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[ STUDENT > # Rev 5 - Add Xm 7/29/10
[ STUDENT > # in the subsequent rev, will change X to w*L
[ STUDENT >
[ STUDENT > restart; Digits:=4;
                                Digits := 4
[ STUDENT > # Construct Thevinin equivalent of R1, L1, Xm feeding
output at mag branch
[ STUDENT > # Vth is with output open circuited... could also move X1
together with X2... not done here
[ STUDENT > # can move X1 and X2 to either side of Xm as convenient
[ STUDENT > # try the way that makes the Thev ckt simpler:
[ STUDENT > Vth:=Vs*I*XM/(I*XM+R1);
                                Vth :=  $\frac{I V_s X_M}{I X_M + R_1}$ 
[ STUDENT > # Zth is Vth/Isc
[ STUDENT > Isc:=Vs/R1;
                                Isc :=  $\frac{V_s}{R_1}$ 
[ STUDENT > Zth:=Vth/Isc;
                                Zth :=  $\frac{I X_M R_1}{I X_M + R_1}$ 
[ STUDENT >
[ STUDENT >
[ STUDENT > Z:=Zth+2*I*X2+R2/s;
                                Z :=  $\frac{I X_M R_1}{I X_M + R_1} + 2 I X_2 + \frac{R_2}{s}$ 
[ STUDENT >
[ STUDENT > # find current I2 by ohms law
[ STUDENT > I2:=Vth/Z;
                                I2 :=  $\frac{I V_s X_M}{(I X_M + R_1) \left( \frac{I X_M R_1}{I X_M + R_1} + 2 I X_2 + \frac{R_2}{s} \right)}$ 
[ STUDENT > I2:=simplify(I2);
                                I2 :=  $\frac{I s X_M V_s}{I X_M R_1 s - 2 X_2 s X_M + 2 I X_2 s R_1 + I R_2 X_M + R_2 R_1}$ 
[ STUDENT > Iabs:=evalc(abs(I2));
Iabs :=  $\left( \frac{s^2 X_M^2 V_s^2 (-2 X_2 s X_M + R_2 R_1)^2}{((-2 X_2 s X_M + R_2 R_1)^2 + (X_M R_1 s + 2 X_2 s R_1 + R_2 X_M)^2)} \right)^{1/2}$ 

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$$\left. + \frac{s^2 XM^2 Vs^2 (XM RI s + 2 X2 s RI + R2 XM)^2}{((-2 X2 s XM + R2 RI)^2 + (XM RI s + 2 X2 s RI + R2 XM)^2)} \right)^{1/2}$$

STUDENT > # NEED TO CONVERT THIS TO A MAGNITUDE

STUDENT > # Find eq circuit total power P2 (Pairgap) leaving stator using total equivalent resistance R2/s. (note than angle of I is irrelevant in this particular calc.... can calculate real power and apparent power without ever dealing with current angle.

STUDENT > P2:=Iabs^2*R2/s;

$$P2 := \left(\frac{s^2 XM^2 Vs^2 (-2 X2 s XM + R2 RI)^2}{((-2 X2 s XM + R2 RI)^2 + (XM RI s + 2 X2 s RI + R2 XM)^2)} + \frac{s^2 XM^2 Vs^2 (XM RI s + 2 X2 s RI + R2 XM)^2}{((-2 X2 s XM + R2 RI)^2 + (XM RI s + 2 X2 s RI + R2 XM)^2)} \right) R2 / s$$

STUDENT > # The above quantity acts the same as the following quantity.

STUDENT > # Find Shaft Horsepower (**neglecting motor mech losses...maybe need a better name) P_SHP using eq circuit total power (I^2*R2/s) minus rotor losses (I^2*R2)
 # = I^2*R2*(1/s - 1) =
 # = I^2*R2*(1/s - s/s)
 # = I^2*R2*(1-s)/s

STUDENT > P_SHP:=Iabs^2*R2*(1-s)/s;

$$P_SHP := \left(\frac{s^2 XM^2 Vs^2 (-2 X2 s XM + R2 RI)^2}{((-2 X2 s XM + R2 RI)^2 + (XM RI s + 2 X2 s RI + R2 XM)^2)} + \frac{s^2 XM^2 Vs^2 (XM RI s + 2 X2 s RI + R2 XM)^2}{((-2 X2 s XM + R2 RI)^2 + (XM RI s + 2 X2 s RI + R2 XM)^2)} \right) R2 (1 - s) / s$$

