730 mm

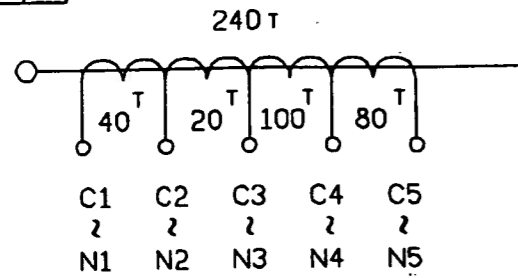


PRELIMINARY	POLETTI
TITLE	GENERAL ELECTRIC INTERNATIONAL, INC.
CURRENT TRANSFORMER DATA AND EXCITATION CURVE	POWER PLANT ENGINEERING
132/176/220MVA TRANSFORMER	POWER PLANT SYSTEMS DEPARTMENT
PROJECT	POLETTI 500 MW COMBINED CYCLE PLANT
MADE FOR	NEW YORK POWER AUTHORITY
TYPE IDENT. NO.	DRAWING NO.
	23A3368A 2/3
SHEET	REV.
DWN. Y. C. Hsu 03-12-'01	FORTUNE ELECTRIC CO., LTD.
CHKD. S. M. WANG 03-12-'01	
APPD. I. C. CHENG 03-12-'01	

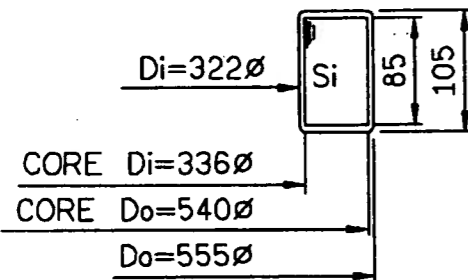
SYM.	DATE	REVISIONS	REVD.	CHKD.	APPD.
△					
△					

SCALE 1:1 UNIT in./mm  
PROJECTION

H1,H2,H3



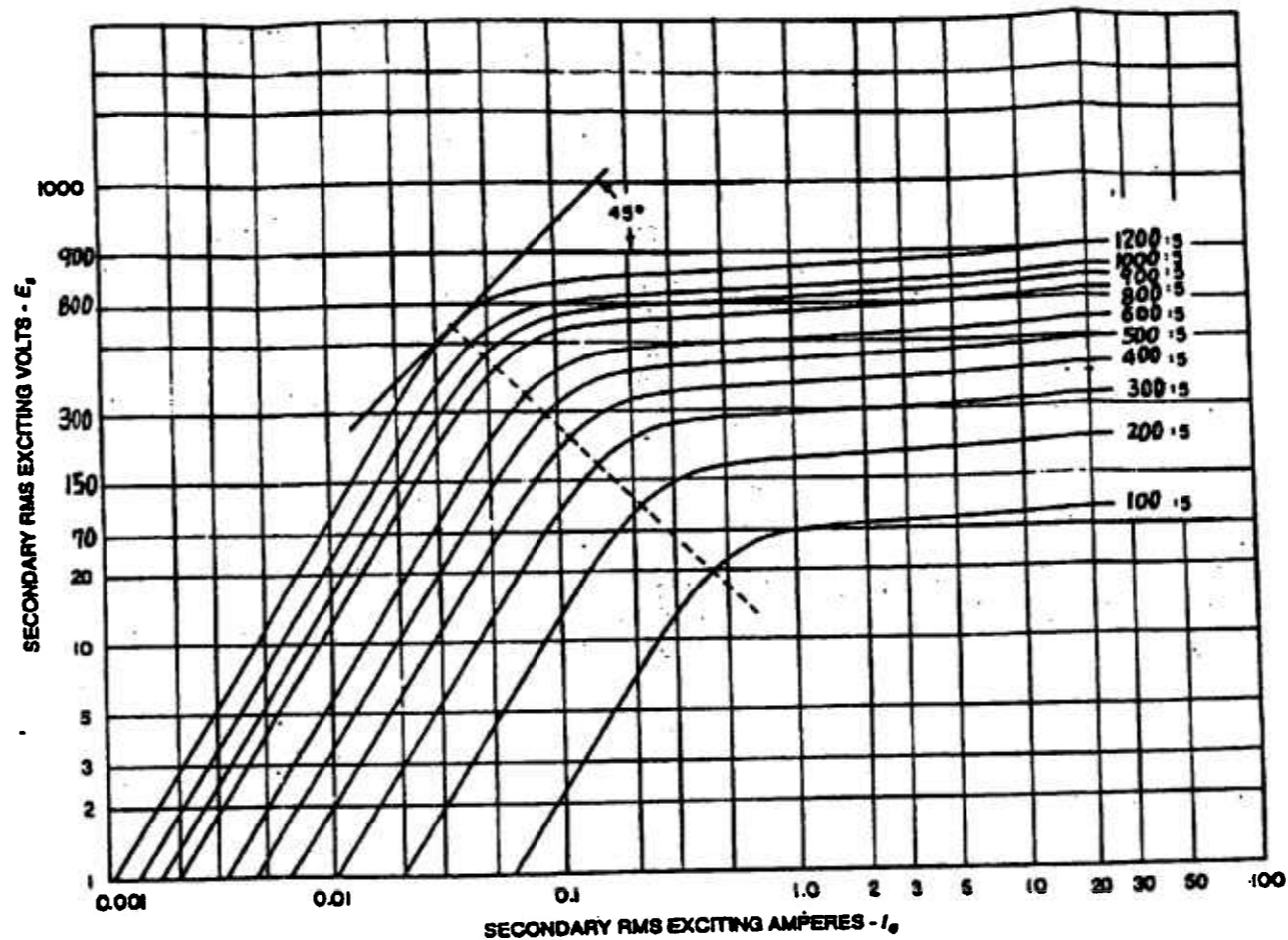
CT NO	MULTI RATIO	SECONDARY CONNECTIONS	ACCURACY	CAPACITY (VA)
C D E F G H I J K L M N	1200/5A	X1-X5	C800	200
	1000/5A	X2-X5		
	900/5A	X3-X5		
	800/5A	X1-X4		
	600/5A	X2-X4		
	500/5A	X3-X4		
	400/5A	X4-X5		
	300/5A	X1-X3		
	200/5A	X1-X2		
	100/5A	X2-X3		



SECONDARY RESISTANCE ON MAX.TAP 5.0 Ω (AT 75°C)

CORE AREA 8670 mm<sup>2</sup>

CORE MEAN LENGTH 1380 mm



SYM.	DATE	REVISIONS	REVD.	CHKD.	APPD.
△					
△					

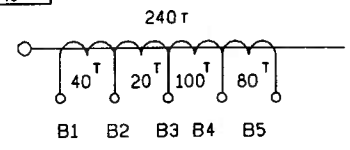
SCALE 1:1 UNIT in./mm  
PROJECTION

PRELIMINARY	POLETTI
TITLE CURRENT TRANSFORMER DATA AND EXCITATION CURVE	GENERAL ELECTRIC INTERNATIONAL, INC.
PROJECT 132/176/220MVA TRANSFORMER	POWER PLANT ENGINEERING
MADE FOR POLETTI 500 MW COMBINED CYCLE PLANT	POWER PLANT SYSTEMS DEPARTMENT
NEW YORK POWER AUTHORITY	PVE IDENT. NO. DRAWING NO. SHEET REV.
	23A3368A 1/3
DWN. Y. C. Hsu 03-12-'01	
CHKD. S. M. WANG 03-12-'01	
APPD. I. C. CHENG 03-12-'01	

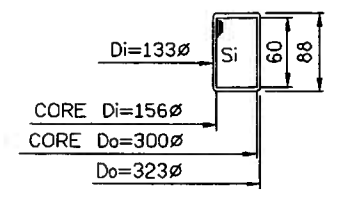
NYPA POLETTI 500MW CCPP CTG GSU 7A & 7B CT SAT CURVES

A  
B  
C  
D  
E

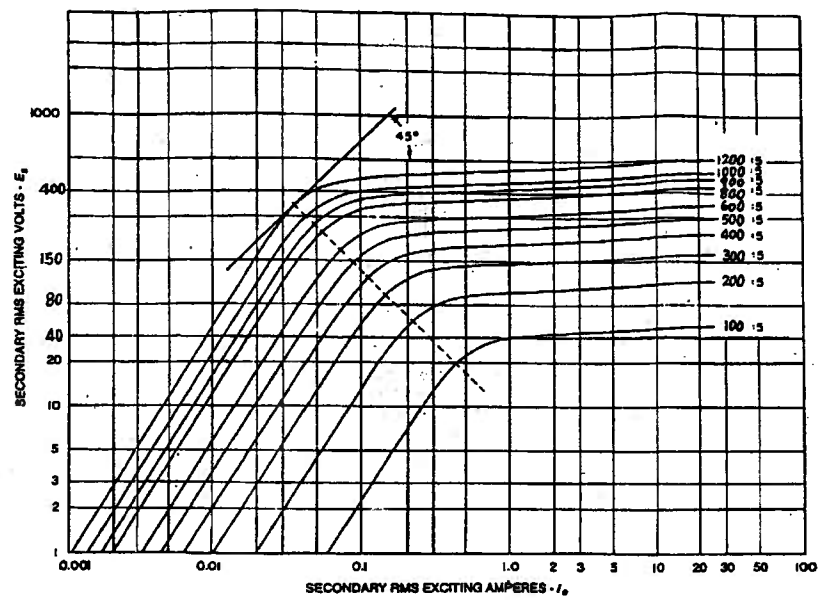
H0



CT NO.	MULTI RATIO	SECONDARY CONNECTIONS	ACCURACY	CAPACITY (VA)
B	1200/5A	X1-X5	C400	100
	1000/5A	X2-X5		
	900/5A	X3-X5		
	800/5A	X1-X4		
	600/5A	X2-X4		
	500/5A	X3-X4		
	400/5A	X4-X5		
	300/5A	X1-X3		
	200/5A	X1-X2		
	100/5A	X2-X3		



SECONDARY RESISTANCE ON MAX.TAP 2.8 Ω (AT 75°C)  
 CORE AREA 4320 mm<sup>2</sup>  
 CORE MEAN LENGTH 720 mm




SYM.	DATE	REVISIONS	REVD.	CHKD.	APPD.	SCALE	UNIT
△						1:1	in./mm
△						PROJECTION	

PRELIMINARY		POLETTI	
TITLE CURRENT TRANSFORMER DATA AND EXCITATION CURVE 132/176/220MVA TRANSFORMER		GENERAL ELECTRIC INTERNATIONAL, INC. POWER PLANT ENGINEERING	
PROJECT POLETTI 500 MW COMBINED CYCLE PLANT		POWER PLANT SYSTEMS DEPARTMENT	
MADE FOR NEW YORK POWER AUTHORITY	PPE IDENT. NO.	DRAWING NO. 23A3368A 3/3	SHEET CONT. OF 3
	DWN. Y. C. Hsu 03-12-'01	FORTUNE ELECTRIC CO., LTD.	
	CHKD. S. M. WANG 03-12-'01		
	APPD. I. C. CHENG 03-12-'01		

SIZE DWG NO 365B1836 SH REV

REVISIONS			
REV	DESCRIPTION	DATE	APPROVED

REVISE ON CAD ONLY  
UG PART: 365B1836G0001



## Steam Turbine Generator Unit

---

### TURBINE

TURBINE NO. 270T606    RATING: 190787 KW    3600 RPM    23 STAGES  
 STEAM CONDITIONS: PRESSURE 1800 PSIA    TEMPERATURE 1050 °F    EXHAUST PRESSURE: 2.42" HgA

---

### GENERATOR

HYDROGEN-COOLED GENERATOR NO. 290T606		RATING
2 POLES 3 PHASE WYE CONN. 60 HERTZ	GAS 98% PURITY AT	30 PSIG
TOTAL TEMPERATURE AT RATING	KVA:	231000
GUARANTEED NOT TO EXCEED:	ARMATURE AMPS:	7409
100 °C ON ARMATURE BY DETECTOR	ARMATURE VOLTS:	18000
110 °C ON FIELD BY RESISTANCE	FIELD AMPS:	1843
MAXIMUM COLD GAS TEMPERATURE: 42 °C	EXCITATION VOLTS:	350
INLET WATER: 35 °C	POWER FACTOR:	0.85

CAUTION! BEFORE INSTALLING, OPERATING, OR DISMANTLING, READ INST. GEK-110103


GE Power Systems  
General Electric Company

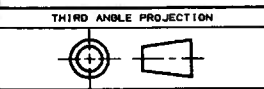
Schenectady, New York  
Made In U.S.A.

APPLIED PRACTICES	348A9200
IT.	NOMENCLATURE IDENT
LIST OF COMPLEMENTARY DOCUMENTS	

(G1)

BOM ISSUED

UNLESS OTHERWISE SPECIFIED	SIGNATURES	DATE	 GE Power Generation GENERAL ELECTRIC COMPANY GENERATOR Schenectady, NY
DIMENSIONS ARE IN INCHES.	DRAWN L. MARTINEZ	02-07-11	
TOLERANCES ON:	CHECKED F. SCHROEDER	02-07-17	DATA PLATE FIRST MADE FOR 290T606    B7FO
2 PL. DECIMALS ±	ENGRG		
3 PL. DECIMALS ±	ISSUED F. SCHROEDER	02-07-17	
ANGLES ±			SIZE CABE CODE    DWG NO
FRACTIONS ±			B    365B1836
	SIN TO: 362B7265	SCALE NONE	SHEET 1



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DT-2N

N6DC

NYPA POLETTI 500MW CCPP STG NAMEPLATE



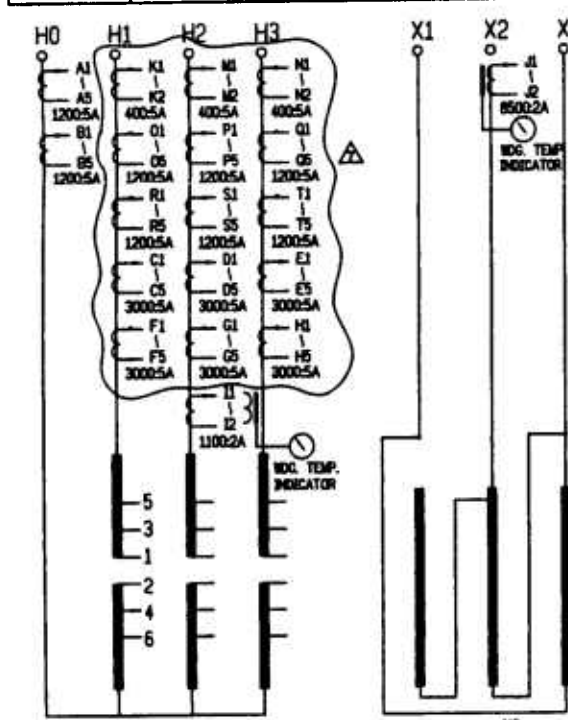
# TRANSFORMER

3 PHASE 60 HZ CORE FORM STANDARD IEEE C57.12  
 TYPE OF COOLING ONAN/ONAF/ONAF OUTDOOR USE

WINDING	CONN. TO	CAPACITY (MVA)			VOLTAGE RATING (kV)	CURRENT (A)			IMPULSE (BIL)
		ONAN	ONAF	ONAF		ONAN	ONAF	ONAF	
HV	H1, H2, H3	140	188	234	145	557	749	932	650 kV
LV	X1, X2, X3				18	4491	6030	7506	150 kV

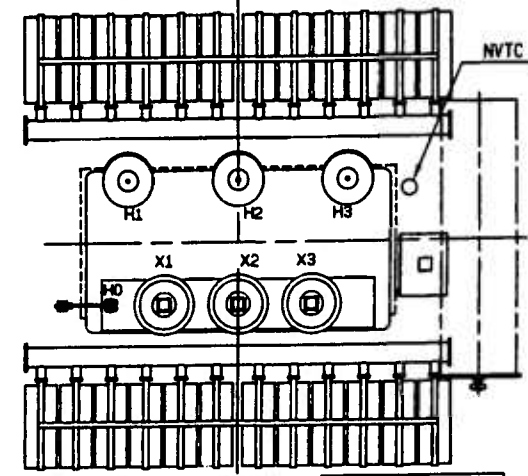
LOAD CAPABILITY 40°C AMBIENT TEMP.		INSULATING OIL	MINERAL OIL	APPROXIMATE WEIGHTS	
WDC. TEMP. RISE BY RESISTANCE	65 °C	WINDING MATERIAL	COPPER	CORE & WINDINGS	183,565 lbs
OIL TEMP. RISE	65 °C	INSULATING OIL IN MAIN TANK	MINERAL OIL PCB FREE	TANK & FITTINGS	113,260 lbs
IMPEDANCE	%	OIL 11,950 GALLONS 89,770 lbs			
65°C AT 140 MVA		OIL FOR MAIN TANK 6,830 GALLONS 51,275 lbs			
		OIL FOR RADIATORS 3,870 GALLONS 29,090 lbs			
		OIL FOR CONSERVATOR 1,250 GALLONS 9,405 lbs			
		TOTAL WEIGHT 386,595 lbs			

POSITION	CT NO	CURRENT MULTI RATIO SECONDARY CONNECTIONS										ACCURACY
		1200:5A	1000:5A	900:5A	800:5A	600:5A	500:5A	400:5A	300:5A	200:5A	100:5A	
H0	A	X1-X5	X2-X5	X3-X5	X1-X4	X2-X4	X3-X4	X4-X5	X1-X3	X1-X2	X2-X3	C800
H0	B	X1-X5	X2-X5	X3-X5	X1-X4	X2-X4	X3-X4	X4-X5	X1-X3	X1-X2	X2-X3	C400
H1, H2, H3	C, D, E F, G, H	3000:5A	2500:5A	2200:5A	2000:5A	1500:5A	1200:5A	1000:5A	800:5A	500:5A	300:5A	C800
H2	I	1100:2A										-
X2	J	8500:2A										-
H1, H2, H3	K, M, N	400:5A										0.380.9
H1, H2, H3	O, P, Q R, S, T	1200:5A	1000:5A	900:5A	800:5A	600:5A	500:5A	400:5A	300:5A	200:5A	100:5A	C800



VOLTAGE (kV)	CURRENT (A)			NO VOLTAGE TAP CHANGER	
	ONAN	ONAF	ONAF	IND.	CON.
152.250	531	713	887	1	1-2
148.625	544	730	909	2	2-3
145.000	557	749	932	3	3-4
141.375	572	768	956	4	4-5
137.750	587	788	981	5	5-6

WITHSTAND: COMPLETE TRANSFORMER ±15PSI PRESSURE



VECTOR GROUP: Ynd1  
 PURCHASER General Electric Company  
 DATE OF TEST Oct. 2002 YEAR OF MANUFACTURE Oct. 2002 SERIAL NO. 01009

**FORTUNE ELECTRIC CO., LTD.**  
 MADE IN TAIWAN

INSTRUCTION MANUAL: 24-9506 TR-NL22-5777

SYM.	DATE	REVISIONS	REV'D.	CHKD.	APPR.
△	10.7.02	BCT and ratio Change	M.H. Yang	S.M. Wang	S.M. Wang
△	8.09.02	Current ratio and Accuracy Change(K/M)	M.H. Yang	S.M. Wang	S.M. Wang
△	6.13.02	Add BCT(OP,QR,S,T) and plate size change CT NO(K/M) add slip over metering	M.H. Yang	S.M. Wang	S.M. Wang
△	6.07.02	Add BCT(K/M)-CUSTOMER SUPPLY	M.H. Yang	S.M. Wang	S.M. Wang
△	1.16.02	OUTLINE DRAWING TO ALTER	Y.C. Hsu	S.M. Wang	S.M. Wang
△	9.21.01	APPROXIMATE WEIGHTS CHANGED	Y.C. Hsu	S.M. Wang	S.M. Wang
△	7.23.01	HV BCT SPEC. CHANGED	Y.C. Hsu	S.M. Wang	S.M. Wang

MATERIAL: STAINLESS STEEL PLATE: 16t-300x500  
 006-1181496

UNIT	SCALE	PROJECTION
in/(mm)	1:1	

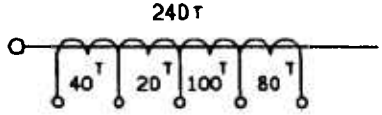
TITLE	PRELIMINARY	POLETTI
NAME PLATE		
140/188/234MVA TRANSFORMER		
PROJECT		
POLETTI 500 MW COMBINED CYCLE PLANT		
MADE FOR		
NEW YORK POWER AUTHORITY		
DWN. Y. C. Hsu	03-12-01	
CHKD. S. M. WANG	03-12-01	
APPD. I. C. CHENG	03-12-01	



