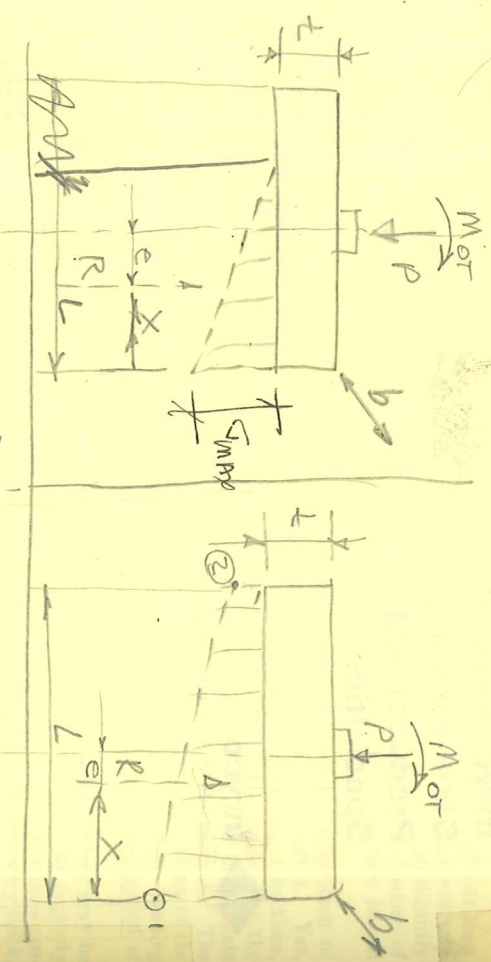


footing. In that case, the pressure diagram becomes triangular, as shown in Fig. 7-12d. The pressures extend over a distance of $3(b/2 - e)$. The maximum pressure is

$$p = \frac{2P}{3(b/2 - e)} \quad (7-18)$$

Treatment of a square or rectangular spread footing with overturning moment M about one principal axis is similar. For full bearing on the footing, the maximum and



$$\left. \begin{aligned} M_{OT} = \\ M_{RESIST} = \end{aligned} \right\} \frac{MR}{M_{OT}} \approx 1.5 \text{ TO } 1.8$$

$$X = \frac{MR - M_{OT}}{W_{TOTAL}} \quad (W_{TOTAL} \approx P)$$

SOLV PRESS = $\frac{2W}{3(X)(b)}$

~~L = 3X~~

$$W = \frac{\sigma_{MAX}}{2} (3X)(b)$$

$$\Rightarrow \sigma_{MAX} \approx \frac{2W}{3Xb}$$

SOLV PRESS!

~~ANALYSIS~~

$$e = \frac{1}{2}L - X$$

$$p_1 = \frac{P}{bL} \left(1 + \frac{6e}{L} \right)$$

$$p_2 = \frac{P}{bL} \left(1 - \frac{6e}{L} \right)$$

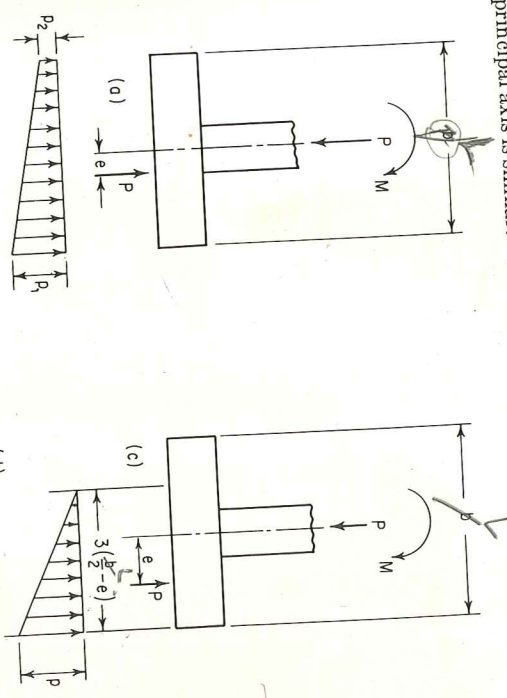


Fig. 7-12. Footings subjected to overturning.

minimum pressures are

$$p_1 = \frac{P}{bL} \left(1 + \frac{6e}{L} \right) \quad (7-19a)$$

$$p_2 = \frac{P}{bL} \left(1 - \frac{6e}{L} \right) \quad (7-19b)$$

where L = length of footing in the plane of overturning
 b = length of the other side of the footing
 When $e > L/6$, the resultant lies outside the middle third and full bearing does not exist. In that case, the pressure diagram is a triangular prism, and the maximum pressure is

$$p = \frac{2P}{3b(L/2 - e)} \quad (7-20)$$

For square or rectangular footings subjected to overturning about two principal axes and for unsymmetrical footings, the procedure is generally similar. Eccentricities of the loading, e_1 and e_2 , are determined about the two principal axes. Then, for bearing over the entire footing, the maximum soil pressure is computed from

$$p = \frac{P}{A} \left(1 + \frac{e_1c_1}{r_1^2} + \frac{e_2c_2}{r_2^2} \right) \quad (7-21)$$