STUDENT > # In the linear range of small s where R2 dominates the denominator:

STUDENT > # P APPROX EQUAL V2^2*s/R2 (not just prop)

STUDENT > # Slope of P_SHP vs s is Papprox/s = V^2/R2

STUDENT >

STUDENT > # find rotational speed w

STUDENT > w:=wsync*(1-s);

$$w := wsync (1 - s)$$

STUDENT >

STUDENT > # find Torque T

STUDENT > T:=P_SHP/w;

$$T := \left(\frac{s^2 XM^2 Vs^2 (-2 X2 s XM + R2 RI)^2}{((-2 X2 s XM + R2 RI)^2 + (XM RI s + 2 X2 s RI + R2 XM)^2)} + \frac{s^2 XM^2 Vs^2 (XM RI s + 2 X2 s RI + R2 XM)^2}{((-2 X2 s XM + R2 RI)^2 + (XM RI s + 2 X2 s RI + R2 XM)^2)} \right) R2 / (s wsync)$$

STUDENT > # in the range where R2/s dominates the denominator (the linear range of T vs s), the following hold:

STUDENT > # T linear with s

STUDENT > # T prop to V^2

STUDENT > # T prop to (1/R)

STUDENT > # T APPROX EQUAL to (V^2*s)/(R2wsync) (not just prop)

STUDENT > # T prop to V^2 ANY SPEED (not just the linear range with s)

STUDENT > # is there a more direct way to find T directly (without going through p_shp)

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STUDENT > subs1:={R1=1,R2=0.15,X1=0.5,X2=0.5,Vs=1,wsync=60,XM=20};

subs1 := {R2 = .15, RI = 1, XI = .5, XM = 20, wsync = 60, Vs = 1, X2 = .5}

STUDENT > subs2:={R1=1,R2=0.7,X1=0.5,X2=0.5,Vs=1,wsync=60,XM=20};

subs2 := {RI = 1, XI = .5, XM = 20, wsync = 60, Vs = 1, X2 = .5, R2 = .7}

STUDENT > T1:=subs(subs1,T);