GENERAL ELECTRIC INTERNATIONAL, INC.  
 POWER PLANT ENGINEERING  
 POWER PLANT SYSTEMS DEPARTMENT  
 DRAWING NO. 22-5777  
 SHEET CONT. ON SH. REV. △

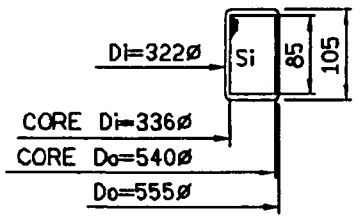
NYP& POLETTI 500MW CCPP STG GSU NAMEPLATE

H1, H2, H3

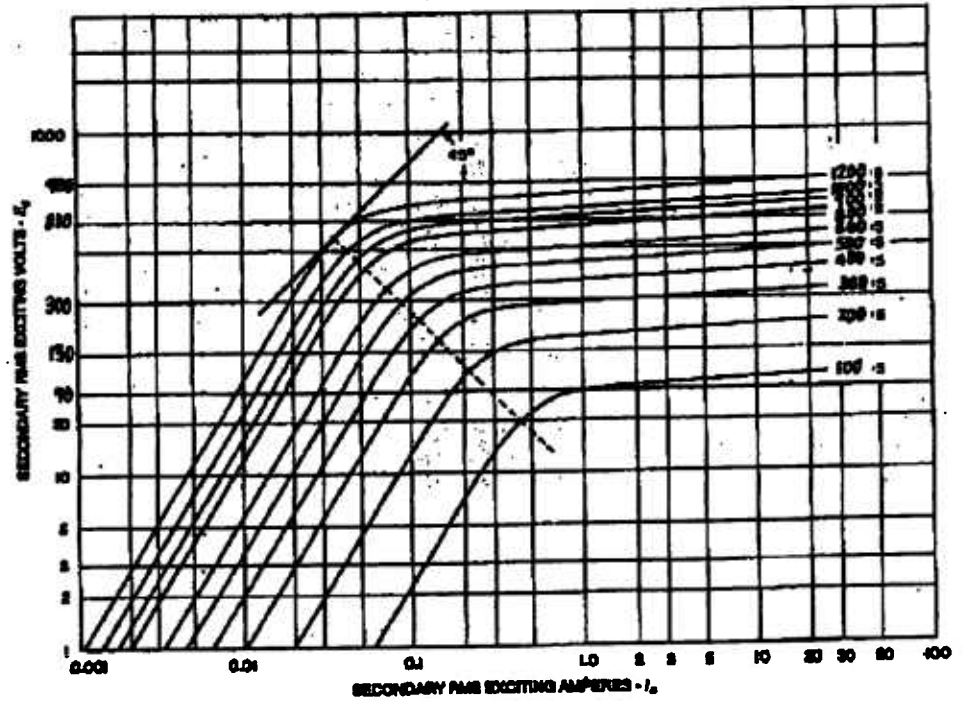


C1 C2 C3 C4 C5  
 2 2 2 2 2  
 N1 N2 N3 N4 N5

CT NO.	MULTI RATIO	SECONDARY CONNECTIONS	ACCURACY	CAPACITY (VA)
C D E F G H I J K L M N	1200/5A	X1-X5	C800	200
	1000/5A	X2-X5		
	900/5A	X3-X5		
	800/5A	X1-X4		
	600/5A	X2-X4		
	500/5A	X3-X4		
	400/5A	X4-X5		
	300/5A	X1-X3		
	200/5A	X1-X2		
	100/5A	X2-X3		



SECONDARY RESISTANCE ON MAX.TAP 5.0 Ω (AT 75°C)  
 CORE AREA 8670 mm<sup>2</sup>  
 CORE MEAN LENGTH 1380 mm

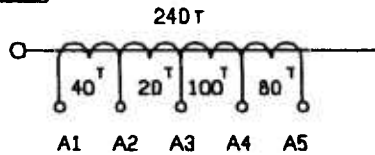


△					
△					
SYM.	DATE	REVISIONS	REV'D.	CHK'D.	APP'D.

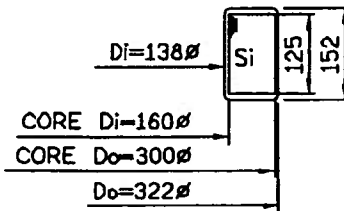
SCALE 1:1  
 UNIT in/(mm)  
 PROJECTION

PRELIMINARY	POLETTI
TITLE CURRENT TRANSFORMER DATA AND EXCITATION CURVE 140/188/234MVA TRANSFORMER	GENERAL ELECTRIC INTERNATIONAL, INC. POWER PLANT ENGINEERING
PROJECT POLETTI 500 MW COMBINED CYCLE PLANT	POWER PLANT SYSTEMS DEPARTMENT
MADE FOR NEW YORK POWER AUTHORITY	PROJECT NO. DRAWING NO. SHEET REV.
	23A33688 1/3
DWN. Y. C. HUI 03-12-'01 CHKD. S. M. WANG 03-12-'01 APPD. I. C. CHENG 03-12-'01	FORTUNE ELECTRIC CO., LTD.

H0



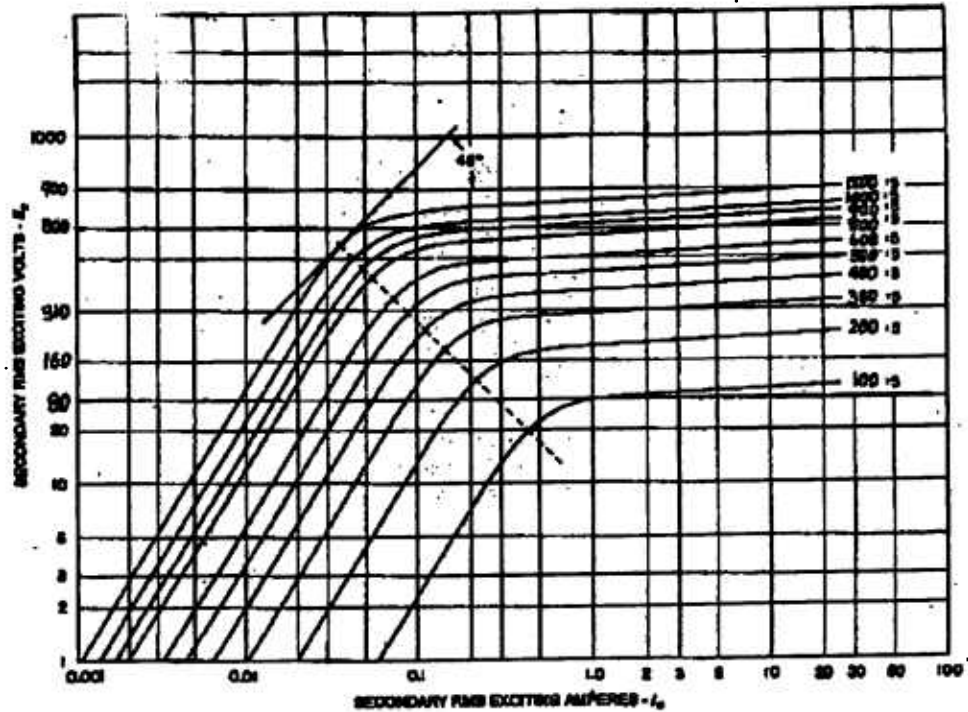
CT NO	MULTI RATIO	SECONDARY CONNECTIONS	ACCURACY	CAPACITY (VA)
A	1200/5A	X1-X5	C800	200
	1000/5A	X2-X5		
	900/5A	X3-X5		
	800/5A	X1-X4		
	600/5A	X2-X4		
	500/5A	X3-X4		
	400/5A	X4-X5		
	300/5A	X1-X3		
	200/5A	X1-X2		
100/5A	X2-X3			



SECONDARY RESISTANCE ON MAX.TAP 5.1 Ω (AT 75°C)

CORE AREA 8750 mm<sup>2</sup>

CORE MEAN LENGTH 730 mm

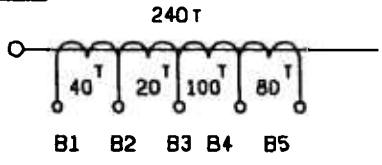


△						SCALE	UNIT
△						1:1	in/(mm)
SYM.	DATE	REVISIONS	REVD.	CHKD.	APPD.	PROJECTION	

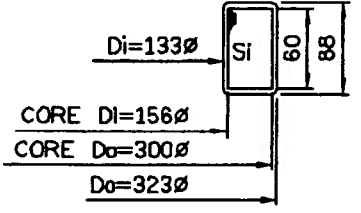
PRELIMINARY		POLETTI	
TITLE		GENERAL ELECTRIC INTERNATIONAL, INC.	
CURRENT TRANSFORMER DATA AND EXCITATION CURVE		POWER PLANT ENGINEERING	
140/188/234MVA TRANSFORMER		POWER PLANT SYSTEMS DEPARTMENT	
PROJECT		PROJECT NO.	
POLETTI 500 MW COMBINED CYCLE PLANT		DRAWING NO.	
MADE FOR		SHEET	
NEW YORK POWER AUTHORITY		23A3368B 2/3	
DATE		REV.	
DWN. Y. C. Hsu 03-12-'01			
CHKD. S. M. WANG 03-12-'01			
APPD. I. C. CHENG 03-12-'01			

FORTUNE ELECTRIC CO., LTD.

H0



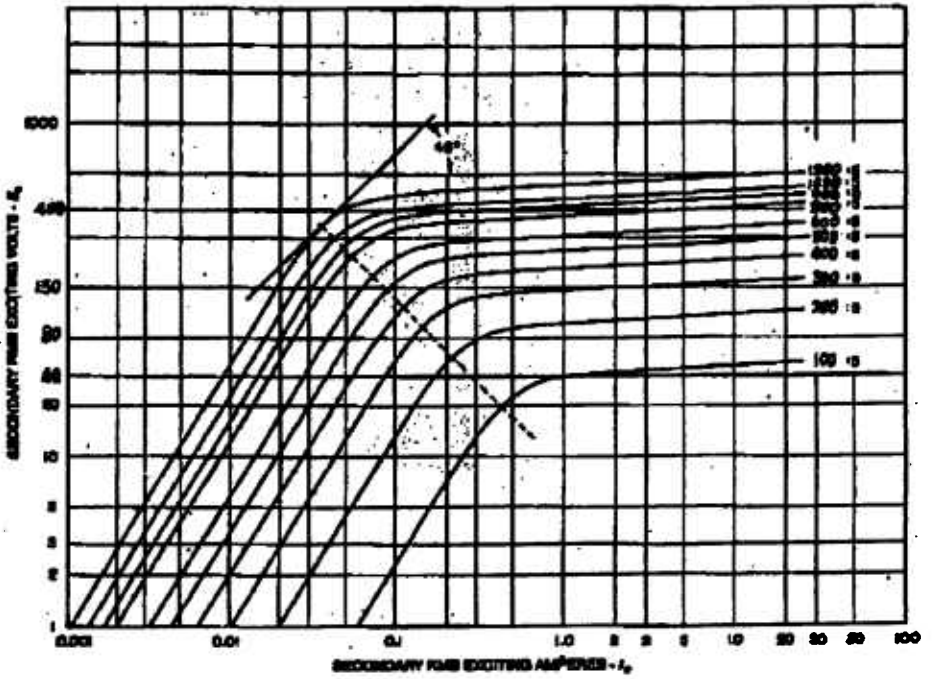
CT NO	MULTI RATIO	SECONDARY CONNECTIONS	ACCURACY	CAPACITY (VA)
B	1200/5A	X1-X5	C400	100
	1000/5A	X2-X5		
	900/5A	X3-X5		
	800/5A	X1-X4		
	600/5A	X2-X4		
	500/5A	X3-X4		
	400/5A	X4-X5		
	300/5A	X1-X3		
	200/5A	X1-X2		
	100/5A	X2-X3		



SECONDARY RESISTANCE ON MAX.TAP 2.8  $\Omega$  (AT 75°C)

CORE AREA 4320 mm<sup>2</sup>

CORE MEAN LENGTH 720 mm



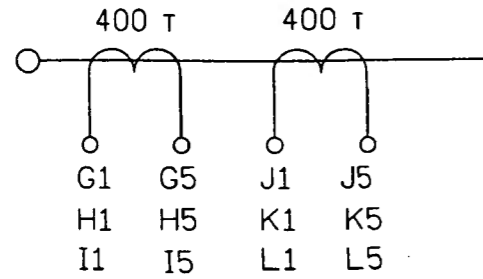
SYM	DATE	REVISIONS	REV'D.	CHK'D.	APP'D.	SCALE	UNIT
$\Delta$						1:1	in/[mm]
$\Delta$						PROJECTION	

PRELIMINARY		POLETTI	
TITLE		GENERAL ELECTRIC INTERNATIONAL, INC.	
CURRENT TRANSFORMER DATA AND EXCITATION CURVE		POWER PLANT ENGINEERING	
140/188/234MVA TRANSFORMER		POWER PLANT SYSTEMS DEPARTMENT	
PROJECT		POLETTI 500 MW COMBINED CYCLE PLANT	
MADE FOR	NEW YORK POWER AUTHORITY	PROJECT NO.	23A33688 3/3
DATE	03-12-01	DRAWING NO.	
CHK'D.	S. M. WANG	SHEET	
APP'D.	I. C. CHENG	REV.	

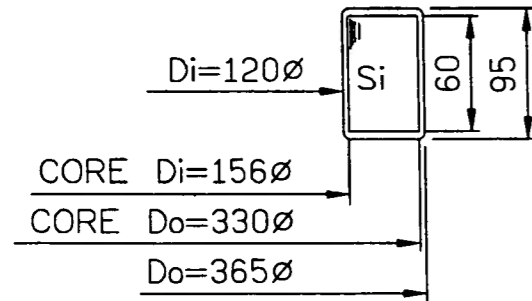
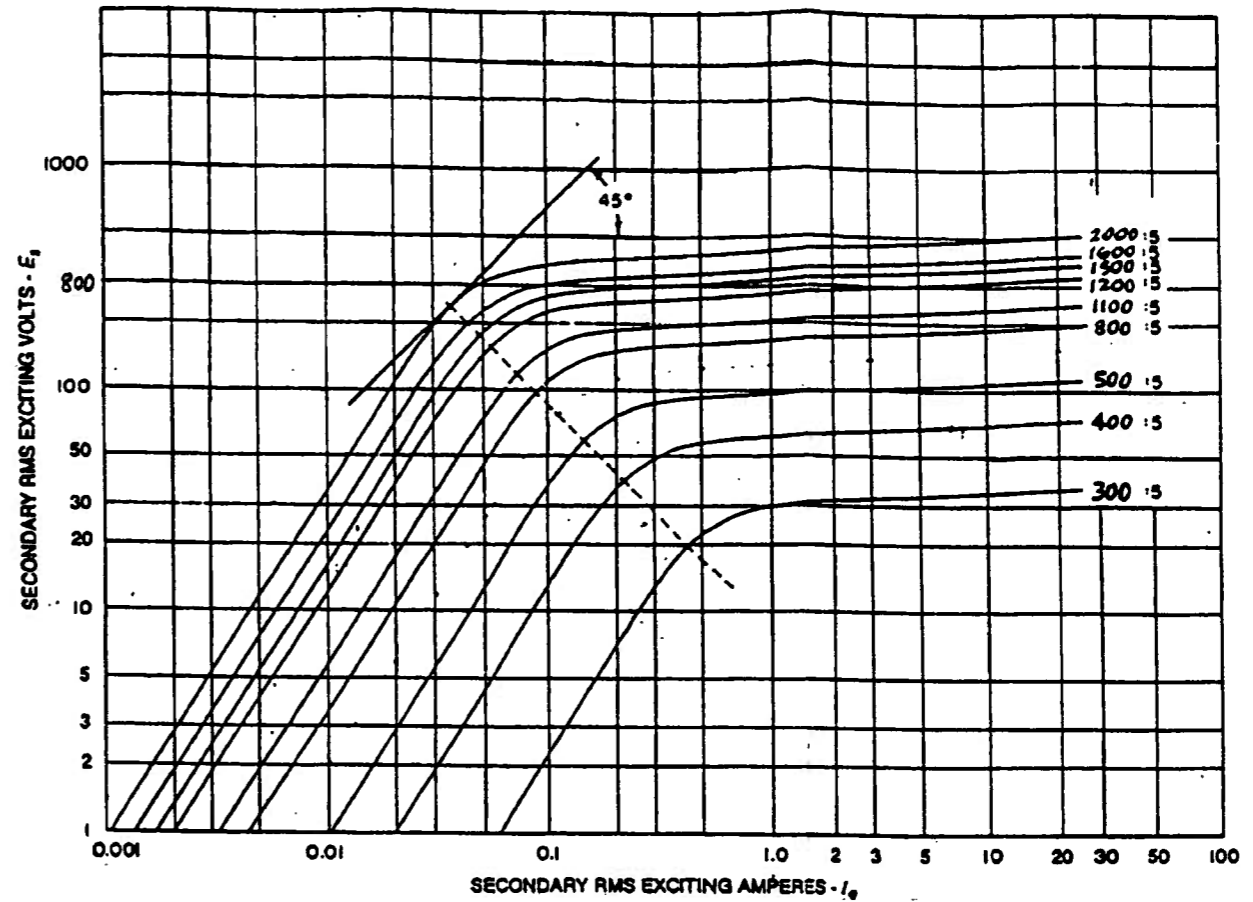
FORTUNE ELECTRIC CO., LTD.



H1, H2, H3



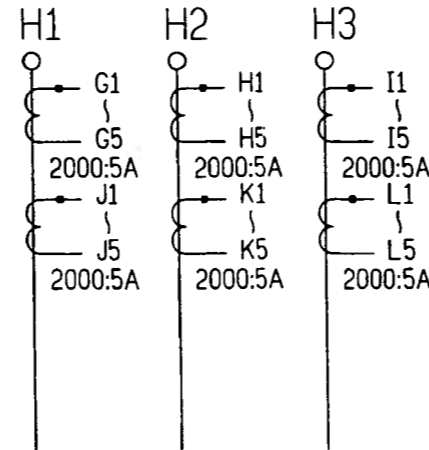
CT NO.	MULTI RATIO	SECONDARY CONNECTIONS	ACCURACY	CAPACITY (VA)
G H I J K L	2000:5A	X1-X5	C800	200
	1600:5A	X2-X5		
	1500:5A	X1-X4		
	1200:5A	X1-X3		
	1100:5A	X2-X4		
	800:5A	X2-X3		
	500:5A	X4-X5		
	400:5A	X1-X2		
	300:5A	X3-X4		



SECONDARY RESISTANCE ON MAX.TAP 1.1  $\Omega$  (AT 75°C)

CORE AREA 5220 mm<sup>2</sup>

CORE MEAN LENGTH 770 mm



PRELIMINARY		POLETTI	
TITLE		GENERAL ELECTRIC INTERNATIONAL, INC.	
BCT EXCITATION CURRENT CURVES		POWER PLANT ENGINEERING	
26/34.6/43.4MVA TRANSFORMER		POWER PLANT SYSTEMS DEPARTMENT	
PROJECT		POLETTI 500 MW COMBINED CYCLE PLANT	
MADE FOR	PPE IDENT. NO.	DRAWING NO.	SHEET
NEW YORK POWER AUTHORITY		23A3992 3/3	2
		CONT. ON SH.	15

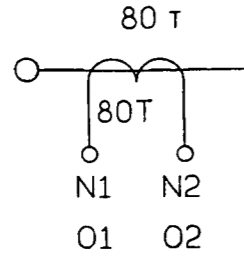
SCALE	1:1	UNIT	in/(mm)
PROJECTION			
SYM.	DATE	REVISIONS	REVD. CHKD. APPD.

DWN.	M. H. Yang	7-9-'02
CHKD.	S. M. Wang	7-9-'02
APPD.	S. M. Wang	7-9-'02

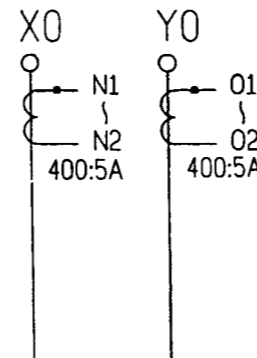
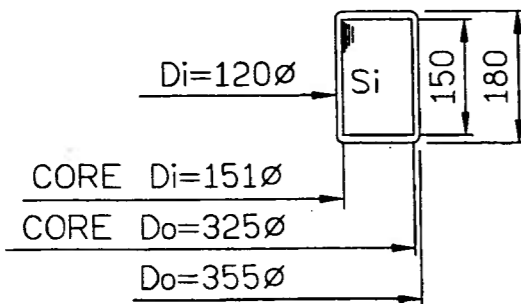
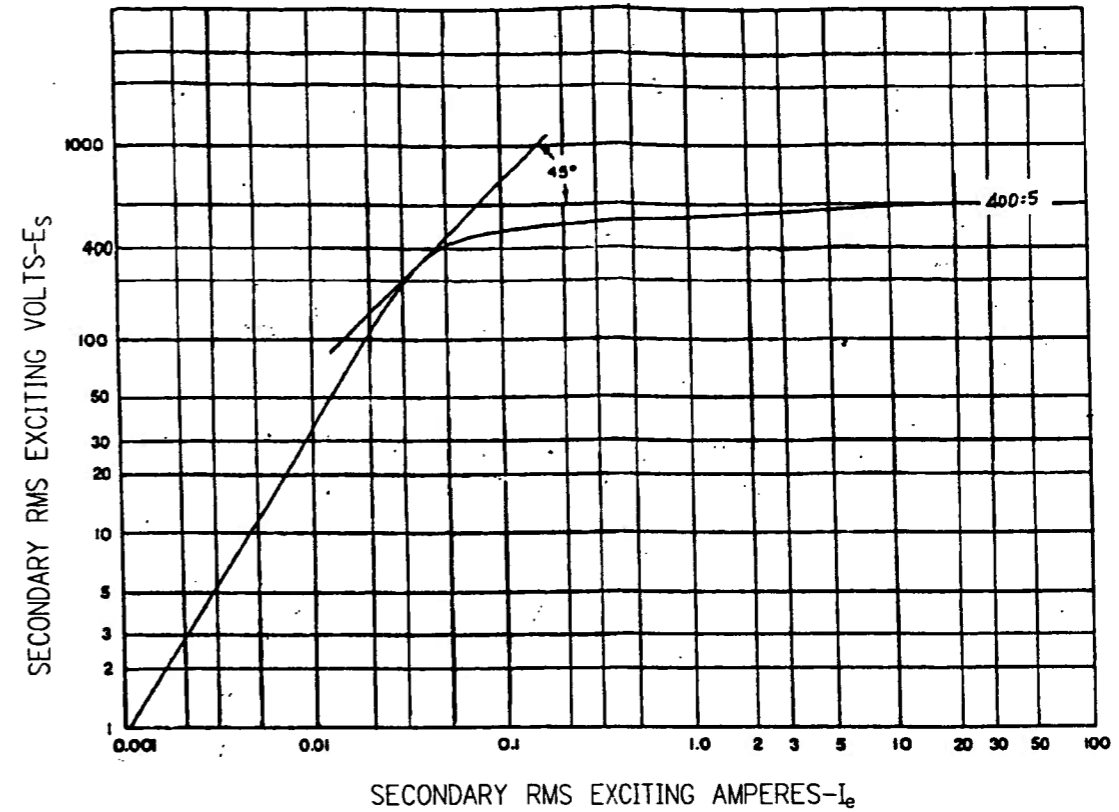


FORTUNE ELECTRIC CO., LTD.

X0, Y0



CT NO.	MULTI RATIO	SECONDARY CONNECTIONS	ACCURACY	CAPACITY (VA)
N O	400:5A	X1-X2	C400	100



SECONDARY RESISTANCE ON MAX.TAP 0.8  $\Omega$  (AT 75°C)

CORE AREA 13050 mm<sup>2</sup>

CORE MEAN LENGTH 800 mm

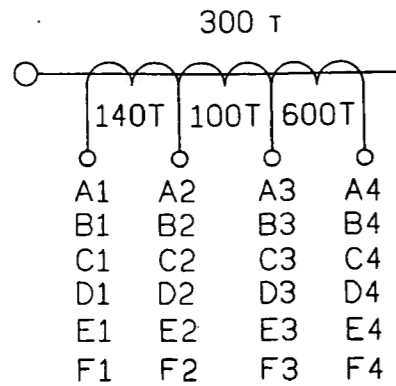
PRELIMINARY		POLETTI	
TITLE		GENERAL ELECTRIC INTERNATIONAL, INC.	
BCT EXCITATION CURRENT CURVES		POWER PLANT ENGINEERING	
26/34.6/43.4MVA TRANSFORMER		POWER PLANT SYSTEMS DEPARTMENT	
PROJECT		POLETTI 500 MW COMBINED CYCLE PLANT	
MADE FOR	PPE IDENT. NO.	DRAWING NO.	SHEET
NEW YORK POWER AUTHORITY		23A3992	2
		CONT. ON SH.	15
DWN. Y. C. Hsu	9-4-'01		
CHKD. S. M. Wang	9-4-'01		
APPD. S. M. Wang	9-4-'01		

SYM.	DATE	REVISIONS	REVD.	CHKD.	APPD.
△	07.09.'02	Page change	M.H.Yang	S.M.Wang	S.M.Wang
△	11.12.'01	PROVIDE LEGIBLE CORVE CHANGED	Y.C.Hsu	S.M.Wang	S.M.Wang

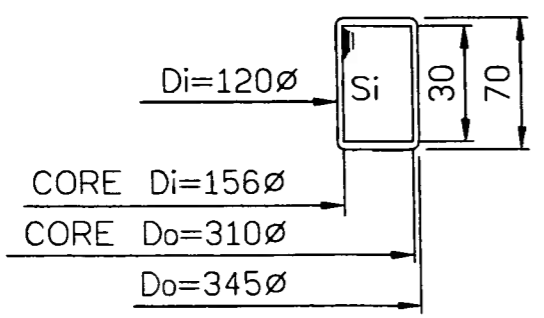
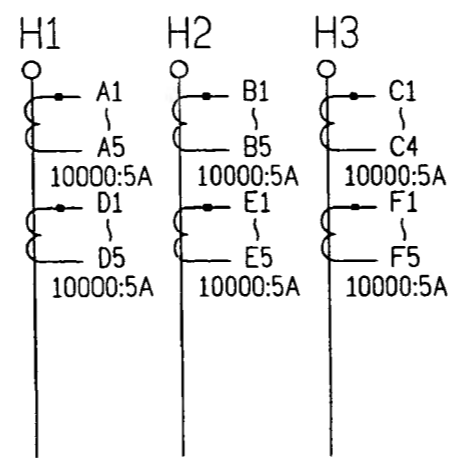
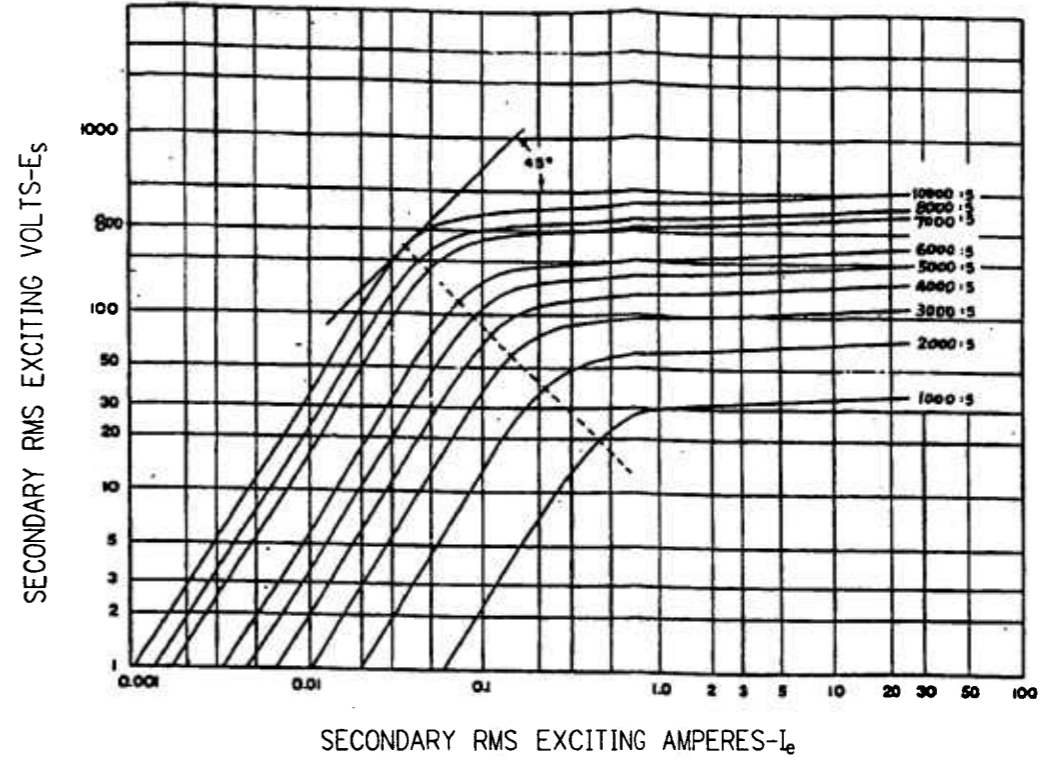
SCALE 1:1 UNIT in/(mm) PROJECTION

**FE** FORTUNE ELECTRIC CO., LTD.

H1, H2, H3



CT NO.	MULTI RATIO	SECONDARY CONNECTIONS	ACCURACY	CAPACITY (VA)
A B C D E F	10000:5A	X1-X5	C800	200
	8000:5A	X1-X4		
	7000:5A	X2-X5		
	6000:5A	X3-X5		
	5000:5A	X2-X4		
	4000:5A	X3-X4		
	3000:5A	X1-X2		
	2000:5A	X4-X5		
	1000:5A	X2-X3		



SECONDARY RESISTANCE ON MAX.TAP 1.6 Ω (AT 75°C)

CORE AREA 6930 mm<sup>2</sup>

CORE MEAN LENGTH 750 mm

SYM.	DATE	REVISIONS	REVD.	CHKD.	APPD.
△	07.09.'02	Page change	M.H.Yang	S.M.Wang	S.M.Wang
△	12.10.'01	MULTI RATIO CHANGED	Y.C.Hsu	S.M.Wang	S.M.Wang
△	11.12.'01	MULTI RATIO CHANGED	Y.C.Hsu	S.M.Wang	S.M.Wang

PRELIMINARY		POLETTI	
TITLE		GENERAL ELECTRIC INTERNATIONAL, INC.	
BCT EXCITATION CURRENT CURVES		POWER PLANT ENGINEERING	
26/34.6/43.4MVA TRANSFORMER		POWER PLANT SYSTEMS DEPARTMENT	
PROJECT		POLETTI 500 MW COMBINED CYCLE PLANT	
MADE FOR	PPE IDENT. NO.	DRAWING NO.	SHEET
NEW YORK POWER AUTHORITY		23A3992	1/3
		CONT. ON SH.	2
			15
			REV. C
SCALE 1:1		UNIT in/[mm]	
PROJECTION		DWN. Y. C. Hsu 9-4-'01	
		CHKD. S. M. Wang 9-4-'01	
		APPD. S. M. Wang 9-4-'01	

**FE** FORTUNE ELECTRIC CO., LTD.

NYPA POLETTI 500MW CCPP UAT CT SAT CURVES



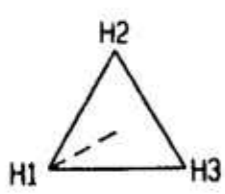
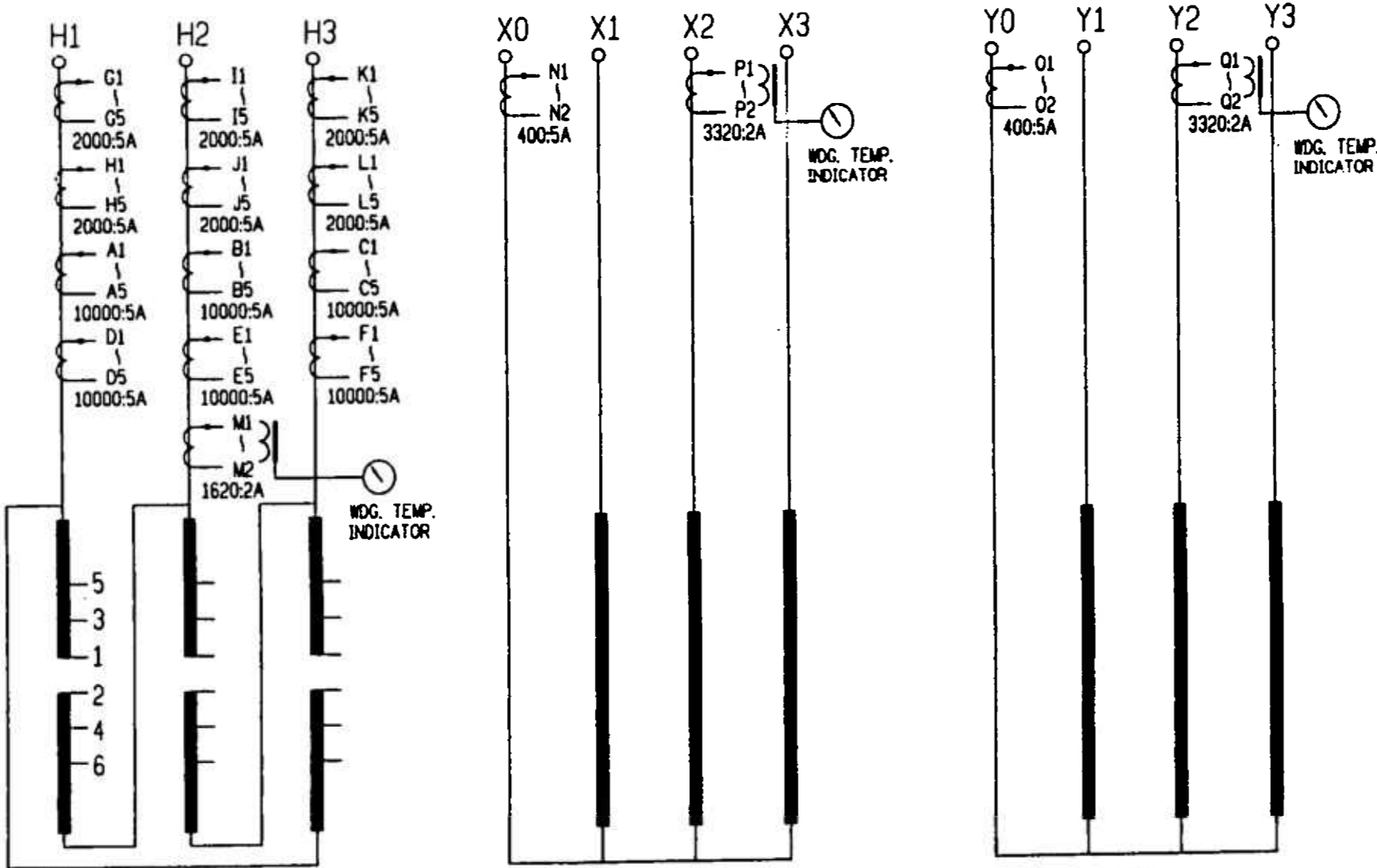
# TRANSFORMER

3 PHASE	60 HZ	CORE FORM	STANDARD IEEE C57.12
TYPE OF COOLING		ONAN/ONAF/ONAF	OUTDOOR USE

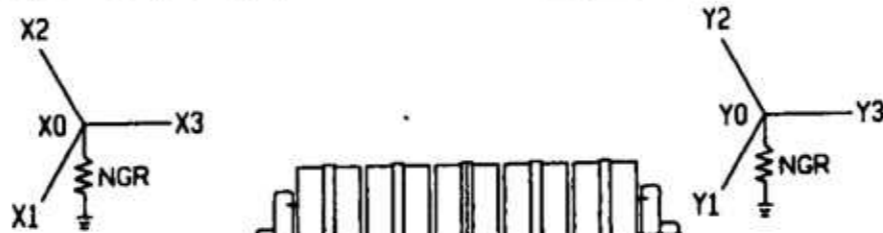
WINDING	CONN. TO	CAPACITY (MVA)			VOLTAGE RATING (kV)	CURRENT (A)			IMPULSE (BIL)
		ONAN	ONAF	ONAF		ONAN	ONAF	ONAF	
HV	H1, H2, H3	26	34.6	43.4	18	834	1110	1392	150 kV
LV1	X1, X2, X3	13	17.3	21.7	4.16	1804	2401	3012	75 kV
LV2	Y1, Y2, Y3	13	17.3	21.7		NEUTRAL			75 kV

LOAD CAPABILITY 40°C AMBIENT TEMP. WDG. TEMP. RISE BY RESISTANCE 65 °C OIL TEMP. RISE 65 °C	INSULATING OIL	MINERAL OIL	APPROXIMATE WEIGHTS CORE & WINDINGS 52,000 lbs TANK & FITTINGS 29,800 lbs OIL 3,500 GALLONS 26,200 lbs TOTAL WEIGHT 108,000 lbs
IMPEDANCE [ ] % AT 18-4.16kV-13MVA 85°C (HV-LV1) IMPEDANCE [ ] % AT 18-4.16kV-13MVA 85°C (HV-LV2)	WINDING MATERIAL	COPPER	
WITHSTAND: COMPLETE TRANSFORMER ±15Psi PRESSURE			

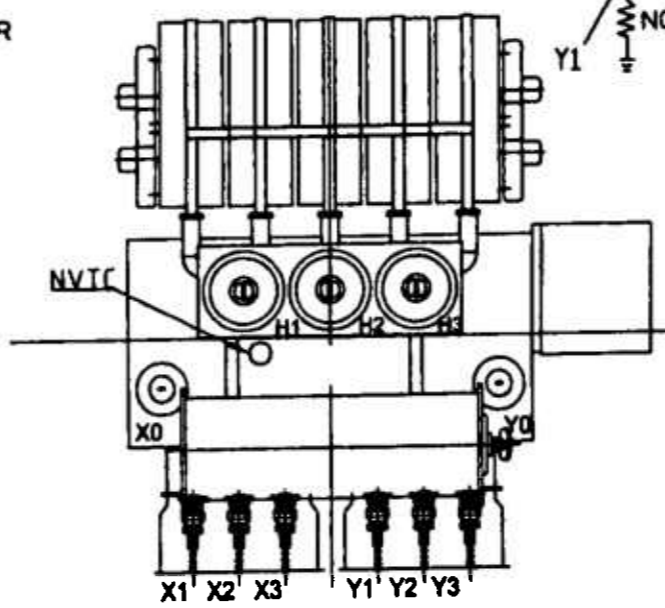
POSITION	CT NO	CURRENT MULTI RATIO									ACCURACY
		SECONDARY CONNECTIONS									
H1, H2, H3	A, B, C	10000:5A	8000:5A	7000:5A	6000:5A	5000:5A	4000:5A	3000:5A	2000:5A	1000:5A	C800
	D, E, F	X1-X5	X1-X4	X2-X5	X3-X5	X2-X4	X3-X4	X1-X2	X4-X5	X2-X3	
H2	M	1620:2A (FOR WTI) X1-X2									-
X0, Y0	N, O	400:5A X1-X2									C400
X2, Y2	P, Q	3320:2A (FOR WTI) X1-X2									-
H1, H2, H3	G, I, K	2000:5A	1600:5A	1500:5A	1200:5A	1100:5A	800:5A	500:5A	400:5A	300:5A	C800
	H, J, L	X1-X5	X2-X5	X1-X4	X1-X3	X2-X4	X2-X3	X4-X5	X1-X2	X3-X4	



VECTOR GROUP: Dyn11yn11



VOLTAGE (kV)	CURRENT (A)			NO VOLTAGE TAP CHANGER	
	ONAN	ONAF	ONAF	IND.	CON.
18.90	794	1057	1326	1	1-2
18.45	814	1083	1358	2	2-3
18.00	834	1110	1392	3	3-4
17.55	855	1138	1426	4	4-5
17.10	878	1168	1465	5	5-6



YEAR OF MANUFACTURE Sep. 2002

SERIAL NO. 01072

INSTRUCTION MANUAL: 24A0231

## FORTUNE ELECTRIC CO., LTD.

MADE IN TAIWAN

TR-NL22-5483

MATERIAL: STAINLESS STEEL PLATE: 1.6t-300x500  
0.06"-11.81"x19.68"

PRELIMINARY	POLETTI	GENERAL ELECTRIC INTERNATIONAL, INC.
TITLE	NAME PLATE	POWER PLANT ENGINEERING
PROJECT	26/34.6/43.4MVA TRANSFORMER	POWER PLANT SYSTEMS DEPARTMENT
POLETTI 500 MW COMBINED CYCLE PLANT	MADE FOR	NEW YORK POWER AUTHORITY
SCALE	UNIT	PROJECTION
1:1	in/[mm]	
DWN. Y. C. Hsu	03-12-'01	
CHKD. S. M. WANG	03-12-'01	
APPD. I. C. CHENG	03-12-'01	
DRAWING NO.	SHEET	REV.
22-5483	1	D
CONT. ON SH.	02	

SYM.	DATE	REVISIONS	CHKD.	APPD.
Δ	10.07.02	BCT and Type of cooling Change	M.H. Yang	S.M. Wang
Δ	07.03.02	Add BCT (G,H,J,K,L) and outline drawing of fan	M.H. Yang	S.M. Wang
Δ	12.10.01	SECONDARY CON. H1, H2, H3 changed	Y.C. Hsu	S.M. Wang
Δ	11.12.01	POSITION H1, H2, H3 changed	Y.C. Hsu	S.M. Wang

FORTUNE ELECTRIC CO., LTD.