T1 :=

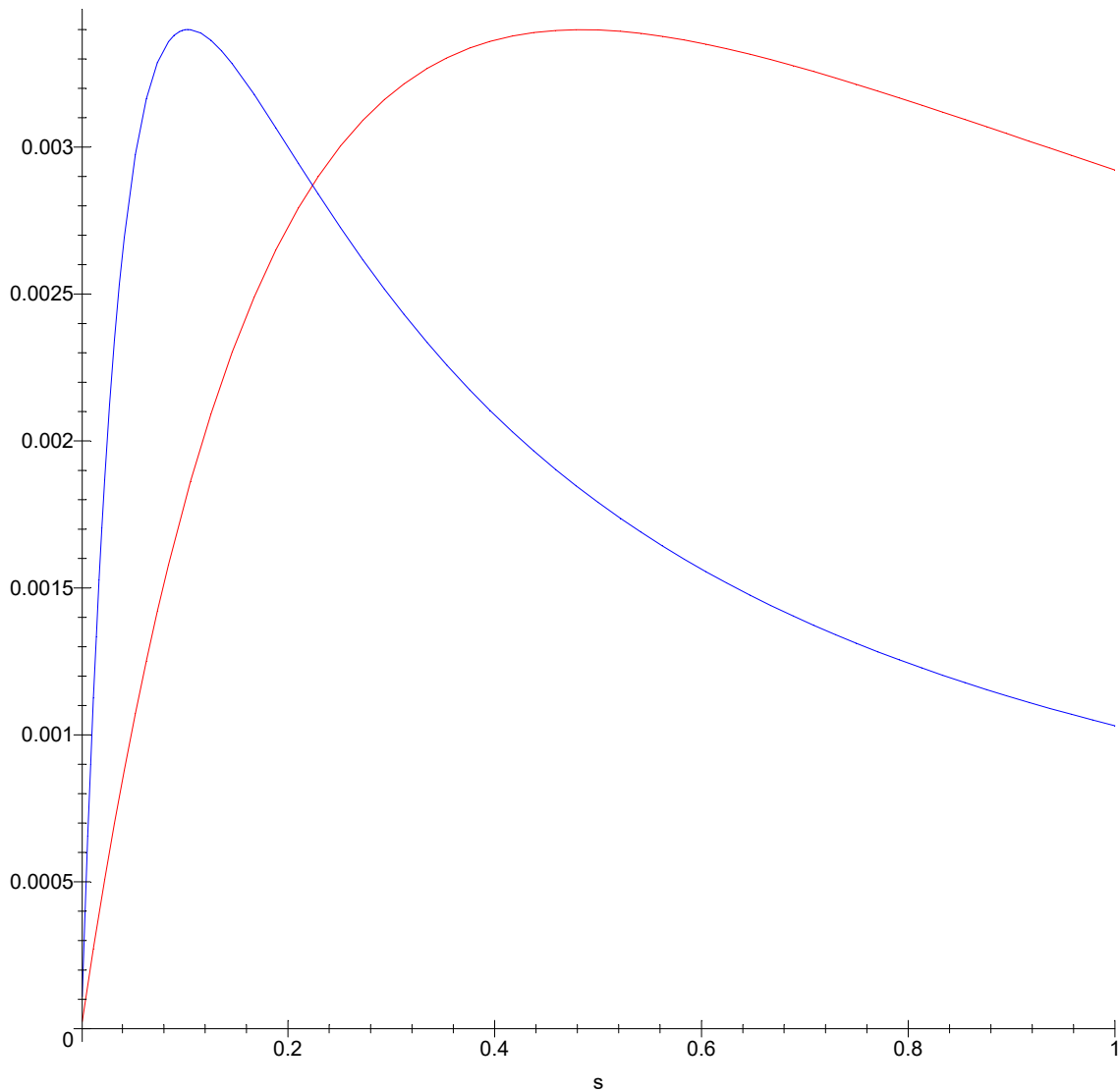
$$.002501 \frac{400 \frac{s^2 (-20.0 s + .15)^2}{((-20.0 s + .15)^2 + (21.0 s + 3.00)^2)} + 400 \frac{s^2 (21.0 s + 3.00)^2}{((-20.0 s + .15)^2 + (21.0 s + 3.00)^2)}}{s}$$

STUDENT > T2:=subs(subs2,T);

T2 :=

$$.01167 \frac{400 \frac{s^2 (-20.0 s + .7)^2}{((-20.0 s + .7)^2 + (21.0 s + 14.0)^2)} + 400 \frac{s^2 (21.0 s + 14.0)^2}{((-20.0 s + .7)^2 + (21.0 s + 14.0)^2)}}{s}$$

STUDENT > plot({T1,T2},s=0.001..1,color=[red,blue],thickness=[0,4]);
#T2=2nd one has higher rotor resistance



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[ STUDENT > # Find slip at the location of Tmax (s_Tmax)
[ STUDENT >
[ STUDENT >
[ STUDENT > dT_ds := (diff(T,s));

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$$dT_ds := \left(2 \frac{s XM^2 Vs^2 \%2^2}{(\%2^2 + \%1^2)^2} - 4 \frac{s^2 XM^3 Vs^2 \%2 X2}{(\%2^2 + \%1^2)^2} \right. \\ \left. - 2 \frac{s^2 XM^2 Vs^2 \%2^2 (-4 \%2 X2 XM + 2 \%1 (XM RI + 2 X2 RI))}{(\%2^2 + \%1^2)^3} + 2 \frac{s XM^2 Vs^2 \%1^2}{(\%2^2 + \%1^2)^2} \right)$$

$$+ 2 \frac{s^2 XM^2 Vs^2 \%1 (XM RI + 2 X2 RI)}{(\%2^2 + \%1^2)^2}$$

$$- 2 \frac{s^2 XM^2 Vs^2 \%1^2 (-4 \%2 X2 XM + 2 \%1 (XM RI + 2 X2 RI))}{(\%2^2 + \%1^2)^3} \Bigg) R2 / (s wsync)$$