686008HC-ISdH

# HVB SF6 GAS CIRCUIT BREAKER

TYPE OFPTD-20XH-100 FORM HAG

△ RATED MAX. VOLTAGE 27.5 KV RATED VOLTAGE RANGE FACTOR 1

BASIC IMPULSE LEVEL 125 KV FREQUENCY 60 Hz

RATED CONTINUOUS CURRENT 8000 A RATED SHORT CIRCUIT CURRENT 100 kA △

RATED INTERRUPTING TIME 70 ms △

RATED HYDRAULIC OIL PRESSURE 4550 psig TRIP LOCKOUT HYDRAULIC OIL PRESSURE 3700 psig

NORMAL GAS PRES. AT 68° F 71 psig CLOSING & TRIP LOCKOUT GAS PRES. AT 68° F 57 psig

CLOSING CONTROL VOLTAGE RANGE 90 TO 140 VDC CLOSING CONTROL CURRENT 2.1 A

TRIP CONTROL VOLTAGE RANGE 70 TO 140 VDC TRIP CONTROL CURRENT 4.5 A

TOTAL WEIGHT OF SF6 GAS 72 lbs TOTAL WEIGHT OF BREAKER WITH SF6 GAS 33000 lbs

INSTRUCTION BOOK NO. HIB-0018 WIRING DIAGRAM NO. 3HB00751

BREAKER SERIAL NO. 480021 YEAR OF MANUFACTURE 2002

BREAKER REQUISITION NO. GE PO. NO. 180168687-000

△ SPECIFICATION NO. GE SPEC. NO. 510X0009S-F336 REV 2 △

## HITACHI

HITACHI POWER SYSTEMS INDONESIA  
 EJIP Industrial Park, Plot 8E  
 Lemahabang, Bekasi 17550, Indonesia  
 Tel.:(62-21) 8970350

HPSI-3HB00989

## NOTE

- MATERIAL : SUS 304-CP
- THICKNESS : 0.6 mm

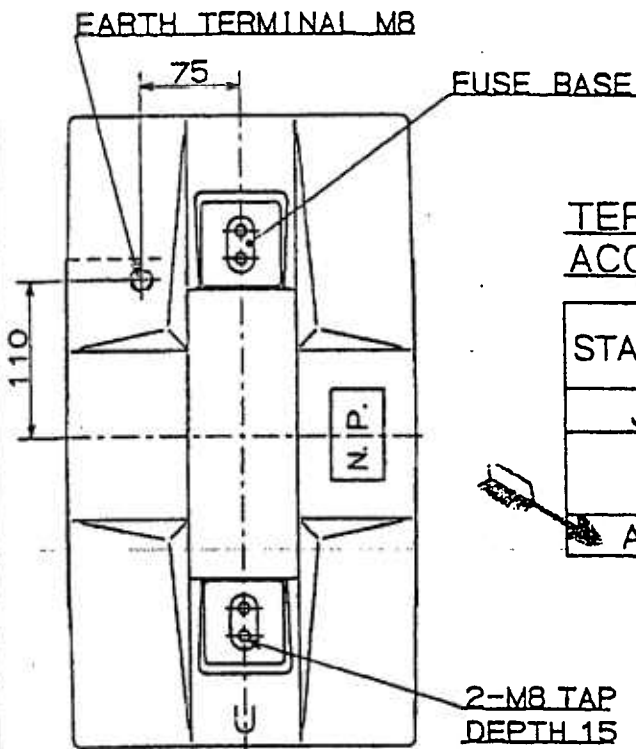
144  
160

REV NO.	SYMBOL	DESC ZONE	REVISION	DATE	REV.	CHG.	APPR.
1	△		CORRECTION REVISION SPEC. NO.	03.04.31	EDY	RMW	GOTO
2	△		CORRECTION OF RACK FORM TYPE	03.02.13	EDY	RMW	GOTO
3	△		REVISION SPECIFICATION NO. AND	03.07.13	EDY	RMW	GOTO
4	△		REVISION AS COMMENTS & FOR CORRECTION	02.11.20	EDY	RMW	GOTO
5	△		REVISION TO VALUE TO FROM AS SPEC COMMENTS	02.08.03	EDY	RMW	GOTO
6	△		REVISION AS COMMENTS	02.08.18	EDY	RMW	GOTO

PROJECT NAME :		POLETTI 500MW CONDENSER CYCLE PLANT STEAM TURBINE GENERATOR STG	
CUSTOMER NAME :		NEW YORK POWER AUTHORITY	
PURCHASE ORDER NO. :		GENERAL ELECTRIC CORP 14 POWER SYSTEMS 180368687-000	
SPECIFICATION NO. :		510X0009S-F336 REV 2	
CHG.	EDY	01.12.31	REQD.
CHG.	RMW	01.12.31	
CHG.	RMW	01.12.31	
APPR.	GOTO	01.12.31	
HITACHI POWER SYSTEMS INDONESIA			DRG. NO. HPSI-3HB00989

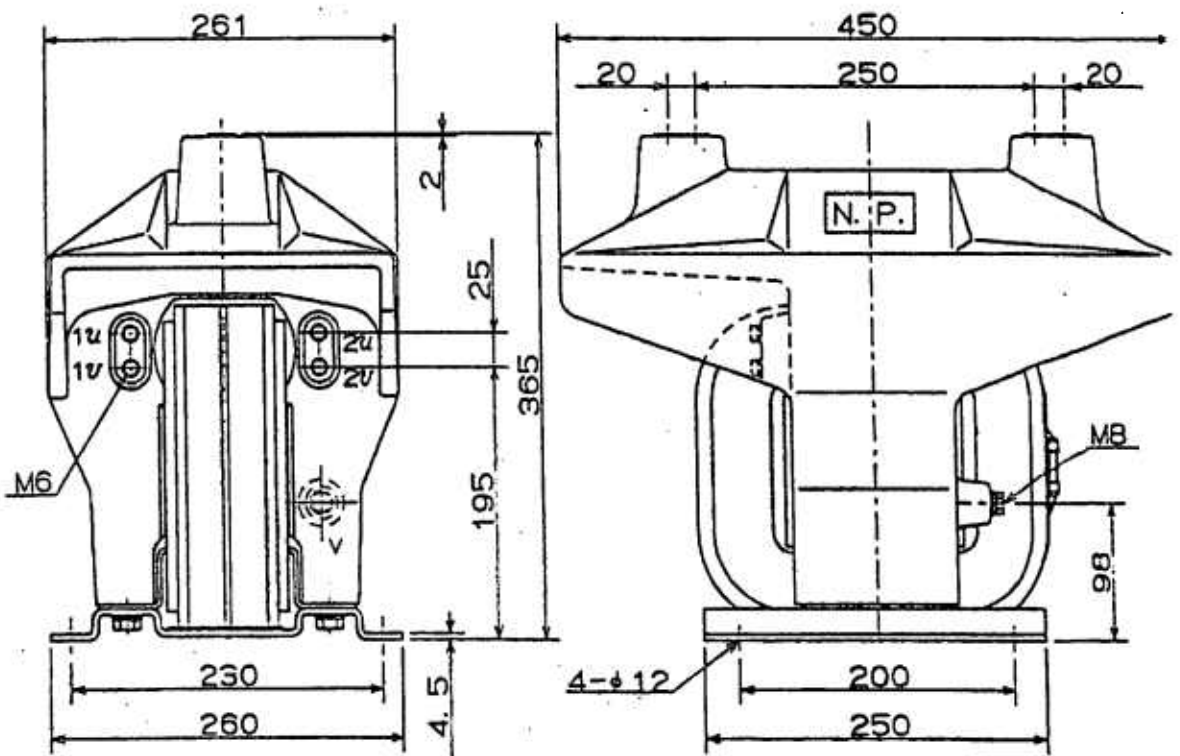
### NYPA POLETTI 500MW CAPP CTG 7A & 7B CB NAMEPLATE

INDOOR MOLDING TYPE  
 TYPE GE-6  
 PHASE 1  
 MASS 55kg



TERMINAL MARK  
 ACCORDING TO STANDARD

STANDARD	TERMINAL MARK	
	PRIM.	SEC.
JEC	U. V	1u.1v 2u.2v
IEC BS	A. N	1a.1n 2a.2n
ANSI	H1. H2	X1. X2 Y1. Y2



APP	5-Feb-'99	M. Furuya	MAR	REVISION
CHD	5-Feb-'99	M. Inoue	TOKO	D414950-01-000
DSN	4-Feb-'99	J. Matsunaga	ELECTRIC	OUTLINE DRAWING FOR

NYPA POLETTI 500MW CCPP CTG/STG PT1 & PT3 NAMEPLATE INFORMATION

INDOOR MOLDING TYPE  
 TYPE GE-6  
 STANDARD ANSI C 57.13

POS. NO.	FREQ.	B.I.L. (kv)	PRIM. VOLTAGE (kv)	RATIO	ACCURACY CLASS
2	60	125	18 / $\sqrt{3}$	150:1	0.3Z
3	60	125	18 / $\sqrt{3}$	150&150:1	0.3Y *

\* CLASS 0.3Y (75VA) ~~and 100VA~~  
 © GUARANTEE BURDEN 100VA PF.0.85

APP	30 Nov '98	M. F. ...	Ⓢ	Changed "Ⓢ"	1 - Mar '99 J. Matsunaga
CHD	27 Nov '98	M. ...	MAR	REVISION	
DSN	17 Nov '98	J. Matsunaga	TOKO	KI-1527-2a	
			ELECTRIC	SPECIFICATION	
				DATE 2002	



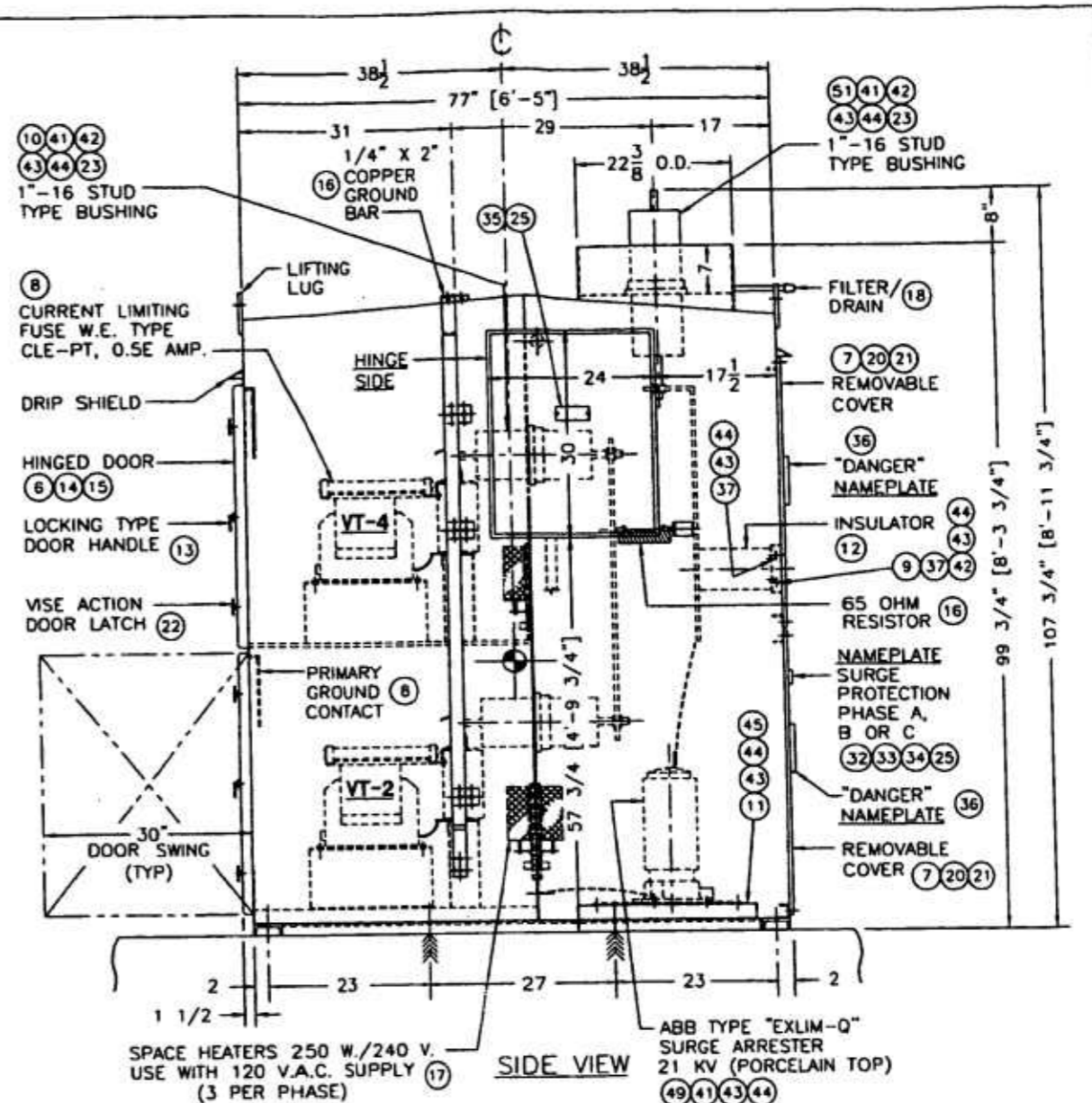
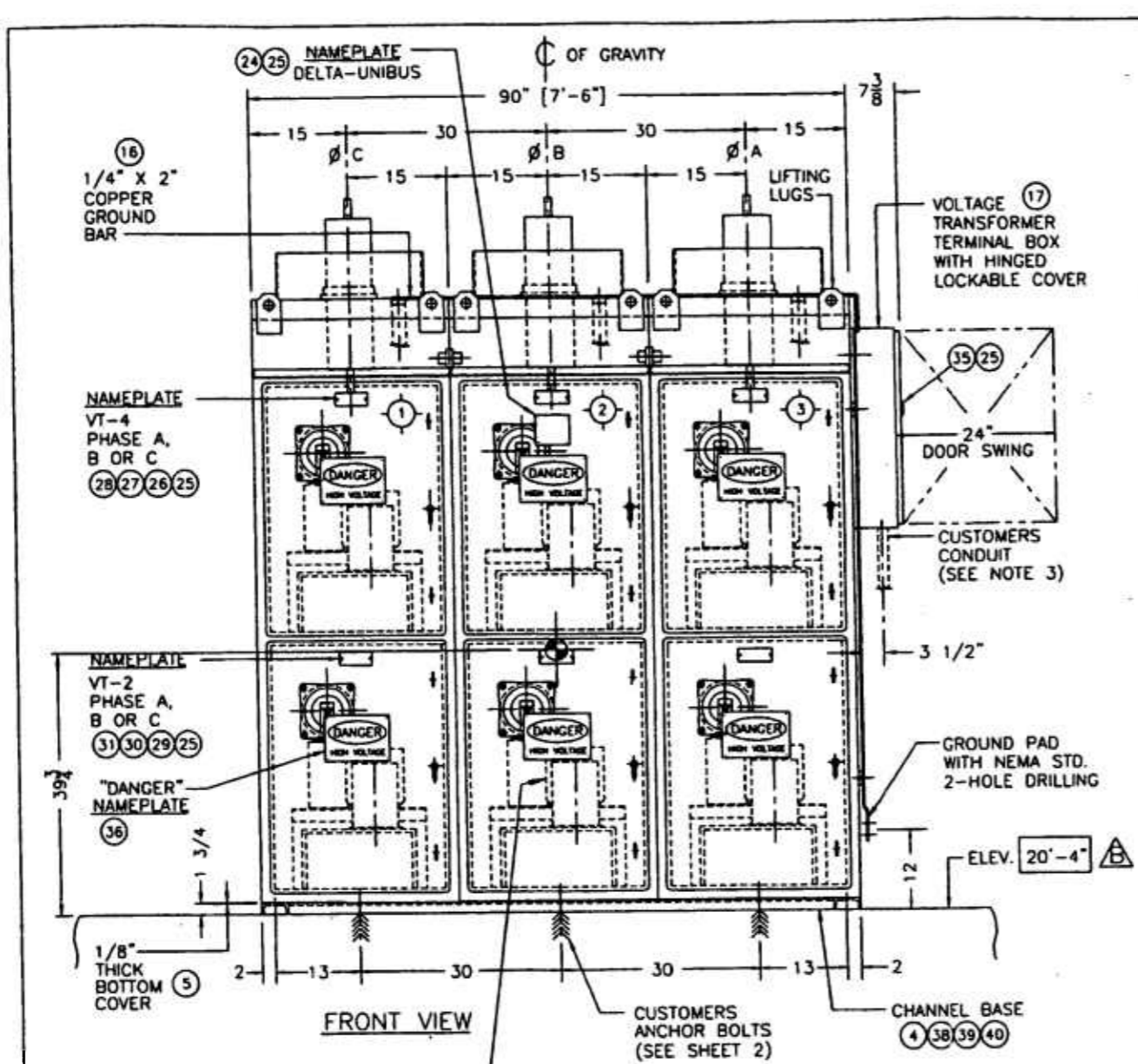
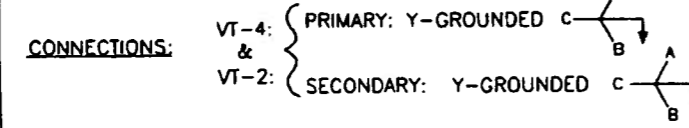


ABB TYPE "VIZ-12G" VOLTAGE TRANSFORMERS  
 18,000/120 V., 60 HZ., SINGLE PHASE, (19)  
 RATIO 150:1, 125 KV BIL  
**ACCURACY CLASS:**  
 LINE TO LINE 0.3 W, X, M, Y & Z  
 LINE TO NEUTRAL 0.3 W, X, M, Y & 1.2 Z  
**THERMAL RATINGS:**  
 LINE TO LINE 1500 VA. @ 55° C  
 LINE TO NEUTRAL 1000 VA. @ 55° C



- NOTES:**
- FOR WIRING DIAGRAM SEE DWG. T-171147X150
  - FOR LIST OF MATERIALS SEE DWG. T-140014X234-M
  - CUSTOMERS CONDUIT MAY ENTER THE V.T. TERMINAL BOX AT ANY POINT ON THE TOP, BOTTOM OR SIDES. TO BE DETERMINED BY CUSTOMER.
  - CUBICLE IS CONSTRUCTED OF 11GA. STEEL.
  - VOLTAGE TRANSFORMERS ARE GROUNDED BY AN INTERNAL GRID.
  - WHEN V.T.'S ARE IN THE DISCONNECT POSITION THE PRIMARY OF THE V.T. IS GROUNDED.
  - ⊙ = CENTER OF GRAVITY

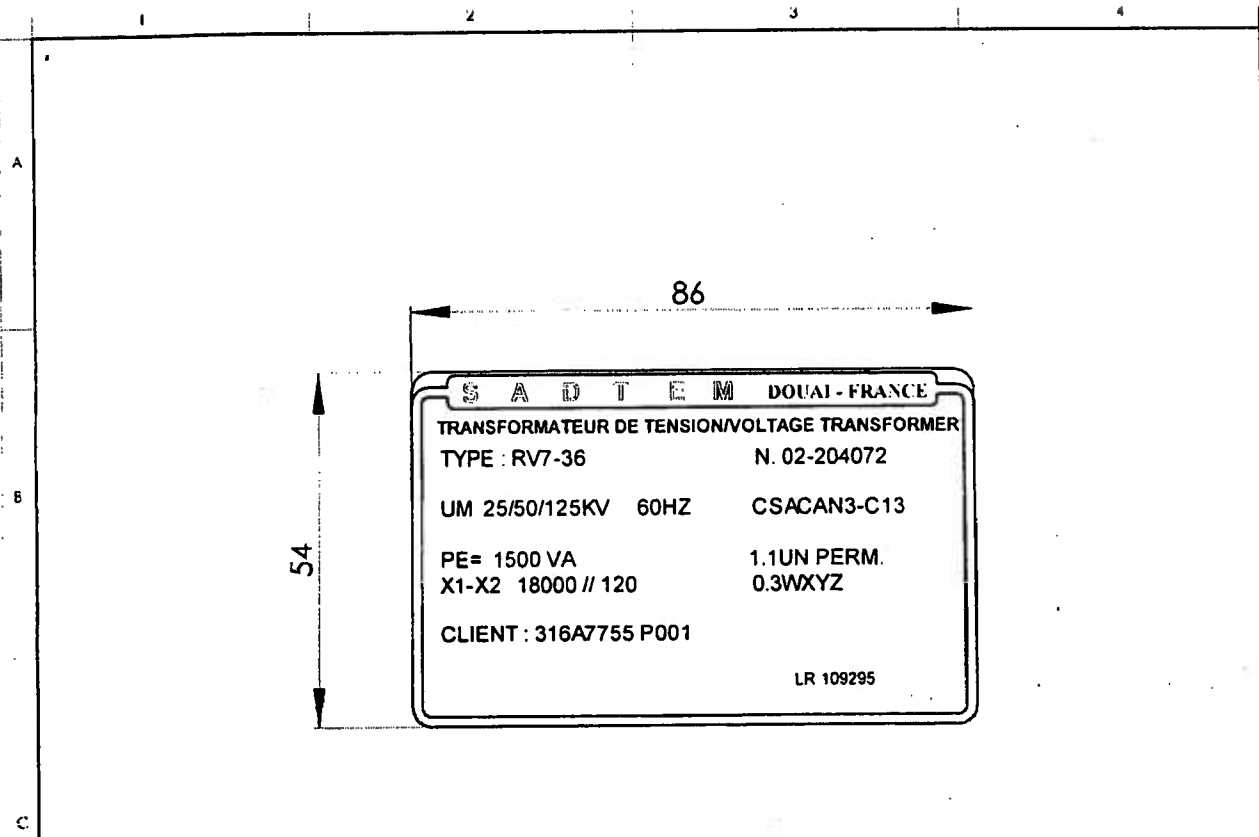
REV.	DATE	DESCRIPTION	DWN.	APPV'D.	RC'D.	NEXT ASSY.	USED ON
B	10-22-02	REVISED PER CUSTOMER APPROVAL RECEIVED ON 10-17-02	RD	R2			
A	8-30-02	REVISED PHASE PHASING, REMOVE CAPACITOR & RATING OF L.A. WAS 18 KV.	OYVD	R2			

REVISION RECORD

MATERIAL: SEE NOTE 2		P.M.F. J.O. #D-4589		DELTA-UNIBUS CORP. CHICAGO, ILLINOIS 60131	
FINISH: LIGHT GRAY ENAMEL PER ANSI # 61		THIS DRAWING IS THE PROPERTY OF THE DELTA UNIBUS CORPORATION, AND MAY NOT BE REPRODUCED IN ANY MANNER OR USED FOR ANY PURPOSE EXCEPT AS SPECIFICALLY AUTHORIZED BY THE DELTA UNIBUS CORPORATION.		VOLTAGE TRANSFORMER & SURGE PROTECTION CUBICLE ASSEMBLY DRAWING	
DATE: 6-05-02		DWN. BY: OYVD		SIZE: C	DWG. NO: T-140014X234
WEIGHT: 6000#		CHK: R2		REV: B	
SCALE: 3/4" = 12"		APPV: R.L.		AutoCAD# P0142341.DWG SHEET 1 OF 2	

NYPA POLETTI 500MW CAPP STG PT2 & PT4 NAMEPLATE INFORMATION





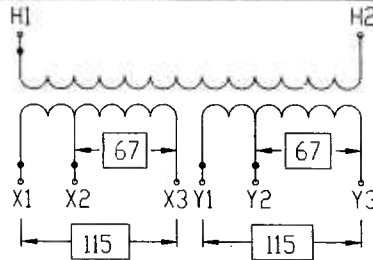
A		Création							
Date: 8 July. 05		Echelle: Scale: 1		Appareil: RV7-36		Format: A4			
Dessiné: DRN: B. LAPEYRE				Matière: POLYESTER		Finition:			
Vérifié par: CHK'D:				<div style="text-align: center; border: 1px solid black; padding: 5px;"> <p><b>SADTEM</b></p> <p>RV7-26 18000 - 120</p> </div>		<p><b>NAMEPLATE</b></p>			
		A						Destination: BE-U5	
<i>Propriété exclusive de SADTEM. Remis à titre confidentiel. aucune partie ne peut être reproduite, utilisée ou communiquée sans son autorisation écrite.</i> <i>The present document is the exclusive property of SADTEM, confidentially handed, it can't be communicated to third party, neither used or reproduced without his written agreement.</i>								Feuille: 1/1	

6.00

# ABCD

138 KV OIL FILLED OUTDOOR VOLTAGE TRANSFORMER

BIL  KV Hz   
 PRIMARY  KV  
 SECONDARY  V  
 TERTIARY  V  
 RATIO   
 ACCURACY   
 GAL. OIL  UNIT WT  LBS  
 SERIAL NO.  F.O.#   
 MFG. DATE:  CATALOG#   
 CUST. P.O.#



TYPE: ANSI GROUP 3

SECONDARY THERMAL CONNECTION LIMIT  
 X1-X3 + Y1-Y3  VA  
 X2-X3 + Y2-Y3  VA  
 X1-X3 OR Y1-Y3  VA  
 X2-X3 OR Y2-Y3  VA

300 WEST ANTELOPE ROAD, MEDFORD OREGON 97503-1089 USA

4.50

CUST: PACS Industries Inc  
 PO # D105-467-4110  
 QTY: 9 each

NYP A POLETTI 500MW CCPP 138KV PTS NAMEPLATE

MATERIAL (.025) STAINLESS STEEL

REVISION 0

## UXTR-138 Nameplate

DTR M. SWARTS  
 APD DATE  
 DWG 52-641-40  
 REVISION DWG SIZE SCALE TOLERANCE TITLE SHEET  
 0 A FULL +- 0 BLANK VOLTAGE TRANSFORMER NAMEPLATE 1 OF 1

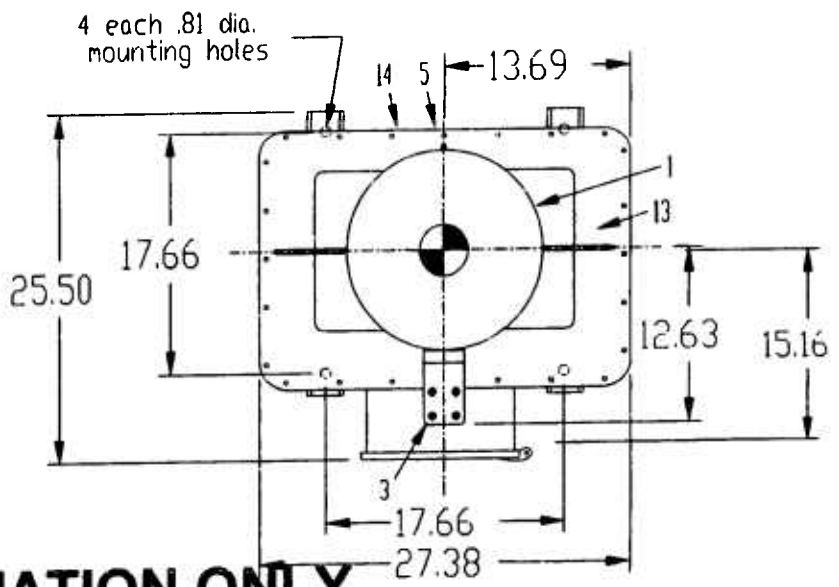
# ALSTOM

300 WEST ANTELOPE ROAD  
MEDFORD, OREGON USA 97503-1089

**ADCU**

VOLTAGE TRANSFORMER  
138kV CLASS 650kV BIL

- 1 . ALUMINUM WEATHER DOME WITH OIL LEVEL INDICATOR
- 2 . SECONDARY TERMINALS FOR CONNECTION WITH Cu or Al
- 3 . ONE PIECE CAST ALUMINUM HEAD CEMENTED TO PORCELAIN WITH REMOVABLE PRIMARY FOUR HOLE SPADE TERMINAL (.56 DIA. HOLES ON 1.75 SQUARE)
- 4 . NEMA GROUND PAD
- 5 . 0.38" OIL SAMPLE VALVE
- 6 . JUNCTION BOX WITH (2) 1.50" CONDUIT HUBS
- 7 . WET PROCESSED PORCELAIN (ASA#70 LT. GREY)
- 8 . CAST ALUMINUM TANK
- 9 . LIFTING PROVISIONS
- 10 . H2 BUSHING WITH GROUND BAR
- 11 . STAINLESS STEEL NAMEPLATE
- 12 . LV IDENTIFICATION PLATE
- 13 . CAST ALUMINUM TANK COVER CEMENTED TO PORCELAIN
- 14 . NON-PCB LABEL

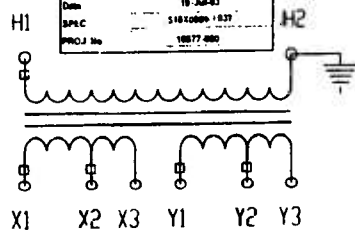


**FOR INFORMATION ONLY**

NOTE: ALL STAINLESS STEEL HARDWARE

CHARACTERISTICS

ACCURACY : 0.30% W,X,Y,Z,ZZ

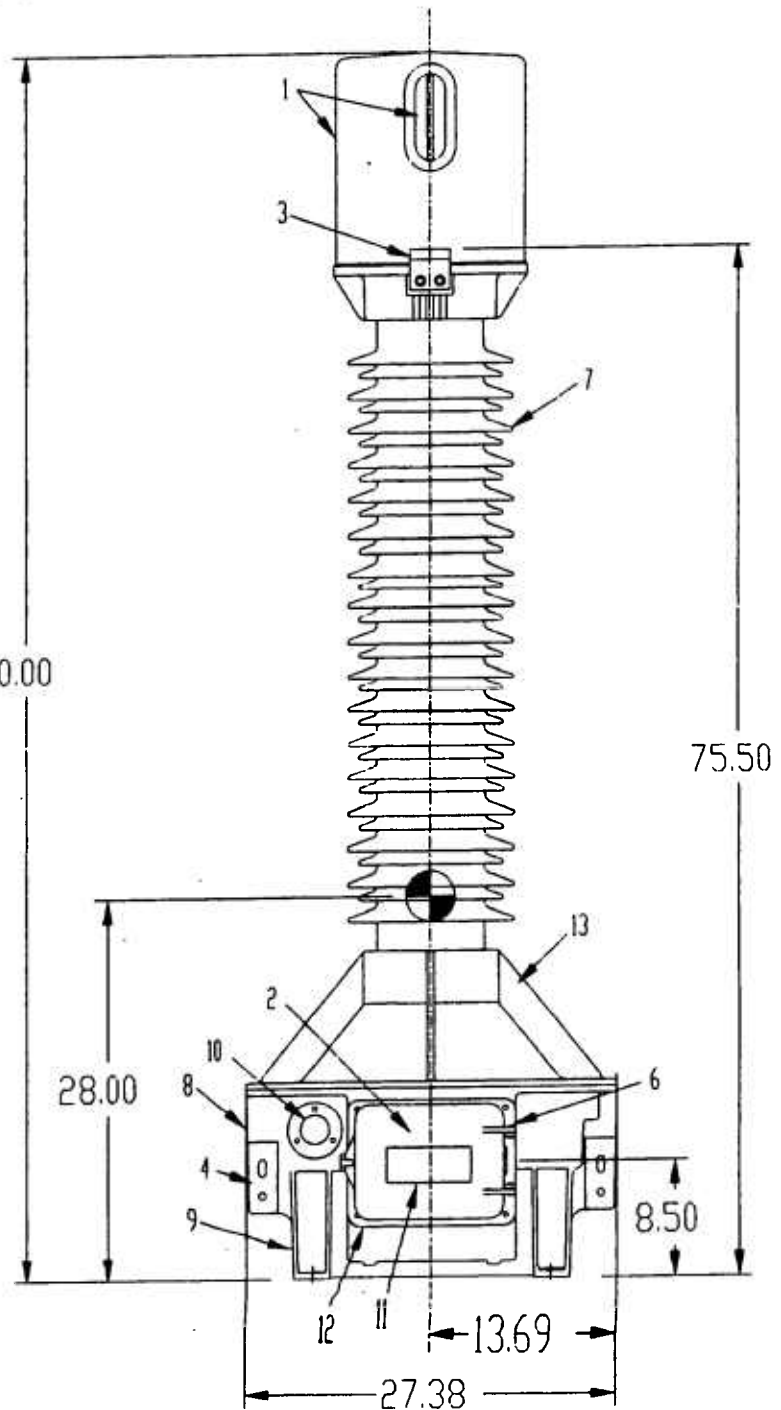


CONNECTION DIAGRAM:

DUAL TAPPED SECONDARY

- Catalog Number.....UXTR-138
- Ratio (pri/sec).....700/1200 & 700/1200 :1
- Primary Volts (L-G)...80500
- Sec/Tert Volts.....115/67
- Creep.....150"
- Oil.....23gal
- Weight.....975 lbs.
- Color.....ASA #70
- Strike.....48"
- Untanking Height.....145"
- Thermal VA.....7500 TOTAL
  - simultaneous max per winding...3750
  - max per tapped winding.....2700
  - max, one winding.....5400
  - max, one tapped winding.....3900

Cust: PACS UIndustries  
PO # D105-467-4110



ALSTOM USA INC.  
300 WEST ANTELOPE ROAD MEDFORD, OREGON U.S.A.

PART # UXTR-138	SD # H 8283	SHEET 1 OF 1
DATE 1 JUNE 1998	DRAWN BY M Dickinson	CHECKED BY SCALE: N.T.S. TOLERANCE: +/- .25"

Poletti 500MW Combined Cycle Power Project  
Fault Current Results Summary

The table below summarizes the fault current levels at the connection point of the Poletti CCPP units into the Con Edison system at the Astoria West 138kV bus. The short circuit analysis was performed both with and without the Poletti CCPP in service for select Con Edison 138kV busses. The results show an increase, on average, of about 40% in fault current levels at the Astoria West 138kV bus, and approximately 2-3% in the Con Edison 138kV system two busses away at East 179<sup>th</sup> Street and Vernon East 138kV.

Faulted Station Bus	Total Bus Fault Current Levels <sup>1</sup>					
	***** (Symmetrical RMS kA) *****					
	W/O Poletti 500MW CCPP			W/Poletti 500MW CCPP		
	3LG	2LG	1LG	3LG	2LG	1LG
Astoria West 138kV	24.9	26.9	27.4	34.2	37.5	38.8
East 179 <sup>th</sup> Street 138kV	39.8	41.7	38.2	40.5	42.4	38.8
Vernon East 138kV	33.7	35.3	36.0	34.7	36.3	37.0

<sup>1</sup> Fault Study was performed on the latest issue of the NYISO Short Circuit Database using Aspen OneLiner V9.7 Short Circuit program.

New York Power Authority --- 2005 System Fault Study With Poletti 500MW CCPP O/S

Summary of fault being displayed:

1. 3LG Bus fault on:

AST-WEST 138. kV

	+ SEQ		- SEQ		0 SEQ		A PHASE		B PHASE		C PHASE	
	24949.8@	-88.9	0.0@	0.0	0.0@	0.0	24949.8@	-88.9	24949.8@	151.1	24949.8@	31.1
	0.06222+j3.21375		0.0671+j3.21148		0.21911+j2.35422		THEVENIN IMPEDANCE (OHM)					

SHORT CIRCUIT MVA= 6002.7

X/R RATIO= 51.6473

R0/X1= 0.06818

X0/X1= 0.73254

BUS	64 AST-WEST	138.KV	AREA	2	ZONE	10	TIER	0	(PREFault V=1.007@ 0.0 PU)		B PHASE		C PHASE		
		+ SEQ		- SEQ		0 SEQ		A PHASE							
		>	0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0	
VOLTAGE (KV, L-G)	>	0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0
BRANCH CURRENT (A) TO	>														
752 ASTW-DUM	138. 1L	1944.1@	91.2	0.0@	0.0	0.0@	0.0	0.0@	0.0	1944.1@	91.2	1944.1@	-28.8	1944.1@	-148.8
129 QUEENSBG	138. 2L	1938.6@	92.1	0.0@	0.0	0.0@	0.0	0.0@	0.0	1938.6@	92.1	1938.6@	-27.9	1938.6@	-147.9
129 QUEENSBG	138. 15L	1887.3@	91.8	0.0@	0.0	0.0@	0.0	0.0@	0.0	1887.3@	91.8	1887.3@	-28.2	1887.3@	-148.2
129 QUEENSBG	138. 14L	3584.6@	91.1	0.0@	0.0	0.0@	0.0	0.0@	0.0	3584.6@	91.1	3584.6@	-28.9	3584.6@	-148.9
129 QUEENSBG	138. 1L	4031.8@	89.3	0.0@	0.0	0.0@	0.0	0.0@	0.0	4031.8@	89.3	4031.8@	-30.7	4031.8@	-150.7
0 HG 5	138. 2L	3052.7@	92.2	0.0@	0.0	0.0@	0.0	0.0@	0.0	3052.7@	92.2	3052.7@	-27.8	3052.7@	-147.8
102 HG 6	138. 1L	3070.8@	92.0	0.0@	0.0	0.0@	0.0	0.0@	0.0	3070.8@	92.0	3070.8@	-28.0	3070.8@	-148.0
100 HG3TAP	138. 1L	25.6@	81.8	0.0@	0.0	0.0@	0.0	0.0@	0.0	25.6@	81.8	25.6@	-38.2	25.6@	-158.2
99 HG2TAP	138. 1L	25.5@	81.7	0.0@	0.0	0.0@	0.0	0.0@	0.0	25.5@	81.7	25.5@	-38.3	25.5@	-158.3
166 AST G3	20. 2T	2696.6@	90.9	0.0@	0.0	0.0@	0.0	0.0@	0.0	2696.6@	90.9	2696.6@	-29.1	2696.6@	-149.1
166 AST G3	20. 1T	2696.6@	90.9	0.0@	0.0	0.0@	0.0	0.0@	0.0	2696.6@	90.9	2696.6@	-29.1	2696.6@	-149.1
CURRENT TO FAULT (A)	>	24949.8@	-88.9	0.0@	0.0	0.0@	0.0	0.0@	0.0	24949.8@	-88.9	24949.8@	151.1	24949.8@	31.1
THEVENIN IMPEDANCE (OHM)	>	3.21435@	88.9	3.21218@	88.8	2.36439@	84.7								

New York Power Authority --- 2005 System Fault Study With Poletti 500MW CAPP O/S

Summary of fault being displayed:

2. 2LG Bus fault on:

AST-WEST 138. kV

	+ SEQ		- SEQ		0 SEQ		A PHASE		B PHASE		C PHASE	
	17524.7@	-88.1	7434.9@	89.5	10100.8@	93.6	0.0@	0.0	26919.7@	147.0	25857.1@	37.0
	THEVENIN IMPEDANCE (OHM)											
	0.06222+j3.21375		0.0671+j3.21148		0.21911+j2.35422							