$$- \frac{\left(\frac{s^2 XM^2 Vs^2 \%2^2}{(\%2^2 + \%1^2)^2} + \frac{s^2 XM^2 Vs^2 \%1^2}{(\%2^2 + \%1^2)^2} \right) R2}{s^2 wsync}$$

$$\%1 := XM RI s + 2 X2 s RI + R2 XM$$

$$\%2 := -2 X2 s XM + R2 RI$$

STUDENT >

STUDENT > `dT_ds:=simplify(diff(T,s));`

$$dT_ds := - (XM^2 RI^2 s^2 + 4 X2^2 s^2 XM^2 - R2^2 XM^2 + 4 XM RI^2 s^2 X2 + 4 X2^2 s^2 RI^2 - R2^2 RI^2) XM^2 Vs^2 R2 / ((4 X2^2 s^2 XM^2 + R2^2 RI^2 + XM^2 RI^2 s^2 + 4 XM RI^2 s^2 X2 + 2 XM^2 RI s R2 + 4 X2^2 s^2 RI^2 + R2^2 XM^2)^2 wsync)$$

STUDENT > # Exampine dT/ds at slip =0 (slope of torque speed near zero

STUDENT > `simplify(subs(s=0,dT_ds));`

$$\frac{Vs^2 XM^2}{R2 wsync (XM^2 + RI^2)}$$

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STUDENT > `s_Tmax:=solve(dT_ds=0,s);` # as can see entire behavior with R1, R2, X. Loc of peak goes to lower slip (higher speed) as R2 dec, R1 and X inc

$$s_Tmax := \frac{\sqrt{\%1 (XM^2 + RI^2)} R2}{\%1}, - \frac{\sqrt{\%1 (XM^2 + RI^2)} R2}{\%1}$$

$$\%1 := 4 X2^2 XM^2 + XM^2 RI^2 + 4 XM RI^2 X2 + 4 X2^2 RI^2$$

STUDENT > # Choose the positive root

STUDENT > `equation1:=sTmax=s_Tmax[1];`

$$equation1 := sTmax = \frac{\sqrt{(4 X2^2 XM^2 + XM^2 RI^2 + 4 XM RI^2 X2 + 4 X2^2 RI^2) (XM^2 + RI^2)} R2}{4 X2^2 XM^2 + XM^2 RI^2 + 4 XM RI^2 X2 + 4 X2^2 RI^2}$$

STUDENT > `R2:=solve(equation1,R2);`

$$R2 := \frac{sTmax (4 X2^2 XM^2 + XM^2 RI^2 + 4 XM RI^2 X2 + 4 X2^2 RI^2)}{\sqrt{(4 X2^2 XM^2 + XM^2 RI^2 + 4 XM RI^2 X2 + 4 X2^2 RI^2) (XM^2 + RI^2)}}$$

STUDENT > # Above is the value $c_{\tilde{r}}^{-2}$ which gives Maple V Release 4 - Student Edition

speed corresponding to slip sTmax

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STUDENT > s_Tmax1:=evalf(subs(subs1,s_Tmax[1]));

s_Tmax1 := sTmax

STUDENT > Tmax:=subs(s=s_Tmax[1],T);

can see Tmax dec as R2 inc.

CAN ALSO SEE TMAX prop to V^2

$$T_{max} := \left(\frac{sT_{max}^2 XM^2 Vs^2 \left(-2 X2 sT_{max} XM + \frac{sT_{max} \%1 RI}{\sqrt{\%1 (XM^2 + RI^2)}} \right)^2}{\left(\left(-2 X2 sT_{max} XM + \frac{sT_{max} \%1 RI}{\sqrt{\%1 (XM^2 + RI^2)}} \right)^2 + \%2^2 \right)^2} + \frac{sT_{max}^2 XM^2 Vs^2 \%2^2}{\left(\left(-2 X2 sT_{max} XM + \frac{sT_{max} \%1 RI}{\sqrt{\%1 (XM^2 + RI^2)}} \right)^2 + \%2^2 \right)^2} \right) \%1 / (\sqrt{\%1 (XM^2 + RI^2)} wsync)$$

%1 := 4 X2^2 XM^2 + XM^2 RI^2 + 4 XM RI^2 X2 + 4 X2^2 RI^2

%2 := XM RI sTmax + 2 X2 sTmax RI + $\frac{sT_{max} \%1 XM}{\sqrt{\%1 (XM^2 + RI^2)}}$