SHORT CIRCUIT MVA= 6476.7

X/R RATIO= 31.0955

R0/X1= 0.06818

X0/X1= 0.73254

BUS	64 AST-WEST	138.KV	AREA	2 ZONE	10 TIER	0	(PREFault V=1.007@ 0.0 PU)							
			+ SEQ		- SEQ		0 SEQ	A PHASE		B PHASE		C PHASE		
			>	>	>	>	>	>	>	>	>	>	>	
VOLTAGE (KV, L-G)			23.882@	-1.7	23.882@	-1.7	23.882@	-1.7	71.647@	-1.7	0.000@	0.0	0.000@	0.0
BRANCH CURRENT (A) TO														
752 ASTW-DUM	138.	1L	1361.8@	92.0	582.7@	-90.5	1115.0@	-89.7	339.8@	-97.8	2256.5@	-40.6	2259.3@	-137.0
129 QUEENSBG	138.	2L	1362.3@	92.9	577.3@	-89.5	1175.4@	-83.8	390.5@	-80.7	2368.5@	-39.2	2224.7@	-133.1
129 QUEENSBG	138.	15L	1326.2@	92.5	562.0@	-89.8	586.6@	-84.1	179.5@	88.7	1950.2@	-27.9	1849.7@	-146.6
129 QUEENSBG	138.	14L	2518.9@	91.9	1067.5@	-90.5	1175.4@	-83.8	283.6@	83.0	3752.7@	-29.2	3526.3@	-146.3
129 QUEENSBG	138.	1L	2833.2@	90.0	1200.7@	-92.4	586.6@	-84.1	1050.1@	89.4	3857.9@	-22.0	3667.7@	-158.3
0 HG 5	138.	2L	2149.2@	93.0	904.8@	-89.4	794.7@	-80.4	459.1@	86.1	3110.3@	-24.7	2885.0@	-148.5
102 HG 6	138.	1L	2162.0@	92.7	910.1@	-89.6	796.0@	-80.4	465.9@	85.6	3129.4@	-24.8	2897.9@	-148.7
100 HG3TAP	138.	1L	18.3@	82.6	7.4@	-100.2	0.1@	79.7	11.0@	84.4	23.1@	-21.7	22.6@	-174.4
99 HG2TAP	138.	1L	18.2@	82.5	7.3@	-100.2	0.1@	79.7	11.0@	84.3	23.0@	-21.8	22.5@	-174.4
166 AST G3	20.	2T	1888.8@	91.7	808.3@	-90.7	1946.5@	-90.1	869.4@	-94.5	3404.1@	-46.0	3418.5@	-132.4
166 AST G3	20.	1T	1888.8@	91.7	808.3@	-90.7	1946.5@	-90.1	869.4@	-94.5	3404.1@	-46.0	3418.5@	-132.4
CURRENT TO FAULT (A)			>	>	>	>	>	>	>	>	>	>	>	>
THEVENIN IMPEDANCE (OHM)			>	>	>	>	>	>	>	>	>	>	>	>
			3.21435@	88.9	3.21218@	88.8	2.36439@	84.7	0.0@	0.0	26919.7@	147.0	25857.1@	37.0

New York Power Authority --- 2005 System Fault Study With Poletti 500MW CAPP O/S

Summary of fault being displayed:

3. 1LG Bus fault on:

AST-WEST 138. kV

			FAULT CURRENT (A @ DEG)				
	+ SEQ	- SEQ	0 SEQ	A PHASE	B PHASE	C PHASE	
	9127.5@ -87.7	9127.5@ -87.7	9127.5@ -87.7	27382.5@ -87.7	0.0@ 0.0	0.0@ 0.0	
			THEVENIN IMPEDANCE (OHM)				
	0.06222+j3.21375	0.0671+j3.21148	0.21911+j2.35422				

SHORT CIRCUIT MVA= 6588.0

X/R RATIO= 25.1973

R0/X1= 0.06818

X0/X1= 0.73254

BUS	64 AST-WEST	138.KV	AREA	2 ZONE	10 TIER	0	(PREFault V=1.007@ 0.0 PU)		A PHASE	B PHASE	C PHASE
		>	+ SEQ	- SEQ	0 SEQ	0 SEQ	0.000@	0.0	75.054@-115.5	78.138@ 114.4	
VOLTAGE (KV, L-G)		>	50.868@ -0.6	29.319@-178.9	21.581@ 177.0	0.000@	0.0	75.054@-115.5	78.138@ 114.4		
BRANCH CURRENT (A) TO		>									
752 ASTW-DUM	138. 1L		703.3@ 92.4	715.3@ 92.4	1007.6@ 88.9	2425.1@ 90.9	300.6@ 82.9	304.7@ 79.0			
129 QUEENSBG	138. 2L		710.5@ 93.3	708.7@ 93.3	1062.1@ 94.8	2481.2@ 94.0	353.2@ 97.6	353.3@ 98.1			
129 QUEENSBG	138. 15L		691.7@ 93.0	690.0@ 93.0	530.1@ 94.6	1911.6@ 93.4	161.5@ -91.9	161.9@ -93.0			
129 QUEENSBG	138. 14L		1313.8@ 92.3	1310.5@ 92.3	1062.1@ 94.8	3685.7@ 93.1	254.6@ -97.5	255.9@ -98.7			
129 QUEENSBG	138. 1L		1477.7@ 90.5	1474.0@ 90.5	530.1@ 94.6	3480.6@ 91.1	947.6@ -91.7	948.2@ -92.1			
0 HG 5	138. 2L		1127.5@ 93.4	1110.7@ 93.4	718.1@ 98.3	2954.4@ 94.6	406.7@ -93.2	410.2@ -97.2			
102 HG 6	138. 1L		1134.1@ 93.2	1117.3@ 93.2	719.3@ 98.3	2968.6@ 94.4	412.7@ -93.7	416.4@ -97.7			
100 HG3TAP	138. 1L		10.0@ 83.2	9.0@ 82.6	0.1@-101.6	18.9@ 83.0	9.5@ -92.1	9.7@-101.9			
99 HG2TAP	138. 1L		9.9@ 83.2	9.0@ 82.6	0.1@-101.6	18.8@ 82.9	9.5@ -92.1	9.6@-102.0			
166 AST G3	20. 2T		975.3@ 92.1	992.3@ 92.1	1758.9@ 88.6	3724.8@ 90.4	777.3@ 85.3	781.3@ 83.2			
166 AST G3	20. 1T		975.3@ 92.1	992.3@ 92.1	1758.9@ 88.6	3724.8@ 90.4	777.3@ 85.3	781.3@ 83.2			
CURRENT TO FAULT (A)		>	9127.5@ -87.7	9127.5@ -87.7	9127.5@ -87.7	27382.5@ -87.7	0.0@ 0.0	0.0@ 0.0			
THEVENIN IMPEDANCE (OHM)		>	3.21435@ 88.9	3.21218@ 88.8	2.36439@ 84.7						

New York Power Authority --- 2005 System Fault Study With Poletti 500MW CAPP O/S

Summary of fault being displayed:

1. 3LG Bus fault on:

E 179 ST 138. kV

	+ SEQ		- SEQ		0 SEQ		A PHASE		B PHASE		C PHASE	
	39826.9@	-87.5	0.0@	0.0	0.0@	0.0	39826.9@	-87.5	39826.9@	152.5	39826.9@	32.5
	0.08761+j 2.0189		0.10122+j2.01188		0.6975+j2.23418		THEVENIN IMPEDANCE (OHM)					

SHORT CIRCUIT MVA= 9616.1

X/R RATIO= 23.045

R0/X1= 0.34548

X0/X1= 1.10663

BUS	82 E 179 ST	138.KV	AREA	2	ZONE	10	TIER	0	(PREFault V=1.010@ 0.0 PU)		A PHASE		B PHASE		C PHASE		
VOLTAGE (KV, L-G)	>	0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0
BRANCH CURRENT (A) TO	>																
0 E 179 SR	138. 2L	5293.7@	91.6	0.0@	0.0	0.0@	0.0	0.0@	0.0	5293.7@	91.6	5293.7@	-28.4	5293.7@	-148.4		
134 SHM CRK	138. 13L	3824.9@	93.5	0.0@	0.0	0.0@	0.0	0.0@	0.0	3824.9@	93.5	3824.9@	-26.5	3824.9@	-146.5		
134 SHM CRK	138. 1L	3824.9@	93.5	0.0@	0.0	0.0@	0.0	0.0@	0.0	3824.9@	93.5	3824.9@	-26.5	3824.9@	-146.5		
121 TREMNT12	138. 13L	1930.0@	92.0	0.0@	0.0	0.0@	0.0	0.0@	0.0	1930.0@	92.0	1930.0@	-28.0	1930.0@	-148.0		
121 TREMNT12	138. 1L	1930.0@	92.0	0.0@	0.0	0.0@	0.0	0.0@	0.0	1930.0@	92.0	1930.0@	-28.0	1930.0@	-148.0		
120 TREMNT11	138. 14L	1930.0@	92.0	0.0@	0.0	0.0@	0.0	0.0@	0.0	1930.0@	92.0	1930.0@	-28.0	1930.0@	-148.0		
120 TREMNT11	138. 1L	1930.0@	92.0	0.0@	0.0	0.0@	0.0	0.0@	0.0	1930.0@	92.0	1930.0@	-28.0	1930.0@	-148.0		
101 HG TR#4	138. 1L	6753.9@	92.4	0.0@	0.0	0.0@	0.0	0.0@	0.0	6753.9@	92.4	6753.9@	-27.6	6753.9@	-147.6		
98 HG TR#1	138. 1L	6768.9@	92.4	0.0@	0.0	0.0@	0.0	0.0@	0.0	6768.9@	92.4	6768.9@	-27.6	6768.9@	-147.6		
74 DUN-E179	138. 1L	5642.9@	93.1	0.0@	0.0	0.0@	0.0	0.0@	0.0	5642.9@	93.1	5642.9@	-26.9	5642.9@	-146.9		
CURRENT TO FAULT (A)	>	39826.9@	-87.5	0.0@	0.0	0.0@	0.0	0.0@	0.0	39826.9@	-87.5	39826.9@	152.5	39826.9@	32.5		
THEVENIN IMPEDANCE (OHM)	>	2.0208@	87.5	2.01443@	87.1	2.34053@	72.7										



New York Power Authority --- 2005 System Fault Study With Poletti 500MW CAPP O/S

Summary of fault being displayed:

2. 2LG Bus fault on:		FAULT CURRENT (A @ DEG)																					
E 179 ST 138. kV		- SEQ				0 SEQ				A PHASE				B PHASE				C PHASE					
+ SEQ		- SEQ				0 SEQ				A PHASE				B PHASE				C PHASE					
25906.4@ -85.0		14034.1@ 88.3				12078.7@ 102.8				0.0@ 0.0				41724.1@ 157.4				36070.5@ 32.3					
0.08761+j 2.0189		0.10122+j2.01188				0.6975+j2.23418																	
SHORT CIRCUIT MVA= 10074.2												X/R RATIO= 11.5083				R0/X1= 0.34548				X0/X1= 1.10663			
BUS 82 E 179 ST		138.KV		AREA 2		ZONE 10		TIER 0		(PREFault V=1.010@ 0.0 PU)													
VOLTAGE (KV, L-G)		>		+ SEQ		- SEQ		0 SEQ		A PHASE				B PHASE				C PHASE					
BRANCH CURRENT (A) TO		>		28.271@ -4.6		28.271@ -4.6		28.271@ -4.6		84.812@ -4.6				0.000@ 0.0				0.000@ 0.0					
0 E 179 SR		138.	2L	3434.1@	94.1	1869.4@	-93.0	1877.7@	-86.1	380.2@-124.1				5496.5@ -27.3				5107.2@-147.0					
134 SHM CRK		138.	13L	2495.9@	95.9	1335.9@	-91.1	682.3@	-57.1	581.0@ 81.4				3935.2@ -13.9				3101.0@-154.3					
134 SHM CRK		138.	1L	2495.9@	95.9	1335.9@	-91.1	682.3@	-57.1	581.0@ 81.4				3935.2@ -13.9				3101.0@-154.3					
121 TREMNT12		138.	13L	1259.5@	94.4	674.1@	-92.6	584.6@	-87.8	105.9@-179.0				1938.1@ -24.9				1838.4@-149.5					
121 TREMNT12		138.	1L	1259.5@	94.4	674.1@	-92.6	593.6@	-87.9	107.4@-174.2				1941.0@ -25.2				1843.9@-149.3					
120 TREMNT11		138.	14L	1259.5@	94.4	674.1@	-92.6	592.7@	-87.9	106.7@-174.6				1941.3@ -25.2				1842.9@-149.3					
120 TREMNT11		138.	1L	1259.5@	94.4	674.1@	-92.6	584.0@	-87.7	105.3@-179.3				1938.4@ -24.9				1837.6@-149.5					
101 HG TR#4		138.	1L	4376.0@	94.9	2410.7@	-91.0	2479.7@	-71.7	540.9@ -48.4				7496.4@ -23.9				6069.6@-143.4					
98 HG TR#1		138.	1L	4385.7@	94.9	2416.1@	-91.0	2503.1@	-71.7	559.2@ -49.1				7525.1@ -24.0				6088.7@-143.2					
74 DUN-E179		138.	1L	3682.3@	95.6	1971.0@	-91.5	1684.0@	-85.0	263.0@ 176.3				5697.9@ -23.4				5320.1@-148.4					
CURRENT TO FAULT (A)		>		25906.4@ -85.0		14034.1@ 88.3		12078.7@ 102.8		0.0@ 0.0				41724.1@ 157.4				36070.5@ 32.3					
THEVENIN IMPEDANCE (OHM)		>		2.0208@ 87.5		2.01443@ 87.1		2.34053@ 72.7															

New York Power Authority --- 2005 System Fault Study With Poletti 500MW CAPP O/S

Summary of fault being displayed:

3. 1LG Bus fault on:		E 179 ST		138. kV		FAULT CURRENT (A @ DEG)				B PHASE		C PHASE			
		+ SEQ		- SEQ		0 SEQ		A PHASE							
		12719.7@ -81.9		12719.7@ -81.9		12719.7@ -81.9		38159.2@ -81.9		0.0@ 0.0		0.0@ 0.0			
		0.08761+j 2.0189		0.10122+j2.01188		0.6975+j2.23418									
		SHORT CIRCUIT MVA= 9213.4		X/R RATIO= 7.06847		R0/X1= 0.34548		X0/X1= 1.10663							
BUS		82 E 179 ST		138.KV		AREA 2 ZONE 10 TIER 0		(PREFault V=1.010@ 0.0 PU)		B PHASE		C PHASE			
		>		+ SEQ		- SEQ		0 SEQ		A PHASE					
VOLTAGE (KV, L-G)		>		54.956@ -2.6		25.623@-174.8		29.771@ 170.8		0.000@ 0.0		76.517@-125.3		88.511@ 119.8	
BRANCH CURRENT (A) TO		>													
0 E 179 SR		138. 2L		1672.6@ 97.2		1694.3@ 96.8		1977.4@ 89.2		5332.8@ 94.1		379.7@ 56.1		390.0@ 49.7	
134 SHM CRK		138. 13L		1237.0@ 98.9		1210.8@ 98.6		718.5@ 118.3		3134.4@ 103.2		582.5@-103.1		611.5@-106.6	
134 SHM CRK		138. 1L		1237.0@ 98.9		1210.8@ 98.6		718.5@ 118.3		3134.4@ 103.2		582.5@-103.1		611.5@-106.6	
121 TREMNT12		138. 13L		624.3@ 97.5		610.9@ 97.2		615.6@ 87.5		1844.8@ 94.1		116.6@ 3.4		94.2@ -1.2	
121 TREMNT12		138. 1L		624.3@ 97.5		610.9@ 97.2		625.1@ 87.4		1854.1@ 94.0		119.3@ 7.8		96.3@ 4.4	
120 TREMNT11		138. 14L		624.3@ 97.5		610.9@ 97.2		624.2@ 87.5		1853.3@ 94.0		118.5@ 7.5		95.5@ 4.0	
120 TREMNT11		138. 1L		624.3@ 97.5		610.9@ 97.2		615.0@ 87.6		1844.3@ 94.1		115.9@ 3.1		93.6@ -1.5	
101 HG TR#4		138. 1L		2123.5@ 98.1		2184.9@ 98.7		2611.3@ 103.6		6912.9@ 100.4		514.6@ 132.8		502.6@ 119.9	
98 HG TR#1		138. 1L		2128.2@ 98.1		2189.8@ 98.8		2636.0@ 103.6		6947.1@ 100.4		532.2@ 131.8		522.3@ 119.3	
74 DUN-E179		138. 1L		1824.9@ 98.6		1786.4@ 98.3		1773.3@ 90.3		5372.6@ 95.8		287.8@ 0.1		226.0@ -6.7	
CURRENT TO FAULT (A)		>		12719.7@ -81.9		12719.7@ -81.9		12719.7@ -81.9		38159.2@ -81.9		0.0@ 0.0		0.0@ 0.0	
THEVENIN IMPEDANCE (OHM)		>		2.0208@ 87.5		2.01443@ 87.1		2.34053@ 72.7							

New York Power Authority --- 2005 System Fault Study With Poletti 500MW CAPP O/S

Summary of fault being displayed:

1. 3LG Bus fault on:

VERNON E 138. kV

	+ SEQ		- SEQ		0 SEQ		A PHASE		B PHASE		C PHASE	
	33743.4@	-88.6	0.0@	0.0	0.0@	0.0	33743.4@	-88.6	33743.4@	151.4	33743.4@	31.4
	0.05572+j2.37797		0.07193+j 2.3677		0.11194+j1.93888		THEVENIN IMPEDANCE (OHM)					

SHORT CIRCUIT MVA= 8125.0

X/R RATIO= 42.6745

R0/X1= 0.04707

X0/X1= 0.81535

BUS	139 VERNON E	138.KV	AREA	2	ZONE	10	TIER	0	(PREFault V=1.007@ 0.1 PU)		B PHASE		C PHASE	
			+ SEQ				- SEQ		0 SEQ	A PHASE				
VOLTAGE (KV, L-G)	>		0.000@	0.0			0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0
BRANCH CURRENT (A) TO	>													
963 38MO6	138.	1L	392.2@	91.4			0.0@	0.0	0.0@	0.0	392.2@	91.4	392.2@	-148.6
962 38MO4	138.	1L	745.8@	91.2			0.0@	0.0	0.0@	0.0	745.8@	91.2	745.8@	-148.8
960 38MO5	138.	1L	392.2@	91.4			0.0@	0.0	0.0@	0.0	392.2@	91.4	392.2@	-148.6
801 GLENDALE0801	138.	1L	501.3@	92.5			0.0@	0.0	0.0@	0.0	501.3@	92.5	501.3@	-147.5
800 GLENDALE0800	138.	1L	499.4@	92.6			0.0@	0.0	0.0@	0.0	499.4@	92.6	499.4@	-147.4
142 VERQBGR2	138.	1L	5101.8@	90.6			0.0@	0.0	0.0@	0.0	5101.8@	90.6	5101.8@	-149.4
141 VERGRNR2	138.	1L	5865.0@	92.6			0.0@	0.0	0.0@	0.0	5865.0@	92.6	5865.0@	-147.4
131 RNY TR8E	138.	1L	7303.3@	91.5			0.0@	0.0	0.0@	0.0	7303.3@	91.5	7303.3@	-148.5
1251 RAVSW G4 GT	18.	1X	4765.9@	90.7			0.0@	0.0	0.0@	0.0	4765.9@	90.7	4765.9@	-149.3
1261 RAVSW G4 ST	13.8	1X												
170 RAVSW G2	20.	1T	4143.2@	91.3			0.0@	0.0	0.0@	0.0	4143.2@	91.3	4143.2@	-148.7
169 RAVSW G1	20.	1T	4035.6@	91.4			0.0@	0.0	0.0@	0.0	4035.6@	91.4	4035.6@	-148.6
CURRENT TO FAULT (A)	>		33743.4@	-88.6			0.0@	0.0	0.0@	0.0	33743.4@	-88.6	33743.4@	31.4
THEVENIN IMPEDANCE (OHM)	>		2.37862@	88.7			2.36879@	88.3	1.94211@	86.7				

New York Power Authority --- 2005 System Fault Study With Poletti 500MW CAPP O/S

Summary of fault being displayed:

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2. 2LG Bus fault on:
   VERNON E      138. kV

           + SEQ          - SEQ          0 SEQ          A PHASE          B PHASE          C PHASE
23293.6@ -88.2    10495.0@ 90.9    12800.7@ 92.5    0.0@ 0.0    35269.6@ 148.5    34725.2@ 35.1

           THEVENIN IMPEDANCE (OHM)
0.05572+j2.37797  0.07193+j 2.3677  0.11194+j1.93888

SHORT CIRCUIT MVA= 8492.5      X/R RATIO= 33.0752      R0/X1= 0.04707      X0/X1= 0.81535
-----
BUS 139 VERNON E      138.KV AREA 2 ZONE 10 TIER 0      (PREFault V=1.007@ 0.1 PU)
           + SEQ          - SEQ          0 SEQ          A PHASE          B PHASE          C PHASE
VOLTAGE (KV, L-G)    > 24.860@ -0.8    24.860@ -0.8    24.860@ -0.8    74.581@ -0.8    0.000@ 0.0    0.000@ 0.0
BRANCH CURRENT (A) TO >
963 38MO6      138. 1L    270.8@ 91.7    121.5@ -89.4    166.7@ -89.0    18.0@-103.1    417.0@ -34.0    416.4@-143.2
962 38MO4      138. 1L    515.8@ 91.6    230.1@ -89.5    0.1@ 89.2    285.8@ 92.5    664.5@ -11.2    658.5@-166.2
960 38MO5      138. 1L    270.7@ 91.7    121.5@ -89.4    166.7@ -89.0    18.0@-103.1    417.0@ -34.0    416.4@-143.2
801 GLENDALE0801 138. 1L    346.1@ 92.9    155.4@ -88.2    0.1@ 89.2    190.8@ 93.8    446.6@ -9.8    442.5@-165.0
800 GLENDALE0800 138. 1L    344.7@ 93.0    154.8@ -88.2    0.1@ 89.2    190.1@ 93.9    444.9@ -9.7    440.8@-165.0
142 VERQBGR2    138. 1L    3519.8@ 90.9    1582.6@ -90.2    1874.1@ -87.3    70.0@ 67.9    5332.1@ -31.6    5175.2@-146.1
141 VERGRNR2    138. 1L    4045.4@ 93.0    1822.5@ -88.2    1211.5@ -69.3    1119.2@ 75.9    5934.0@ -19.8    5196.0@-151.6
131 RNY TR8E    138. 1L    5070.3@ 91.9    2238.2@ -89.4    2006.6@ -89.4    832.2@ 98.5    7197.5@ -26.9    7192.7@-150.1
1251 RAVSW G4 GT 18. 1X    3279.0@ 91.0    1522.7@ -87.8    3270.9@ -90.8    1514.3@ -91.8    5768.0@ -44.5    5978.8@-134.7
1261 RAVSW G4 ST 13.8 1X
170 RAVSW G2    20. 1T    2853.4@ 91.7    1290.2@ -89.5    2125.3@ -89.2    564.7@ -94.4    4616.3@ -37.7    4619.6@-139.7
169 RAVSW G1    20. 1T    2779.3@ 91.7    1256.7@ -89.4    2048.5@ -89.1    528.5@ -94.4    4483.7@ -37.4    4485.1@-139.8

CURRENT TO FAULT (A) > 23293.6@ -88.2    10495.0@ 90.9    12800.7@ 92.5    0.0@ 0.0    35269.6@ 148.5    34725.2@ 35.1
THEVENIN IMPEDANCE (OHM) > 2.37862@ 88.7    2.36879@ 88.3    1.94211@ 86.7
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New York Power Authority --- 2005 System Fault Study With Poletti 500MW CCPP O/S

Summary of fault being displayed:

3. 1LG Bus fault on:		FAULT CURRENT (A @ DEG)										B PHASE		C PHASE			
VERNON E 138. kV		+ SEQ		- SEQ		0 SEQ		A PHASE		B PHASE		C PHASE					
		11999.5@ -87.9	11999.5@ -87.9	11999.5@ -87.9	35998.6@ -87.9	0.0@	0.0	0.0@	0.0	0.0@	0.0	0.0@	0.0				
		THEVENIN IMPEDANCE (OHM)															
		0.05572+j2.37797	0.07193+j 2.3677	0.11194+j1.93888													
		SHORT CIRCUIT MVA= 8668.1		X/R RATIO= 27.8995		R0/X1= 0.04707		X0/X1= 0.81535									
BUS	139 VERNON E	138.KV	AREA	2	ZONE	10	TIER	0	(PREFault V=1.007@ 0.1 PU)		B PHASE		C PHASE				
		+ SEQ		- SEQ		0 SEQ		A PHASE		B PHASE		C PHASE					
		>	51.724@	-0.3	28.424@	-179.6	23.304@	178.8	0.000@	0.0	77.108@	-117.0	78.317@	116.4			
VOLTAGE (KV, L-G)		>	139.5@	92.1	138.9@	91.8	156.3@	90.6	434.7@	91.5	18.0@	78.5	16.8@	81.1			
BRANCH CURRENT (A) TO		>	138. 1L	139.5@	92.1	138.9@	91.8	156.3@	90.6	434.7@	91.5	18.0@	78.5	16.8@	81.1		
963	38MO6	138. 1L	139.5@	92.1	138.9@	91.8	156.3@	90.6	434.7@	91.5	18.0@	78.5	16.8@	81.1			
962	38MO4	138. 1L	267.3@	91.9	263.1@	91.7	0.0@	0.0	530.3@	91.8	264.3@	-87.4	266.1@	-89.0			
960	38MO5	138. 1L	139.5@	92.1	138.9@	91.8	156.3@	90.6	434.6@	91.5	18.0@	78.5	16.8@	81.1			
801	GLENDAL0801	138. 1L	178.2@	93.2	177.6@	92.9	0.0@	0.0	355.8@	93.1	177.3@	-86.8	178.6@	-87.1			
800	GLENDAL0800	138. 1L	177.5@	93.3	176.9@	93.0	0.0@	0.0	354.4@	93.1	176.6@	-86.7	177.9@	-87.0			
142	VERQBGR2	138. 1L	1810.1@	91.2	1809.5@	90.9	1756.8@	92.4	5376.0@	91.5	60.3@	-129.0	72.5@	-122.2			
141	VERGRNR2	138. 1L	2078.8@	93.4	2083.7@	92.9	1135.7@	110.4	5258.2@	96.8	1039.2@	-105.9	1063.6@	-105.0			
131	RNY TR8E	138. 1L	2656.9@	92.3	2559.1@	91.8	1881.0@	90.2	7096.2@	91.5	723.3@	-76.4	747.6@	-89.9			
1251	RAVSW G4 GT	18. 1X	1672.1@	91.3	1741.0@	93.4	3066.2@	88.8	6475.5@	90.7	1305.8@	86.6	1430.9@	82.3			
1261	RAVSW G4 ST	13.8 1X															
170	RAVSW G2	20. 1T	1459.3@	91.9	1475.1@	91.7	1992.3@	90.4	4926.3@	91.2	531.3@	87.9	522.6@	84.8			
169	RAVSW G1	20. 1T	1421.4@	92.0	1436.9@	91.8	1920.2@	90.5	4778.1@	91.3	497.2@	88.0	488.8@	84.8			
CURRENT TO FAULT (A)		>	11999.5@	-87.9	11999.5@	-87.9	11999.5@	-87.9	35998.6@	-87.9	0.0@	0.0	0.0@	0.0			
THEVENIN IMPEDANCE (OHM)		>	2.37862@	88.7	2.36879@	88.3	1.94211@	86.7									

New York Power Authority --- 2005 System Fault Study With Poletti 500MW CAPP I/S

Summary of fault being displayed:

1. 3LG Bus fault on:

AST-WEST 138. kV

			FAULT CURRENT (A @ DEG)			
	+ SEQ	- SEQ	0 SEQ	A PHASE	B PHASE	C PHASE
	34191.7@ -88.9	0.0@ 0.0	0.0@ 0.0	34191.7@ -88.9	34191.7@ 151.1	34191.7@ 31.1
			THEVENIN IMPEDANCE (OHM)			
	0.04637+j2.37204	0.08445+j2.37225	0.10272+j	1.5192		

SHORT CIRCUIT MVA= 8320.8

X/R RATIO= 51.1541

R0/X1= 0.0433

X0/X1= 0.64046

BUS	64 AST-WEST	138.KV	AREA	2	ZONE	10	TIER	0	(PREFault V=1.018@ 0.0 PU)					
			+ SEQ				- SEQ		0 SEQ	A PHASE	B PHASE	C PHASE		
VOLTAGE (KV, L-G)	>		0.000@	0.0			0.000@	0.0	0.000@	0.0	0.000@	0.0		
BRANCH CURRENT (A) TO	>													
752 ASTW-DUM	138. 1L	1944.1@	91.2				0.0@	0.0	0.0@	0.0	1944.1@	91.2	1944.1@ -28.8	1944.1@-148.8
129 QUEENSBG	138. 2L	1938.6@	92.1				0.0@	0.0	0.0@	0.0	1938.6@	92.1	1938.6@ -27.9	1938.6@-147.9
129 QUEENSBG	138. 15L	1887.3@	91.8				0.0@	0.0	0.0@	0.0	1887.3@	91.8	1887.3@ -28.2	1887.3@-148.2
129 QUEENSBG	138. 14L	3584.6@	91.1				0.0@	0.0	0.0@	0.0	3584.6@	91.1	3584.6@ -28.9	3584.6@-148.9
129 QUEENSBG	138. 1L	4031.8@	89.3				0.0@	0.0	0.0@	0.0	4031.8@	89.3	4031.8@ -30.7	4031.8@-150.7
0 HG 5	138. 2L	3052.7@	92.2				0.0@	0.0	0.0@	0.0	3052.7@	92.2	3052.7@ -27.8	3052.7@-147.8
102 HG 6	138. 1L	3070.8@	92.0				0.0@	0.0	0.0@	0.0	3070.8@	92.0	3070.8@ -28.0	3070.8@-148.0
100 HG3TAP	138. 1L	25.6@	81.8				0.0@	0.0	0.0@	0.0	25.6@	81.8	25.6@ -38.2	25.6@-158.2
99 HG2TAP	138. 1L	25.5@	81.7				0.0@	0.0	0.0@	0.0	25.5@	81.7	25.5@ -38.3	25.5@-158.3
15811 NYPA POL ST1	18. 1T	3120.7@	91.1				0.0@	0.0	0.0@	0.0	3120.7@	91.1	3120.7@ -28.9	3120.7@-148.9
15711 NYPA POL GT2	18. 1T	3059.7@	91.2				0.0@	0.0	0.0@	0.0	3059.7@	91.2	3059.7@ -28.8	3059.7@-148.8
15611 NYPA POL GT1	18. 1T	3061.5@	91.2				0.0@	0.0	0.0@	0.0	3061.5@	91.2	3061.5@ -28.8	3061.5@-148.8
166 AST G3	20. 2T	2696.6@	90.9				0.0@	0.0	0.0@	0.0	2696.6@	90.9	2696.6@ -29.1	2696.6@-149.1
166 AST G3	20. 1T	2696.6@	90.9				0.0@	0.0	0.0@	0.0	2696.6@	90.9	2696.6@ -29.1	2696.6@-149.1
CURRENT TO FAULT (A)	>	34191.7@	-88.9				0.0@	0.0	0.0@	0.0	34191.7@	-88.9	34191.7@ 151.1	34191.7@ 31.1
THEVENIN IMPEDANCE (OHM)	>	2.37249@	88.9				2.37375@	88.0	1.52267@	86.1				

New York Power Authority --- 2005 System Fault Study With Poletti 500MW CAPP I/S

Summary of fault being displayed:

2. 2LG Bus fault on:

AST-WEST 138. kV

+ SEQ	- SEQ	C	LT CURRE	A @ DEG)	B PHASE	C PHASE
24583.0@ -88.3	9607.9@ 90.6	1497	92.4	A PHASE	37487.9@ 144.6	36845.7@ 39.0
			THEVENIN IM	IMPEDANCE (OHM)		
0.04637+j2.37204	0.08445+j2.37225	0.10272	.5192			

SHORT CIRCUIT MVA= 9123.0

X/R =

Z = 33.8638

X0/X1= 0.0433

X0/X1= 0.64046

BUS	64 AST-WEST	138.KV	AREA	2	ZONE	10	TIE	0	(PREF.	V=1.018@	0.0 PU)	A PHASE	B PHASE	C PHASE		
		>	+ SEQ	- SEQ			0 SEQ	-1			A PHASE	B PHASE	C PHASE			
VOLTAGE (KV, L-G)		>	22.807@	-1.4		22.807@	4	22.807@	-1		68.420@	-1.4	0.000@	0.0	0.000@	0.0
BRANCH CURRENT (A) TO		>														
752 ASTW-DUM	138. 1L		1387.9@	91.8		556.4@	-90.2	1064.8@	-89.5		236.7@	-98.8	2242.4@	-40.1	2241.6@	-137.4
129 QUEENSBG	138. 2L		1388.1@	92.7		551.3@	-89.2	1122.5@	-83.6		288.0@	-76.6	2349.2@	-38.7	2206.9@	-133.7
129 QUEENSBG	138. 15L		1351.4@	92.4		536.7@	-89.6	560.2@	-83.8		256.8@	88.1	1947.3@	-27.9	1851.1@	-146.7
129 QUEENSBG	138. 14L		2566.7@	91.7		1019.4@	-90.2	1122.5@	-83.6		432.9@	84.2	3745.2@	-29.2	3528.1@	-146.4
129 QUEENSBG	138. 1L		2887.0@	89.9		1146.6@	-92.1	560.2@	-83.8		1184.5@	88.7	3861.1@	-22.4	3684.8@	-157.9
0 HG 5	138. 2L		2189.8@	92.8		864.0@	-89.1	758.9@	-80.1		576.5@	86.5	3106.8@	-24.8	2892.7@	-148.4
102 HG 6	138. 1L		2202.7@	92.6		869.1@	-89.4	760.2@	-80.1		583.8@	86.1	3125.9@	-25.0	2905.8@	-148.7
100 HG3TAP	138. 1L		18.6@	82.4		7.0@	-99.9	0.1@	80.0		11.7@	83.8	23.1@	-22.6	22.7@	-173.6
99 HG2TAP	138. 1L		18.5@	82.4		7.0@	-99.9	0.1@	80.0		11.6@	83.8	23.0@	-22.6	22.6@	-173.6
15811 NYPA POL ST1	18. 1T		2270.9@	91.7		847.8@	-87.0	1818.7@	-90.2		396.3@	-94.1	3637.8@	-42.0	3762.9@	-135.7
15711 NYPA POL GT2	18. 1T		2226.5@	91.7		831.2@	-87.0	1761.1@	-90.2		366.8@	-94.4	3553.3@	-41.7	3672.7@	-136.0
15611 NYPA POL GT1	18. 1T		2227.9@	91.7		831.7@	-87.0	1761.1@	-90.2		365.9@	-94.4	3554.8@	-41.7	3674.2@	-136.0
166 AST G3	20. 2T		1925.0@	91.5		771.9@	-90.5	1858.9@	-89.8		708.2@	-94.2	3370.5@	-45.3	3377.7@	-132.9
166 AST G3	20. 1T		1925.0@	91.5		771.9@	-90.5	1858.9@	-89.8		708.2@	-94.2	3370.5@	-45.3	3377.7@	-132.9
CURRENT TO FAULT (A)		>	24583.0@	-88.3		9607.9@	90.6	14978.2@	92.4		0.0@	0.0	37487.9@	144.6	36845.7@	39.0
THEVENIN IMPEDANCE (OHM)		>	2.37249@	88.9		2.37375@	88.0	1.52267@	86.1							

New York Power Authority --- 2005 System Fault Study With Poletti 500MW CAPP I/S

Summary of fault being displayed:

3. 1LG Bus fault on:

AST-WEST 138. kV

	+ SEQ		- SEQ		0 SEQ		A PHASE		B PHASE		C PHASE	
	12942.2@	-87.8	12942.2@	-87.8	12942.2@	-87.8	38826.5@	-87.8	0.0@	0.0	0.0@	0.0
	0.04637+j2.37204		0.08445+j2.37225		0.10272+j 1.5192							

SHORT CIRCUIT MVA= 9448.8

X/R RATIO= 26.8206

R0/X1= 0.0433

X0/X1= 0.64046

BUS	64 AST-WEST	138.KV	AREA	2	ZONE	10	TIER	0	(PREFault V=1.018@ 0.0 PU)		B PHASE	C PHASE
		>	+ SEQ	- SEQ	0 SEQ	A PHASE			0.000@	0.0	75.574@-113.3	76.891@ 112.3
VOLTAGE (KV, L-G)		>	50.422@	-0.6	30.722@-179.9	19.707@ 178.3			0.000@	0.0		
BRANCH CURRENT (A) TO		>										
752 ASTW-DUM	138. 1L		714.1@	92.3	749.5@ 91.4	920.1@ 90.2	2383.4@	91.2	197.8@	93.5	186.6@	74.5
129 QUEENSBG	138. 2L		721.2@	93.2	742.6@ 92.3	969.9@ 96.1	2432.7@	94.1	257.5@	109.8	229.7@	102.4
129 QUEENSBG	138. 15L		702.2@	92.9	723.0@ 92.0	484.1@ 95.9	1908.5@	93.3	224.8@	-99.8	239.3@	-90.4
129 QUEENSBG	138. 14L		1333.6@	92.2	1373.2@ 91.3	969.9@ 96.1	3674.5@	92.9	383.4@	-104.6	406.5@	-93.8
129 QUEENSBG	138. 1L		1500.0@	90.4	1544.5@ 89.5	484.1@ 95.9	3526.2@	90.7	1024.1@	-95.1	1061.5@	-90.8
0 HG 5	138. 2L		1144.3@	93.3	1163.9@ 92.4	655.8@ 99.6	2960.3@	94.3	496.6@	-98.0	521.4@	-93.8
102 HG 6	138. 1L		1151.1@	93.1	1170.7@ 92.2	656.8@ 99.6	2974.8@	94.2	503.1@	-98.5	527.8@	-94.2
100 HG3TAP	138. 1L		10.1@	83.1	9.5@ 81.7	0.1@-100.3	19.5@	82.4	9.6@	-94.2	10.1@	-100.8
99 HG2TAP	138. 1L		10.1@	83.1	9.4@ 81.6	0.1@-100.3	19.4@	82.4	9.6@	-94.2	10.0@	-100.9
15811 NYPA POL ST1	18. 1T		1241.4@	92.0	1142.0@ 94.6	1571.5@ 89.5	3952.3@	91.8	380.8@	63.6	422.9@	91.1
15711 NYPA POL GT2	18. 1T		1217.1@	92.0	1119.7@ 94.5	1521.7@ 89.6	3856.1@	91.8	356.7@	62.5	394.3@	91.3
15611 NYPA POL GT1	18. 1T		1217.9@	92.1	1120.4@ 94.5	1521.7@ 89.6	3857.5@	91.8	356.0@	62.5	393.7@	91.3
166 AST G3	20. 2T		990.3@	92.0	1039.7@ 91.1	1606.2@ 89.9	3635.8@	90.8	604.2@	91.3	583.5@	82.9
166 AST G3	20. 1T		990.3@	92.0	1039.7@ 91.1	1606.2@ 89.9	3635.8@	90.8	604.2@	91.3	583.5@	82.9
CURRENT TO FAULT (A)	>		12942.2@	-87.8	12942.2@ -87.8	12942.2@ -87.8	38826.5@	-87.8	0.0@	0.0	0.0@	0.0
THEVENIN IMPEDANCE (OHM)	>		2.37249@	88.9	2.37375@ 88.0	1.52267@ 86.1						



New York Power Authority --- 2005 System Fault Study With Poletti 500MW CAPP I/S

Summary of fault being displayed:

1. 3LG Bus fault on:

E 179 ST 138. kv

	+ SEQ	- SEQ	0 SEQ	A PHASE	B PHASE	C PHASE
	40515.0@ -87.5	0.0@ 0.0	0.0@ 0.0	40515.0@ -87.5	40515.0@ 152.5	40515.0@ 32.5
	THEVENIN IMPEDANCE (OHM)					
	0.08635+j1.98891	0.10074+j1.98214	0.68561+j2.20636			

SHORT CIRCUIT MVA= 9803.4 X/R RATIO= 23.0332 R0/X1= 0.34472 X0/X1= 1.10933

BUS	82 E 179 ST	138.KV	AREA	2	ZONE	10	TIER	0	(PREFault V=1.012@ 0.0 PU)		B PHASE		C PHASE	
		>	+ SEQ	- SEQ	0 SEQ	0 SEQ	A PHASE	0.0						
VOLTAGE (KV, L-G)		>	0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0
BRANCH CURRENT (A) TO		>												
0 E 179 SR	138. 2L		5949.9@	91.7	0.0@	0.0	0.0@	0.0	5949.9@	91.7	5949.9@	-28.3	5949.9@	-148.3
134 SHM CRK	138. 13L		3829.9@	93.4	0.0@	0.0	0.0@	0.0	3829.9@	93.4	3829.9@	-26.6	3829.9@	-146.6
134 SHM CRK	138. 1L		3829.9@	93.4	0.0@	0.0	0.0@	0.0	3829.9@	93.4	3829.9@	-26.6	3829.9@	-146.6
121 TREMNT12	138. 13L		1932.5@	92.0	0.0@	0.0	0.0@	0.0	1932.5@	92.0	1932.5@	-28.0	1932.5@	-148.0
121 TREMNT12	138. 1L		1932.5@	92.0	0.0@	0.0	0.0@	0.0	1932.5@	92.0	1932.5@	-28.0	1932.5@	-148.0
120 TREMNT11	138. 14L		1932.5@	92.0	0.0@	0.0	0.0@	0.0	1932.5@	92.0	1932.5@	-28.0	1932.5@	-148.0
120 TREMNT11	138. 1L		1932.5@	92.0	0.0@	0.0	0.0@	0.0	1932.5@	92.0	1932.5@	-28.0	1932.5@	-148.0
101 HG TR#4	138. 1L		6756.0@	92.4	0.0@	0.0	0.0@	0.0	6756.0@	92.4	6756.0@	-27.6	6756.0@	-147.6
98 HG TR#1	138. 1L		6771.0@	92.4	0.0@	0.0	0.0@	0.0	6771.0@	92.4	6771.0@	-27.6	6771.0@	-147.6
74 DUN-E179	138. 1L		5650.4@	93.1	0.0@	0.0	0.0@	0.0	5650.4@	93.1	5650.4@	-26.9	5650.4@	-146.9
CURRENT TO FAULT (A)		>	40515.0@	-87.5	0.0@	0.0	0.0@	0.0	40515.0@	-87.5	40515.0@	152.5	40515.0@	32.5
THEVENIN IMPEDANCE (OHM)		>	1.99078@	87.5	1.9847@	87.1	2.31043@	72.7						

New York Power Authority --- 2005 System Fault Study With Poletti 500MW CAPP I/S

Summary of fault being displayed:

2. 2LG Bus fault on:  
E 179 ST 138. kV

				FAULT CURRENT (A @ DEG)					
	+ SEQ	- SEQ	0 SEQ	A PHASE	B PHASE	C PHASE			
	26345.6@ -85.0	14283.0@ 88.4	12269.4@ 102.7	0.0@ 0.0	42410.8@ 157.4	36704.5@ 32.3			
				THEVENIN IMPEDANCE (OHM)					
	0.08635+j1.98891	0.10074+j1.98214	0.68561+j2.20636						

SHORT CIRCUIT MVA= 10262.1      X/R RATIO= 11.5244      R0/X1= 0.34472      X0/X1= 1.10933

BUS	82 E 179 ST	138.KV	AREA	2	ZONE	10	TIER	0	(PREFault V=1.012@ 0.0 PU)							
			+ SEQ				- SEQ		0 SEQ	A PHASE	B PHASE	C PHASE				
VOLTAGE (KV, L-G)	>		28.348@	-4.5			28.348@	-4.5	28.348@	-4.5	85.043@	-4.5	0.000@ 0.0	0.000@ 0.0		
BRANCH CURRENT (A) TO	>															
0 E 179 SR	138. 2L		3884.3@	94.1			2075.4@	-92.6	2037.6@	-85.8	323.7@	-134.4	6147.0@	-26.8	5722.8@	-147.3
134 SHM CRK	138. 13L		2495.8@	95.9			1341.1@	-91.1	684.6@	-57.0	574.2@	81.1	3940.4@	-13.9	3103.5@	-154.3
134 SHM CRK	138. 1L		2495.8@	95.9			1341.1@	-91.1	684.6@	-57.0	574.2@	81.1	3940.4@	-13.9	3103.5@	-154.3
121 TREMNT12	138. 13L		1259.4@	94.4			676.7@	-92.6	586.6@	-87.8	105.7@	-176.5	1940.5@	-24.9	1840.5@	-149.5
121 TREMNT12	138. 1L		1259.4@	94.4			676.7@	-92.6	595.6@	-87.9	107.6@	-171.7	1943.4@	-25.2	1846.0@	-149.3
120 TREMNT11	138. 14L		1259.4@	94.4			676.7@	-92.6	594.8@	-87.8	106.9@	-172.1	1943.7@	-25.2	1845.0@	-149.3
120 TREMNT11	138. 1L		1259.4@	94.4			676.7@	-92.6	586.0@	-87.7	105.1@	-176.8	1940.8@	-24.9	1839.7@	-149.5
101 HG TR#4	138. 1L		4370.9@	94.9			2417.9@	-91.0	2486.5@	-71.7	557.3@	-49.4	7500.2@	-23.9	6069.4@	-143.4
98 HG TR#1	138. 1L		4380.6@	94.9			2423.3@	-91.0	2510.0@	-71.7	575.8@	-50.0	7529.0@	-24.0	6088.4@	-143.2
74 DUN-E179	138. 1L		3682.0@	95.6			1978.7@	-91.5	1689.6@	-85.0	261.2@	179.2	5705.0@	-23.4	5326.0@	-148.4
CURRENT TO FAULT (A)	>		26345.6@	-85.0			14283.0@	88.4	12269.4@	102.7	0.0@ 0.0	42410.8@ 157.4	36704.5@ 32.3			
THEVENIN IMPEDANCE (OHM)	>		1.99078@	87.5			1.9847@	87.1	2.31043@	72.7						

New York Power Authority --- 2005 System Fault Study With Poletti 500MW CAPP I/S

Summary of fault being displayed:

3. 1LG Bus fault on:  
E 179 ST 138. kV

	+ SEQ		- SEQ		0 SEQ		A PHASE		B PHASE		C PHASE	
	12928.3@	-81.9	12928.3@	-81.9	12928.3@	-81.9	38784.9@	-81.9	0.0@	0.0	0.0@	0.0
	THEVENIN IMPEDANCE (OHM)											
	0.08635+j1.98891		0.10074+j1.98214		0.68561+j2.20636							

SHORT CIRCUIT MVA= 9384.7      X/R RATIO= 7.07845      R0/X1= 0.34472      X0/X1= 1.10933

BUS	82 E 179 ST	138.KV	AREA	2	ZONE	10	TIER	0	(PREFault V=1.012@ 0.0 PU)		B PHASE		C PHASE	
VOLTAGE (KV, L-G)	>	55.096@	-2.6	25.659@	-174.8	29.870@	170.8	0.000@	0.0	76.760@	-125.3	88.693@	119.8	
BRANCH CURRENT (A) TO	>													
0 E 179 SR	138. 2L	1928.3@	97.1	1878.5@	97.1	2147.1@	89.5	5941.9@	94.4	396.1@	41.7	328.5@	50.2	
134 SHM CRK	138. 13L	1232.5@	99.0	1213.9@	98.6	721.4@	118.3	3135.5@	103.2	581.6@	-104.0	607.7@	-106.3	
134 SHM CRK	138. 1L	1232.5@	99.0	1213.9@	98.6	721.4@	118.3	3135.5@	103.2	581.6@	-104.0	607.7@	-106.3	
121 TREMNT12	138. 13L	622.0@	97.5	612.5@	97.1	618.1@	87.6	1846.6@	94.1	112.7@	5.0	96.9@	0.4	
121 TREMNT12	138. 1L	622.0@	97.5	612.5@	97.1	627.6@	87.5	1855.9@	94.0	115.8@	9.6	99.3@	5.9	
120 TREMNT11	138. 14L	622.0@	97.5	612.5@	97.1	626.7@	87.5	1855.1@	94.0	114.9@	9.3	98.4@	5.4	
120 TREMNT11	138. 1L	622.0@	97.5	612.5@	97.1	617.5@	87.6	1846.1@	94.1	112.0@	4.8	96.3@	0.1	
101 HG TR#4	138. 1L	2112.6@	98.1	2188.5@	98.7	2620.0@	103.7	6914.2@	100.4	536.0@	133.3	508.4@	118.6	
98 HG TR#1	138. 1L	2117.2@	98.1	2193.4@	98.7	2644.8@	103.7	6948.4@	100.4	553.6@	132.4	528.3@	118.1	
74 DUN-E179	138. 1L	1818.2@	98.6	1791.0@	98.2	1780.4@	90.3	5377.6@	95.8	275.7@	1.9	232.8@	-4.6	
CURRENT TO FAULT (A)	>	12928.3@	-81.9	12928.3@	-81.9	12928.3@	-81.9	38784.9@	-81.9	0.0@	0.0	0.0@	0.0	
THEVENIN IMPEDANCE (OHM)	>	1.99078@	87.5	1.9847@	87.1	2.31043@	72.7							

New York Power Authority --- 2005 System Fault Study With Poletti 500MW CCPP I/S

Summary of fault being displayed:

1. 3LG Bus fault on:  
VERNON E 138. kV

			FAULT CURRENT (A @ DEG)					
	+ SEQ	- SEQ	0 SEQ	A PHASE	B PHASE	C PHASE		
	34772.6@ -88.6	0.0@ 0.0	0.0@ 0.0	34772.6@ -88.6	34772.6@ 151.4	34772.6@ 31.4		
			THEVENIN IMPEDANCE (OHM)					
	0.05294+j2.31488	0.07076+j2.30522	0.11213+j	1.91				

SHORT CIRCUIT MVA= 8399.2

X/R RATIO= 43.7266

R0/X1= 0.04844

X0/X1= 0.8251

BUS	139 VERNON E	138.KV	AREA	2	ZONE	10	TIER	0	(PREFault V=1.011@ 0.1 PU)		B PHASE		C PHASE		
									0 SEQ	A PHASE	0.000@	0.0	0.000@	0.0	0.000@
VOLTAGE (KV, L-G)	>		0.000@	0.0		0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0	0.000@	0.0
BRANCH CURRENT (A) TO	>														
963 38MO6	138. 1L		405.7@	91.3		0.0@	0.0	0.0@	0.0	405.7@	91.3	405.7@	-28.7	405.7@	-148.7
962 38MO4	138. 1L		771.4@	91.2		0.0@	0.0	0.0@	0.0	771.4@	91.2	771.4@	-28.8	771.4@	-148.8
960 38MO5	138. 1L		405.6@	91.3		0.0@	0.0	0.0@	0.0	405.6@	91.3	405.6@	-28.7	405.6@	-148.7
801 GLENDALE0801	138. 1L		518.6@	92.4		0.0@	0.0	0.0@	0.0	518.6@	92.4	518.6@	-27.6	518.6@	-147.6
800 GLENDALE0800	138. 1L		516.6@	92.5		0.0@	0.0	0.0@	0.0	516.6@	92.5	516.6@	-27.5	516.6@	-147.5
142 VERQBGR2	138. 1L		5906.0@	90.5		0.0@	0.0	0.0@	0.0	5906.0@	90.5	5906.0@	-29.5	5906.0@	-149.5
141 VERGRNR2	138. 1L		5890.9@	92.6		0.0@	0.0	0.0@	0.0	5890.9@	92.6	5890.9@	-27.4	5890.9@	-147.4
131 RNY TR8E	138. 1L		7329.7@	91.5		0.0@	0.0	0.0@	0.0	7329.7@	91.5	7329.7@	-28.5	7329.7@	-148.5
1251 RAVSW G4 GT	18. 1X		4765.9@	90.7		0.0@	0.0	0.0@	0.0	4765.9@	90.7	4765.9@	-29.3	4765.9@	-149.3
1261 RAVSW G4 ST	13.8 1X														
170 RAVSW G2	20. 1T		4186.9@	91.3		0.0@	0.0	0.0@	0.0	4186.9@	91.3	4186.9@	-28.7	4186.9@	-148.7
169 RAVSW G1	20. 1T		4077.8@	91.4		0.0@	0.0	0.0@	0.0	4077.8@	91.4	4077.8@	-28.6	4077.8@	-148.6
CURRENT TO FAULT (A)	>		34772.6@	-88.6		0.0@	0.0	0.0@	0.0	34772.6@	-88.6	34772.6@	151.4	34772.6@	31.4
THEVENIN IMPEDANCE (OHM)	>		2.31548@	88.7		2.3063@	88.2	1.91329@	86.6						

New York Power Authority --- 2005 System Fault Study With Poletti 500MW CCPP I/S

Summary of fault being displayed:

2. 2LG Bus fault on:  
VERNON E 138. kV

			FAULT CURRENT (A @ DEG)					
	+ SEQ	- SEQ	0 SEQ	A PHASE	B PHASE	C PHASE		
	23954.8@ -88.2	10862.9@ 90.9	13094.2@ 92.5	0.0@ 0.0	36271.2@ 148.7	35697.1@ 34.9		
			THEVENIN IMPEDANCE (OHM)					
	0.05294+j2.31488	0.07076+j2.30522	0.11213+j	1.91				

SHORT CIRCUIT MVA= 8761.2

X/R RATIO= 33.2656

R0/X1= 0.04844

X0/X1= 0.8251

BUS	139 VERNON E	138.KV	AREA	2 ZONE	10 TIER	0	(PREFault V=1.011@ 0.1 PU)		B PHASE	C PHASE	
			+ SEQ	- SEQ	0 SEQ	A PHASE					
VOLTAGE (KV, L-G)	>	25.053@	-0.9	25.053@	-0.9	25.053@	-0.9	75.159@	-0.9	0.000@ 0.0	0.000@ 0.0
BRANCH CURRENT (A) TO	>										
963 38MO6	138. 1L	279.6@	91.7	126.2@	-89.4	171.1@	-89.0	18.3@	-103.1	430.3@ -33.8	429.5@-143.4
962 38MO4	138. 1L	532.5@	91.6	239.0@	-89.5	0.1@	89.1	293.6@	92.5	687.2@ -11.1	680.9@-166.3
960 38MO5	138. 1L	279.5@	91.7	126.2@	-89.4	171.0@	-89.0	18.3@	-103.1	430.3@ -33.8	429.5@-143.4
801 GLENDALE0801	138. 1L	357.3@	92.8	161.4@	-88.3	0.1@	89.1	196.0@	93.8	461.8@ -9.7	457.6@-165.1
800 GLENDALE0800	138. 1L	355.9@	92.9	160.7@	-88.2	0.1@	89.1	195.3@	93.8	460.0@ -9.7	455.8@-165.1
142 VERQBGR2	138. 1L	4087.4@	90.9	1818.7@	-90.1	2071.9@	-87.0	204.1@	77.4	6127.4@ -31.0	5944.4@-146.8
141 VERGRNR2	138. 1L	4050.0@	93.0	1843.8@	-88.3	1222.4@	-69.3	1093.1@	75.5	5959.8@ -19.7	5213.0@-151.6
131 RNY TR8E	138. 1L	5072.1@	91.9	2262.9@	-89.5	2025.9@	-89.5	791.2@	99.4	7221.4@ -26.9	7216.5@-150.1
1251 RAVSW G4 GT	18. 1X	3267.5@	91.1	1534.5@	-87.8	3296.3@	-90.9	1563.1@	-91.9	5775.9@ -44.7	5990.5@-134.6
1261 RAVSW G4 ST	13.8 1X										
170 RAVSW G2	20. 1T	2874.9@	91.7	1312.3@	-89.5	2141.8@	-89.3	582.2@	-94.6	4655.1@ -37.6	4659.8@-139.8
169 RAVSW G1	20. 1T	2800.0@	91.8	1278.2@	-89.5	2064.3@	-89.2	545.4@	-94.7	4521.3@ -37.3	4523.9@-140.0
CURRENT TO FAULT (A)	>	23954.8@	-88.2	10862.9@	90.9	13094.2@	92.5	0.0@	0.0	36271.2@ 148.7	35697.1@ 34.9
THEVENIN IMPEDANCE (OHM)	>	2.31548@	88.7	2.3063@	88.2	1.91329@	86.6				

New York Power Authority --- 2005 System Fault Study With Poletti 500MW CAPP I/S

Summary of fault being displayed:

3. 1LG Bus fault on:

VERNON E 138. kV

	+ SEQ		- SEQ		0 SEQ		A PHASE		B PHASE		C PHASE	
	12321.9@	-87.9	12321.9@	-87.9	12321.9@	-87.9	36965.6@	-87.9	0.0@	0.0	0.0@	0.0
	0.05294+j2.31488		0.07076+j2.30522		0.11213+j		1.91					

FAULT CURRENT (A @ DEG)

THEVENIN IMPEDANCE (OHM)

SHORT CIRCUIT MVA= 8928.9

X/R RATIO= 27.6902

R0/X1= 0.04844

X0/X1= 0.8251

BUS	139	VERNON E	138.KV	AREA	2	ZONE	10	TIER	0	(PREFault V=1.011@ 0.1 PU)		B PHASE		C PHASE	
				+ SEQ		- SEQ		0 SEQ		A PHASE					
VOLTAGE (KV, L-G)	>	51.988@	-0.4	28.418@	-179.6	23.575@	178.8	0.000@	0.0	77.472@	-117.3	78.718@	116.6		
BRANCH CURRENT (A) TO	>														
963 38MO6	138.	1L	143.9@	92.1	143.1@	91.8	161.0@	90.6	448.0@	91.5	18.4@	78.0	17.2@	81.4	
962 38MO4	138.	1L	275.6@	91.9	271.1@	91.7	0.0@	0.0	546.7@	91.8	272.6@	-87.4	274.3@	-89.0	
960 38MO5	138.	1L	143.9@	92.1	143.1@	91.8	160.9@	90.6	447.9@	91.5	18.4@	78.0	17.2@	81.4	
801 GLENDALE0801	138.	1L	183.8@	93.2	183.0@	93.0	0.0@	0.0	366.8@	93.1	182.8@	-86.7	184.1@	-87.1	
800 GLENDALE0800	138.	1L	183.1@	93.3	182.3@	93.0	0.0@	0.0	365.4@	93.2	182.1@	-86.6	183.4@	-87.1	
142 VERQBGR2	138.	1L	2131.8@	91.2	2063.0@	91.2	1949.7@	92.6	6144.0@	91.6	148.8@	-85.1	184.2@	-125.3	
141 VERGRNR2	138.	1L	2070.4@	93.4	2091.4@	92.9	1150.3@	110.3	5271.9@	96.9	1029.4@	-107.1	1048.3@	-104.6	
131 RNY TR8E	138.	1L	2644.3@	92.3	2566.8@	91.8	1906.4@	90.1	7116.7@	91.5	690.9@	-77.1	721.9@	-88.2	
1251 RAVSW G4 GT	18.	1X	1656.3@	91.4	1740.6@	93.4	3101.8@	88.8	6494.9@	90.7	1350.4@	87.1	1475.0@	81.8	
1261 RAVSW G4 ST	13.8	1X													
170 RAVSW G2	20.	1T	1464.0@	92.0	1488.6@	91.7	2015.4@	90.3	4967.6@	91.2	546.1@	88.5	536.9@	83.9	
169 RAVSW G1	20.	1T	1425.8@	92.1	1449.9@	91.8	1942.6@	90.4	4817.8@	91.3	511.5@	88.6	502.6@	83.8	
CURRENT TO FAULT (A)	>	12321.9@	-87.9	12321.9@	-87.9	12321.9@	-87.9	36965.6@	-87.9	0.0@	0.0	0.0@	0.0		
THEVENIN IMPEDANCE (OHM)	>	2.31548@	88.7	2.3063@	88.2	1.91329@	86.6								