STUDENT > Tmax1:=evalf(subs(subs1,Tmax));

Tmax1 := .003402

STUDENT > # Note that Tmax is independent of R2. Increasing R2 always moves the peak Tmax toward lower speed but doesn't change the magnitude of the peak

STUDENT > # Also note that we would predict this from the change in slope _____

STUDENT >

STUDENT > # find starting Torque by evaluating torque at s=1

STUDENT > T_start:=subs(s=1,T);

$$T_{start} := \left(\frac{XM^2 Vs^2 \left(-2 X2 XM + \frac{sT_{max} \%1 RI}{\sqrt{\%1 (XM^2 + RI^2)}} \right)^2}{\left(\left(-2 X2 XM + \frac{sT_{max} \%1 RI}{\sqrt{\%1 (XM^2 + RI^2)}} \right)^2 + \%2^2 \right)^2} + \frac{XM^2 Vs^2 \%2^2}{\left(\left(-2 X2 XM + \frac{sT_{max} \%1 RI}{\sqrt{\%1 (XM^2 + RI^2)}} \right)^2 + \%2^2 \right)^2} \right)$$

$$sTmax \%1 / (\sqrt{\%1 (XM^2 + RI^2)} wsync)$$

$$\%1 := 4 X2^2 XM^2 + XM^2 RI^2 + 4 XM RI^2 X2 + 4 X2^2 RI^2$$

$$\%2 := XM RI + 2 X2 RI + \frac{sTmax \%1 XM}{\sqrt{\%1 (XM^2 + RI^2)}}$$

STUDENT > # starting torque is heavily dependent on R2. High R2 gives good start torque and low start current - both great for starting but lousy for run efficiency => deep-bar design or variable resistance on wound-rotor rotor.

STUDENT > # starting torque is also propr to V^2 based on above.

STUDENT > # check that this gives the correct starting torque value for a specific set of circuit values.

STUDENT > subs(subs1, T_start);

$$.02414 \left(400 \frac{(-20.0 + 1.448 sTmax)^2}{((-20.0 + 1.448 sTmax)^2 + (21.0 + 28.96 sTmax)^2)^2} + 400 \frac{(21.0 + 28.96 sTmax)^2}{((-20.0 + 1.448 sTmax)^2 + (21.0 + 28.96 sTmax)^2)^2} \right) sTmax$$

STUDENT > # Summary picture of changing R2 (see earlier graph). As R2 increases, TslopevsS (~V^2/R2) decreases, peak moves to left (same height), starting T increases. There is a crossover

STUDENT >

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STUDENT > # Look at slip vs power in the linear range

STUDENT > # first look at slope of T vs N in linear range near s=0

STUDENT > RunningTSlope:=subs(s=0, dT_ds);

$$RunningTSlope := - \frac{\left(-\frac{sTmax^2 \%1 XM^2}{XM^2 + RI^2} - \frac{sTmax^2 \%1 RI^2}{XM^2 + RI^2} \right) XM^2 Vs^2 sTmax \%1}{\sqrt{\%1 (XM^2 + RI^2)} \left(\frac{sTmax^2 \%1 RI^2}{XM^2 + RI^2} + \frac{sTmax^2 \%1 XM^2}{XM^2 + RI^2} \right)^2 wsync}$$

$$\%1 := 4 X2^2 XM^2 + XM^2 RI^2 + 4 XM RI^2 X2 + 4 X2^2 RI^2$$

STUDENT > # This is same thing we came up with previously.

STUDENT > # High R2 gives lower slope and higher slip (moves peak toward lower speeds)

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STUDENT > #Also note that V^2 gives lower slope and higher slip.

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[ STUDENT > #as a close approximation - speed is constant and "slope"  
of power vs s curve is related to  $V^2$  and  $(1/R^2)$   
[ STUDENT > # And actual value of slip (for given horsepower) is  
directly related to the slope.  
[ STUDENT >  
[ STUDENT > # Summary - ** slip prop to  $R^2/V^2$ . Note that  $R^2$  is  
F(Temperature)  
[ STUDENT >  
[ STUDENT >  
[ STUDENT >
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